

The Purpose of the second technical assignment is to evaluate the existing electrical conditions inside the new George Washington University School of Business and Public management. Using the plans and specifications generously provided to me by Smith Group Inc., a single line diagram and a load summary calculation was performed. Also provided is a narrative on the general information included in the electrical system.

The Load summary Calculations adhere to the NEC standards provided in the NEC Handbook. Loads included in the calculation are lighting loads, receptacle loads, mechanical loads, and elevator loads. Feeders were then sized according to the loads, and the main feeder for the building was also sized accordingly. After compiling the load data, the local power utility data was applied to calculate the building cost.

The overall report is meant to provide general knowledge of the building and its electrical system. It will display both the positive and negative areas of the building and will determine the areas that must be re-evaluated.


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## System Narrative

The electrical power for the new George Washington School of Business and Public Management is fed from an existing system. The utility is run in at $13200-120 \mathrm{~V}$ and split so it runs to an existing substation at Funger Hall, an existing substation at Tompkin Hall and to the new Business School. The system can be described as a primary selective radial distribution system. The building utilizes two separate types of utility voltage, a 480/277 system and a 208/120 system. The 480/277 system feeds the majority of the mechanical equipment and most of the electrical lights for the building. The 208/120 system feeds some of the lights and the receptacles. There are two separate panels for the receptacles, as one has been designated isolated ground for computer loads.

Loads for the building are distributed from three switchboards. Switchboard HDP is $4000 \mathrm{Amp}, 480 / 277$ Volt, 3 phase, and 4 wire. It feeds the $H$ panels which provide power to the lighting systems along with the motor control center and the elevator loads. Switchboard CDP is a $1600 \mathrm{Amp}, 208 / 120$ volt, 3 phase, and 4 wire. It provides power to the C panels which are the isolated ground receptacles. The last switchboard is the NDP one, it is rated at 800 Amps , 208/120 Volt, 3 phase, and 4 wires. It provides power to the H panels which provide power to the normal receptacle loads. Emergency power is provided by a diesel generator found in the penthouse of the building. It is connected by automatic switches which will throw in case of power lose and send emergency power to the elevators and the Emergency panels. Otherwise, the elevator power is provided by HDP Switchboard.

## Transformers

Information on the transformers are provided below. One transformer steps down the primary voltage from 13.8 KVA to 480 V . The rest of the transformers step down the primary voltage to $208 / 120 \mathrm{~V}$.

| Transformer Schedule |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Designation | KVA | Primary Voltage | Secondary Voltage | Remark |  |
| T-1 | 2000 | $13.8 \mathrm{KV}, \Delta$ | $480 / 277 \mathrm{~V}, 3 \mathrm{PH}, 4 \mathrm{~W}$ | Dry |  |
| T-2 | 500 | $13.8 \mathrm{KV}, \Delta$ | $208 / 120 \mathrm{~V}, 3 \mathrm{PH}, 4 \mathrm{~W}$ | K-13 |  |
| T-3 | 225 | $13.8 \mathrm{KV}, \Delta$ | $208 / 120 \mathrm{~V}, 3 \mathrm{PH}, 4 \mathrm{~W}$ | Dry |  |
| T-4 | 112.5 | $480 \mathrm{~V}, \Delta$ | $208 / 120 \mathrm{~V}, 3 \mathrm{PH}, 4 \mathrm{~W}$ | Dry |  |
| T-5 | 3 | $480 \mathrm{~V}, \Delta$ | $208 / 120 \mathrm{~V}, 1 \mathrm{PH}, 3 \mathrm{~W}$ | Dry |  |
| T-6 | 30 | $480 \mathrm{~V}, \Delta$ | $208 / 120 \mathrm{~V}, 3 \mathrm{PH}, 4 \mathrm{~W}$ | Dry |  |

## Emergency

The emergency power for the Business School is provided by a 400 KW , $480 / 277,3 \mathrm{PH}, 4$ wire diesel generator. When power is cut to the building, there are two automatic switches that are thrown automatically. The automatic switch on the top floor in the penthouse redirects the power from the generator to the elevators and also sends power down to the bottom floor and the second automatic switch. Power is directed from the generator in the form of a long wire trough. The second switch provides power to another long wire trough. From the trough, power is run directly to the four emergency lighting panels, which provides all emergency light on the four floors. Power is also run from the trough to a step down transformer to provide 208/120V power to the emergency receptacle power panels.

