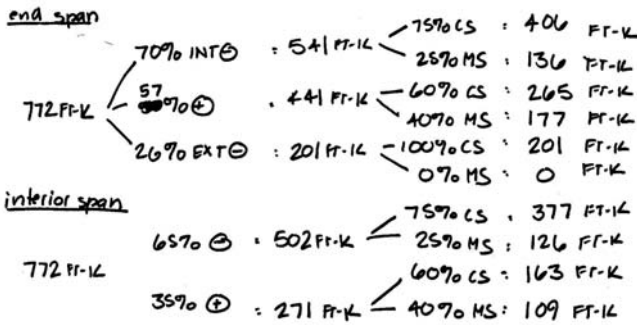


APPENDIX B: CONCRETE FLOOR SYSTEM CALCULATIONS

Direct Design Method, Office Slab with Drops, 30'-0" Maximum Span Condition

OFFICE FLAT PLATE W/ DROPS

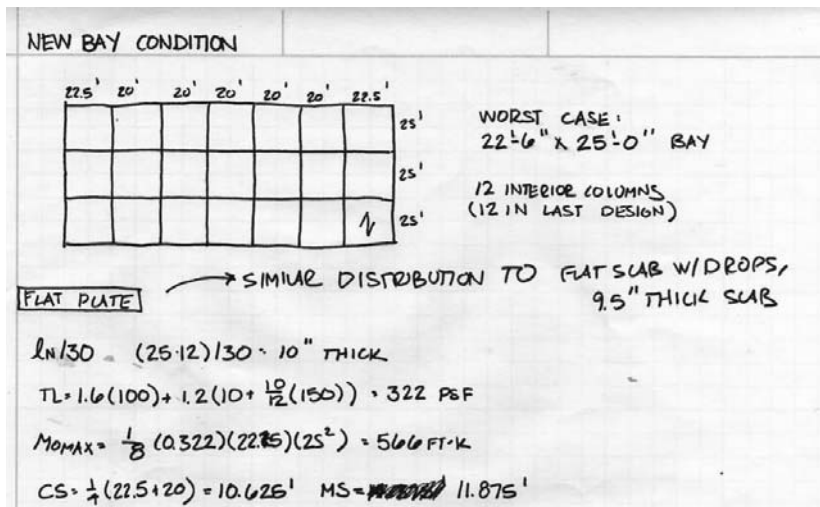
11" THICK 4000 psi NW CONCL., 3" DROPS, 6'-8" x 10'-0"
 $TL = 1.6(100) + 1.2(10 + \frac{1}{12}(150)) + 6 = 343$ PSF
 $M_{0MAX} = \frac{1}{8}(0.343)(20)(30^2) = 772$ FT-K
 CS = 9.375' MS = 10.625'



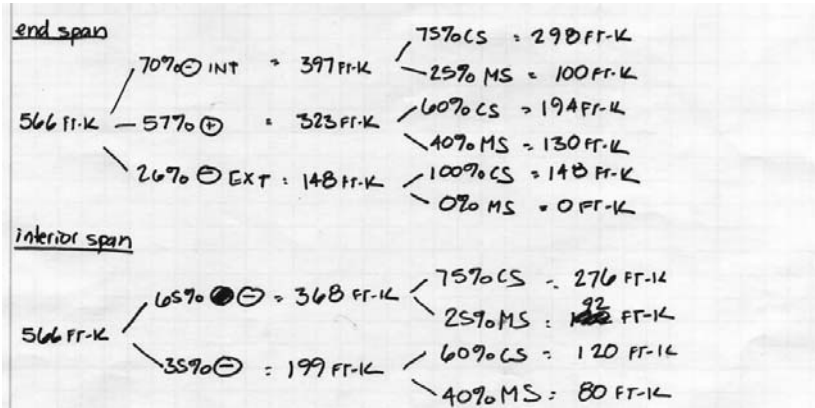
(FLAT SLAB W/ DROPS)

$406 \text{ FT-K} (12) / 9.375 = 520 \text{ IN-K/FT}$ $d = 13"$
 $A_s = \frac{520}{0.9(60)(0.9(\frac{13}{16}))} = 0.823 \