Power is being supplied to the lighting system through the EH1, ED2, EH5, and ED6 panels. The EH and ED panels are rated at 408/277V, 3ph, and 4 wires. They provide power to the emergency lighting systems, with the EH1 panel providing emergency light on the façade. The ELP, EL1, and EL5 are stepped down to 208/120V. These panels provide power to the emergency receptacles as well as the fire systems. All these panels have a 100 A circuit breakers.

## Protection Devices

There are a variety of different electrical protection devices ranging from where the power is run into the building up into the panels that provide the power to the lights and receptacles. The power is run from the company feed into a switchboard, which is then split and run into the basement of the New Business School. The Power is then fed through another load interrupt switch rated the same as in the switchboard, 600A, 3P, 15 KV , and set at 2 positions.

Power is fed into Switchboard HDP and tapped from there to Switchboards CDP and NDP. Each switchboard is rated with a new 15 KV load interrupt switch in the existing 15 KV cubicle on the board. The switches have the switch itself loaded at the same rate mentioned previously, a 3-100A, $5 \mathrm{M}-5 \mathrm{C}$ type fuse, a lighting arrester at 7.5 Kv , and a Key interlock. Each Switchboard also has a transformer to step down the electrical load. Switchboard HDP has transformer T-1, Switchboard CDP has transformer T-2 and Switchboard NDP has transformer T-3. For more information on the transformer, view the table in the section above.

Once run from the Switchboards, the panels are protected individually with their individual bus ratings, and their wire sizes.

Other forms of electrical protection have already been mentioned in the emergency power section. The switches that divert the power to the emergency system and the generator have already been mentioned. Also, the two circuit breakers leading to the automatic transfer switches have been discussed above in the emergency power section.

## Equipment Location

The electrical equipment is located in two primary locations. The Penthouse level on the roof above the sixth floor holds a lot of the emergency equipment. The generator is located in the mechanical room. Also located there are the wire long wire trough and the automatic transfer switch. Next to the mechanical room is the elevator room. The elevator room contains the elevator panel along with the four elevator motors. The motor control center is also located in the penthouse on the roof.

The electrical room on floor P2 is where the majority of the other big electrical systems are located. The 3 switchboards are located in that electrical room, along with the second wire trough and transformers associated with the emergency system.

The panels for each of the floors are located in electrical rooms on each of the floors.

## Liahtina Sustems

Typical lighting system throughout the building is fluorescent system. Fluorescents are used in the circulation spaces, as well as all of the classrooms and the offices. Classrooms take advantage of primarily indirect light, while the circulation spaces use direct light, and the auditorium takes advantage of cove lighting. The fluorescent systems, of course, operate off of 480/277 V power. Accent lighting and under cabinet fluorescent lighting systems are also used to provide light in areas or on task planes. These systems are run off of 208/120V power.

## Shutoff Requirements

The new Business School takes advantage of numerous types of shut-off devices. Most of the rooms have occupancy sensors. The occupancy sensors are provided so that they detect motion within the rooms. When no motion is detected for a preprogrammed amount of time, the lights will automatically shut off. Another type of system that is used in this building is automatic timers. The timers are set to turn off and on at designated times. This type of lighting is used mainly for circulation spaces where it would not be ideal to place a switch in an open area. The automatic switches are run to the building time clock, and often run to a switch that can be controlled from a more discrete location. Finaly, on the exterior of the building, daylight sensors are used. The daylight sensors measures the amount of daylight being received, and turns the lights on or off accordingly.

## Power Factor

There are no capacitors in my building; therefore there are no major power factor corrections.

## Desian Requirements

The biggest issue in the design requirements is allowing for voltage drops.
Because the building is 6 stories, plus the two floors below grade, you have to take into account voltage drop calculations. These calculations for running wires to the penthouse on the roof are very important to the wire sizing.

## Lamp Data

The plans and specifications were provided for me by Smith Group, who did the lighting and electrical design. Smith Group does not spec product data for lamps and ballasts. Therefore, using the information that was given, I chose a set of general lamps.

| Lamp | Wattage | Initial <br> Lumens | Mean <br> Lumens | CRI | CCT | Ballast |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Compact Fluorescent | 5 W | 250 | 210 | 82 | 2700 | Electronic/Dimming |
| Metal Halide | 150 W | 13250 | 11260 | 88 | 3000 | Electronic/Dimming |
| Metal Halide | 70 W | 6500 | 5200 | 82 | 3000 | Electronic/Dimming |
| Linear Fluorescent | 54 W | 5000 | 4500 | 83 | 3000 | Electronic/Dimming |
| Long Fluorescent | 50 W | 4000 | - | 82 | 3000 | Electronic/Dimming |
| Long Fluorescent | 50 W | 4000 | - | 82 | 3000 | Hi-Lume Dimming |
| Compact Triple Tube | 42 W | 3200 | - | 82 | 3000 | Electronic/Dimming |
| Compact Triple Tube | 32 W | 2400 | - | 82 | 3000 | Electronic/Dimming |
| Linear Fluorescent | 32 W | 3100 | 2959 | 85 | 3000 | Electronic/Dimming |
| Linear Fluorescent | 28 W | 2800 | - | 85 | 3000 | Electronic/Dimming |
| Linear Fluorescent | 28 W | 2800 | - | 85 | 3000 | Hi-Lume Dimming |
| Compact Triple Tube | 26 W | 1800 | - | 83 | 3000 | Electronic/Dimming |
| Compact Triple Tube | 18 W | 1200 |  | 83 | 3000 | Electronic/Dimming |
| Short Tube Compact | 9 W | 600 | - | 82 | 2700 | Electronic/Dimming |
| Short Tube Compact | 5 W | 250 | 210 | 82 | 2700 | Electronic/Dimming |

Mechanical Equipment

| Description | HP | KVA | Voltage | Phase | $\begin{gathered} \text { Comb. Starter } \\ \text { Size } \end{gathered}$ | Nema. Encl. | $\begin{gathered} \hline \text { CB } \\ \text { Size } \end{gathered}$ | Wiring Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AHU-1 | $\begin{array}{\|l\|} \hline \text { "1-25" } \\ " 1-7.5 " \end{array}$ | 35.8 | 480 | 3 | - | 1 | 90 | 3/4 + 1/10 G. 3/4"C |
| AHU-2 | $\begin{array}{\|c} \text { "1-15" } \\ \text { "1-7.5" } \\ \hline \end{array}$ | 35.5 | 480 | 3 | - | 1 | 60 | 3/8 + 1/10 G. 3/4"C |
| AHU-3 | $\begin{aligned} & \text { "1-20" } \\ & \text { "1-7.5" } \\ & \hline \end{aligned}$ | 30.2 | 480 | 3 | - | 1 | 90 | 3/6 + 1/10 G. 3/4"C |
| AHU-4 | $\begin{aligned} & \hline \text { "1-20" } \\ & \text { "1-5" } \end{aligned}$ | 27.5 | 480 | 3 | - | 1 | 70 | 3/6 + 1/10 G. 3/4"C |
| AHU-5 | $\begin{aligned} & \hline " 1-25 " \\ & " 1-10 " \\ & \hline \end{aligned}$ | 38.2 | 480 | 3 | - | 1 | 90 | 3/4 + 1/10 G. 1"C |


| AHU-6 | $\begin{gathered} " 1-25 " \\ \text { "1-7.5" } \\ \hline \end{gathered}$ | 35.8 | 480 | 3 | - | 1 | 90 | 3/4 + 1/10 G. 3/4"C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AHU-7 | $\begin{aligned} & \hline " 1-15 " \\ & " 1-7.5 " \\ & \hline \end{aligned}$ | 25.5 | 480 | 3 | - | 1 | 60 | 3/8+1/10 G. 3/4"C |
| AHU-8 | $\begin{aligned} & \hline " 1-20 " \\ & " 1-7.5 " \end{aligned}$ | 30.2 | 480 | 3 | - | 1 | 90 | 3/6 + 1/10 G. 3/4"C |
| AHU-9 | $\begin{aligned} & \hline \text { "1-15" } \\ & \text { "1-5" } \end{aligned}$ | 22.8 | 480 | 3 | - | 1 | 60 | 3/8+1/10 G. 3/4"C |
| AHU-10 | $\begin{aligned} & \text { "1-15" } \\ & \text { "1-5" } \end{aligned}$ | 22.8 | 480 | 3 | - | 1 | 60 | 3/8 + 1/10 G. 3/4"C |
| AHU-11 | $\begin{aligned} & \text { "1-20" } \\ & \text { "1-5" } \end{aligned}$ | 27.5 | 480 | 3 | - | 1 | 70 | 3/6 + 1/10 G. 3/4"C |
| AHU-12 | $\begin{aligned} & \text { "1-20" } \\ & \text { "1-5" } \\ & \hline \end{aligned}$ | 27.5 | 480 | 3 | - | 1 | 70 | 3/6+1/10 G. 3/4"C |
| P-17 AHU-1 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| P-18 AHU-2 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} \hline 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| P-10 AHU-3 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| P-20 AHU-4 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| P-21 AHU-5 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} \hline 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| P-22 AHU-6 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| P-23 AHU-7 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| P-24 AHU-8 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| P-25 AHU-9 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4^{4} \mathrm{C} \\ \hline \end{gathered}$ |
| P-26 AHU-10 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| P-27 AHU-11 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} \hline 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| P-28 AHU-12 <br> Preheat Coil | "3/4" | 1.1 | 480 | 3 | - | 1 | 15 | $\begin{gathered} 3 / 12+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| P-32 FOR BCU-1 | "1/3" | 0.8 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| P-33 FOR BCU-2 | "1/3" | 0.8 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} \hline 2 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| AIRC-1 | "2-1/2" | 2.3 | 208 | 1 | 1 | 1 | 20 | $\begin{gathered} 2 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| TRACKTION ELEVATOR | 75 | 76.4 | 480 | 3 | - | 1 | 175 | $\begin{gathered} 3 / 1+1 / 6 \text { G. } 1 \\ 1 / 2^{2 " C} \\ \hline \end{gathered}$ |
| HYDRAULIC ELEVATOR | 60 | 61.3 | 480 | 3 | - | 1 | 150 | $\begin{gathered} 4 / 2+1 / 6 \text { G. } 1 \\ 1 / 4 " C \end{gathered}$ |


| HEATING COIL, AC-4 |  | 3.8 | 208 | 1 | $\begin{gathered} \text { 30A, 2P, } \\ \text { NFSS } \end{gathered}$ | 1 | 25 | $\begin{gathered} 2 / 12+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HEATING COIL, AC-5 |  | 7.5 | 208 | 1 | 30A, 2P, NFSS | 1 | 45 | 2/6 + 1/10 G. 3/4"C |
| HEATING COIL, AC-6, AC-7 |  | 10 | 480 | 3 | 30A, 2P, NFSS | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| $\begin{gathered} \hline \text { CU- } 2,3,13.5 \mathrm{RLA} \\ 2-3 / 4 \mathrm{HP} \\ \text { CONDENSER } \end{gathered}$ | $\begin{aligned} & \text { "2- } \\ & 3 / 4 " \\ & \hline \end{aligned}$ | 13 | 480 | 3 | 1 | 1 | 40 | $\begin{gathered} 3 / 10+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| CU-4, 14.7 RLA, $1 / 4 \mathrm{HP}$ CONDENSER | "1/4" | 3.7 | 208 | 1 | 1 | 1 | 40 | 2/8 + 1/10 G. 3/4"C |
| $\begin{gathered} \text { CU-5, 7.7 RLA, 1- } \\ 1 / 12 \mathrm{HP} \\ \text { CONDENSER } \end{gathered}$ | "1/12" | 1.8 | 208 | 1 | 1 | 1 | 20 | $\begin{gathered} 2 / 12+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| $\begin{gathered} \text { CU-6,7 13.5 RLA, } \\ 2-3 / 4 \mathrm{HP} \\ \text { CONDENSER } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { "2- } \\ & 3 / 4 \end{aligned}$ | 13 | 480 | 3 | 1 | 3R | 40 | $\begin{gathered} 3 / 10+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| AC-2,3,6,7 | $\begin{aligned} & " 1- \\ & 1 / 2 " \end{aligned}$ | 2.1 | 480 | 3 | 1 | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| AC-4 | "1/2" | 1.1 | 208 | 1 | 1 | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| AC-5 | "1/4" | 0.7 | 208 | 1 | 1 | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| CDP-1 | "1/5" | 670 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| EFT-1 | - | 1.5 | 277 | 1 | - | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| EFT-2 | - | 1 | 277 | 1 | - | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| EFT-3 | - | 1.5 | 120 | 1 | - | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EHT-1,2 | - | - | 277 | 1 | - | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-1.1,1.3 | 10 | 11.2 | 480 | 3 | 1 | 1 | 30 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-1.2 | 10 | 11.2 | 480 | 3 | 1 | 1 | 30 | $\begin{gathered} 6 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| EF-2,3 | 10 | 11.2 | 480 | 3 | 1 | 1 | 30 | $\begin{gathered} 6 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| EF-4 | 15 | 16.7 | 480 | 3 | 2 | 1 | 40 | $\begin{gathered} 3 / 10+1 / 10 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-5 | "1/3" | 0.83 | 480 | 1 | Manuel | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-6A, 6B | "3/4" | 2.1 | 120 | 3 | 1 | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-7 | "1/3" | 0.83 | 480 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |


| EF-8 | "1/3" | 0.83 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EF-9 | "1/3" | 0.83 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} \hline 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-10 | "1/5" | 0.67 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-11 | "1/5" | 0.67 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-12 | "1/6" | 0.51 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \\ \hline \end{gathered}$ |
| EF-13 | - | 0.08 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-14 | - | 0.06 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-15 | - | 0.06 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-16 | - | 0.06 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} \hline 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-17 | - | 0.08 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-18 | - | 0.14 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-19 | - | 0.05 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EF-20 | - | 0.3 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EF-21 | "1/4" | 0.67 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \end{gathered}$ |
| OAF-1 | "1/4" | 0.67 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| SF-17,18 | 30 | 31.8 | 480 | 3 | 3 | 3R | 90 | 3/6 + 1/10 G. 3/4"C |
| VCB-1F,2F | "1/3" | 0.83 | 277 | 1 | 1 | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 \text { " } \mathrm{C} \end{gathered}$ |
| VCB-3F | "2-1/3" | 1.7 | 277 | 1 | 1 | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| UH-1 | "1/20" | 0.25 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| EUH-1 | - | 3.3 | 277 | 1 | 1 | 1 | 15 | $\begin{gathered} \hline 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EUH-2 | - | 5 | 277 | 1 | 1 | 1 | 25 | $\begin{gathered} \hline 2 / 10+1 / 10 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EUH-3 | - | 7.5 | 277 | 1 | 2 | 1 | 35 | 2/8 + 1/10 G. 3/4"C |
| CUH-1 | "1/15" | 0.3 | 120 | 1 | - | 1 | 15 | $3 / 8+1 / 10$ G. $3 / 4 \mathrm{C}$ |
| CUH-2 | "1/10" | 0.4 | 120 | 1 | - | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |


| BCU-1 | 5 | 6 | 480 | 3 | 1 | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BCU-2 | "1 1/2" | 2.1 | 480 | 3 | 1 | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \end{gathered}$ |
| BCU-3 | 1 | 1.4 | 480 | 3 | 1 | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{G} . \\ 3 / 4^{\prime \prime} \mathrm{C} \\ \hline \end{gathered}$ |
| EWH-1 | - | 3 | 277 | 1 | $\begin{gathered} \text { 30A, 2P, } \\ \text { NFSS } \end{gathered}$ | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{G} . \\ 3 / 4 " \mathrm{C} \\ \hline \end{gathered}$ |

Total $\mathrm{KVA}=1368.12 \mathrm{KVA}$

## Plumbina Equipment

| Description | HP | KVA | Voltage | Phase | $\begin{gathered} \text { Comb. Starter } \\ \text { Size } \end{gathered}$ | Nema. Encl. | $\begin{gathered} \hline \mathrm{CB} \\ \text { Size } \\ \hline \end{gathered}$ | Wiring Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fire Pump Fp-1 | 75 | 76.4 | 480 | 3 | - | 1 | - | 3/1/0 + 1/6 g. 2"C |
| $\begin{aligned} & \text { Jockey Pump JP } \\ & -1 \end{aligned}$ | "11/2" | 2.1 | 480 | 3 | 1 | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 " \\ \mathrm{C} \end{gathered}$ |
| Electric Water Heater DWH-1 | - | 18 | 480 | 3 | 30A, 3P, NFSS | 1 | 30 | $\begin{gathered} 3 / 10+1 / 10 \mathrm{g.} 3 / 4 \mathrm{"} \\ \mathrm{C} \end{gathered}$ |
| Electric Water Heater DWH-2 | - | 18 | 480 | 3 | 30A, 3P, NFSS | 1 | 30 | $\begin{gathered} 3 / 10+1 / 10 \mathrm{~g} \cdot 3 / 4 " \\ \mathrm{C} \end{gathered}$ |
| Electric Water Heater DWH-3 | - | 3 | 277 | 1 | 30A, 3P, NFSS | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 " \\ \mathrm{C} \end{gathered}$ |
| Cooling Tower Pump, CT-1 | $\begin{gathered} 1 \\ 1 / 2 " \end{gathered}$ | 2.1 | 480 | 3 | 1 | 3R | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 " \\ \mathrm{C} \end{gathered}$ |
| Elevator Sump Pump | "1/2" | 1.1 | 120 | 1 | Manual | 3R | 20 | - |
| Sewage Ejector <br> Pump, SSP -1 | 2 | 2.7 | 480 | 3 | 1 | 3R | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 " \\ \mathrm{C} \end{gathered}$ |
| Duplex Sump <br> Pump, DSP-1 | 5 | 6.1 | 480 | 3 | 1 | 3R | 15 | $\stackrel{3 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 "}{ }$ |
| Air Compressor, AC-1, Fire Pump Room | "1 1/2" | 2.1 | 480 | 3 | 1 | 1 | 15 | $\begin{gathered} 3 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 " \\ \mathrm{C} \end{gathered}$ |
| Recirculating Pump, HWRP-1 Penthouse | "1/8" | 0.4 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 " \\ \mathrm{C} \\ \hline \end{gathered}$ |
| Recirculating Pump, HWRP-2 Penthouse | "1/40" | 0.2 | 120 | 1 | Manual | 1 | 15 | $\begin{gathered} 2 / 12+1 / 12 \mathrm{~g} \cdot 3 / 4 \mathrm{"} \\ \mathrm{C} \end{gathered}$ |

Total $\mathrm{KVA}=132.2 \mathrm{KVA}$

## NEC Load Calculations

The Lighting Loads have been calculated according to NEC table 220.3A.

|  | 1st floor |  |  |
| :---: | :---: | :---: | :---: |
|  | Area | Load Factor | VA |
| Classroom | 14187 | 3 | 42561 |
| Circulation | 5184 | 0.5 | 2592 |


| 2nd Floor |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Area | Load Factor | VA |
| Classroom | 13900 | 3 | 41700 |
| Circulation | 5600 | 0.5 | 2800 |


| 3rd Floor |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Area | Load Factor | VA |
| Classroom | 13900 | 3 | 41700 |
| Circulation | 5600 | 0.5 | 2800 |

4th Floor

|  | Area | Load Factor | VA |
| :---: | :---: | :---: | :---: |
| Classroom | 13900 | 3 | 41700 |
| Circulation | 5600 | 0.5 | 2800 |

## 5th Floor

|  | Area | Load Factor | VA |
| :---: | :---: | :---: | :---: |
| Classroom | 13900 | 3 | 41700 |
| Circulation | 5600 | 0.5 | 2800 |

6th Floor

|  | Area | Load Factor | VA |
| :---: | :---: | :---: | :---: |
| Classroom | 13900 | 3 | 41700 |
| Circulation | 5600 | 0.5 | 2800 |

P1 and P2

|  | Area | Load Factor | VA |
| :---: | :---: | :---: | :---: |
| P1 Garage | 19500 | 0.5 | 9750 |
| P2 Garage | 19500 | 0.5 | 9750 |

The Receptacle loads were taken from the panel boards. Feeder sizes were calculated by using the KVA loads from the existing panels.

## Receptacle Loads

Receptacle Loads
Ampacity
$\mathrm{I}=(\mathrm{KVA} * 1000) /(\operatorname{sqrt}(3) * \mathrm{~V})$
Amps

$\mathrm{I}=$| 1.25 |  |
| ---: | ---: |
| I | Sized |
| 159.3 | 199.2 |
| 303.7 | 379.6 |


| 2nd Floor | KVA |
| :--- | ---: |
| C2 | 58.6 |
| C2A | 37.1 |
| C2B | 32.2 |
| N2 | 23.5 |
| N2B | 8.7 |


| Non IG <br> VA | 32.2 |
| :--- | :--- |
| IG VA | 95.7 |



| 3rd Floor | KVA |
| :--- | ---: |
| C3 | 66 |
| C3a | 40.6 |
| C3B | 40.4 |
| N3 | 19.1 |
| N3B | 3.4 |


| Non IG <br> VA | 19.1 |
| :--- | :---: |
| IG VA | 106.6 |



| 4th Floor | KVA |
| :--- | ---: |
| C4 | 47.7 |
| C4B | 17.6 |
| N4 | 32 |
| N4B | 7.6 |


| Non IG <br> VA | 32 |
| :--- | :---: |
| IG VA | 65.3 |


| Amps | $\begin{aligned} & 1.25 \\ & \text { Sized } \end{aligned}$ |
| :---: | :---: |
| 88.8 | 111.0 |
| 181.3 | 226.6 |


| 5th Floor | KVA |
| :--- | ---: |
| C5 | 50.5 |
|  |  |
| C5B | 10.9 |
|  |  |
| N5 | 27.8 |
| N5B | 6.1 |


| Non IG |  |
| :--- | :--- |
| VA | 27.8 |
| IG VA | 61.4 |


| Amps |  | $\begin{aligned} & 1.25 \\ & \text { Sized } \end{aligned}$ |
| :---: | :---: | :---: |
| $\mathrm{I}=$ | 77.2 | 96.5 |
| $\mathrm{I}=$ | 170.4 | 213.0 |


| 6th Floor | KVA |
| :--- | ---: |
| C6 | 71.3 |
| C6B | 36.6 |
|  |  |
| N6 | 49.3 |
|  |  |
| N6A | 19.9 |
| N6B | 8.7 |


| Non IG <br> VA | 49.3 |
| :--- | :---: |
| IG VA | 107.9 |



| P1-P2 | KVA |
| :--- | ---: |
| NP2 | 29.5 |
| NPH | 4.8 |


| Non IG <br> VA | 29.5 |
| :--- | :---: |
| Non IG |  |
| VA | 4.8 |



| Total $\mathrm{VA}=$ | 954.1 |
| :--- | :--- |


| Total $N$ Panel VA $=$ | 335.2 |
| :--- | :--- |
| Total C Panel VA $=$ | 618.9 |

Elevator Loads were calculated by sizing the loads on the existing panel.

| KVA $=$ | 367.2 |
| :--- | :--- |

To size the main electrical feed, the loads of all the systems were summed and accounted for.

Main Feed

| N Panels | C Panels | Elevators | Lighting | 480/277 Mech |  |
| ---: | ---: | ---: | ---: | ---: | :--- |
| 335.2 | 618.9 | 367.2 | 245.5 | 795.0 |  |

$$
\begin{array}{|r|r|r|}
\hline \text { total }= & 2361.8 & 3542.63 \\
\hline
\end{array}
$$

The second number is the KVA load value after being sized up by the typical 1.25 factor. The feeder must be sized with a 15 KV conductor, and in this case placed in 3/2AWG wire size with a 4 " conductor.

Below is the comparison of the existing feeder size and wire feeds to what I calculated above for the receptacle panels.

First Floor

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| IG | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ |
| Non-IG | $175 \mathrm{~A}, 4 / 2 / 0$ AWG | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |

Second Floor

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| IG | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ |
| Non-IG | $150 \mathrm{~A}, 4 / 1 / 0 \mathrm{AWG}$ | $150 \mathrm{~A}, 4 / 1 / 0 \mathrm{AWG}$ |

Third Floor

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| IG | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ |
| Non-IG | $150 \mathrm{~A}, 4 / 1 / 0 \mathrm{AWG}$ | $70 \mathrm{~A}, 4 / 4 \mathrm{AWG}$ |

Fourth Floor

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| IG | $250 \mathrm{~A}, 5 / 250 \mathrm{MCM}$ | $250 \mathrm{~A}, 5 / 250 \mathrm{MCM}$ |
| Non-IG | $150 \mathrm{~A}, 4 / 1 / 0 \mathrm{AWG}$ | $150 \mathrm{~A}, 4 / 1 / 0 \mathrm{AWG}$ |

## Fifth Floor

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| IG | $250 \mathrm{~A}, 5 / 250 \mathrm{MCM}$ | $250 \mathrm{~A}, 5 / 250 \mathrm{MCM}$ |
| Non-IG | $225 \mathrm{~A}, 4 / 4 / 0 \mathrm{AWG}$ | $110 \mathrm{~A}, 4 / 1 \mathrm{AWG}$ |

Sixth Floor

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| IG | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ | $375 \mathrm{~A}, 5 / 500 \mathrm{MCM}$ |
| Non-IG | $110 \mathrm{~A}, 3 / 1 \mathrm{AWG}$ | $175 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |

P1 and P2

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| IG | - | - |
| Non-IG | $40 \mathrm{~A}, 4 / 8$ AWG | $30 \mathrm{~A}, 4 / 8$ AWG |

For the most part, the feeders are sized properly. There are a few instances where the calculations to not mimic the existing conditions. This is most likely due to the type of loads contained on the panel board.

The calculations for the lighting loads are provided below along with the existing wire and feeder sizes for the building.

Liahtina Calculations

|  | Existing Panel | Calculated Panel |
| :--- | :--- | :--- |
|  | Feeder Size | Feeder Size |
| First Floor | $225 \mathrm{~A}, 4 / 4 / 0 \mathrm{AWG}$ | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |
| Second Floor | $225 \mathrm{~A}, 4 / 4 / 0 \mathrm{AWG}$ | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |
| Third Floor | $225 \mathrm{~A}, 4 / 4 / 0 \mathrm{AWG}$ | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |
| Fourth Floor | $225 \mathrm{~A}, 4 / 4 / 0 \mathrm{AWG}$ | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |
| Fifth Floor | $225 \mathrm{~A}, 4 / 4 / 0 \mathrm{AWG}$ | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |
| Sixth Floor | $225 \mathrm{~A}, 4 / 4 / 0 \mathrm{AWG}$ | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |
| P1 and P2 | $250 \mathrm{~A}, 5 / 250 \mathrm{MCM}$ | $200 \mathrm{~A}, 4 / 2 / 0 \mathrm{AWG}$ |

Calculated KVA for each floor of the lighting load was calculated at approximately 45 KVA . It was then sized up and a feeder size was calculated according to that sized value. These panel boards also have various pieces of mechanical equipment on them, which would account for why the existing conditions is slightly larger than what was calculated.

## POTOMAC ELECTRIC POWER COMPANY

DISTRICT OF COLUMBIA
STANDARD OFFER SERVICE RATES
EFFECTIVE FEBRUARY 8, 2005 THROUGH MAY 31, 2006

## GENERAL SERVICE PRIMARY SERVICE SCHEDULE "GS 3A"

|  | Billing <br> Months of <br> June - October <br> (Summer) | Billing <br> Months of <br> November - May <br> (Winter) |
| :---: | :---: | :---: |
| Generation |  |  |
| First 6,000 kwh | \$ 0.06826 per kwh | \$ 0.06478 per kwh |
| Additional kwh | \$ 0.06809 per kwh | \$ 0.06379 per kwh |
| First 25 kw | No charge | No charge |
| Additional kw | \$ 0.42377per kw | \$ 0.37121 per kw |
| Procurement Cost Adjustment | www.pepc | monthly rate |
| Transmission |  |  |
| All kwh | \$ 0.00349 per kwh | \$ 0.00349 per kwh |
| Distribution |  |  |
| Customer Charge | \$ 6.48 per month | \$ 6.48 per month |
| First 6,000 kwh | \$ 0.04067 per kwh | \$ 0.03371 per kwh |
| Additional kwh | \$ 0.02558 per kwh | \$ 0.01654 per kwh |
| First 25 kw |  | - |
| Additional kw | \$ 4.69 per kw | \$ 4.09 per kw |
| Delivery Tax | \$ 0.0077 per kwh | \$ 0.0077 per kwh |
| Public Space Occupancy Surcharge | \$ 0.00159 per kwh | \$ 0.00159 per kwh |
| Administrative Credit | www.pepco.com/dc-rates/ for monthly rate |  |
| Reliability Energy Trust Fund | \$ 0.0001 per kwh | \$ 0.0001 per kwh |

## Ltility Information

Because the new Business School has not yet been completed, the cost data for a typical month can not yet be calculated. Knowing that the provider was Pepco, I went to their site and picked out cost data that I believed would applied. Applying the General Service Primary Service Schedule "FS 3A" from the Large Commercial Customer section. Provided below is a copy of those rates for February $8^{\text {th }} 2005$ through May $31^{\text {st }}$ 2006. Also Included is the calculated rate for the KVA data that I calculated above. The rate was calculated for an assumed 12 hour day at full load. KW was not considered.

June - 30 days

$$
K V A=2400
$$

Hours $=12$
Generation
6000 kwh $\$ .06826$ kwh
additional $\quad \$ .06809 \mathrm{kwh}$
Transmission
all kwh $\$ .00349 \mathrm{kwh}$

## Distribution

$\$ 6.48$ per month
6000 kwh 0.04067 kwh
additional $\$ .02558 \mathrm{kwh}$
Delivery Tax
$\$ .0077$ per kwh
Public Space Occupancy $\$ .00159 \mathrm{kwh}$
Reliability Energy Trust Fund $\$ .0001$ kwh

KWH Cost $=\$ 94,812.48$

November - 30 days

$$
\begin{aligned}
\text { KVA } & =2400 \\
\text { Hours } & =12
\end{aligned}
$$

Generation
$6000 \mathrm{kwh} \quad \$ .06478 \mathrm{kwh}$
additional $\$ .06379 \mathrm{kwh}$
Transmission
all kwh $\quad \$ .00349 \mathrm{kwh}$
Distribution
$\$ 6.48$ per month
$6000 \mathrm{kwh} \quad \$ .03371 \mathrm{kwh}$
additional $\$ .01654 \mathrm{kwh}$
Delivery Tax
$\$ .0077$ per kwh
Public Space Occupancy
$\$ .00159 \mathrm{kwh}$
Reliability Energy Trust Fund
\$. 0001 kwh
KWH Cost $=\quad \$ 83,808.72$

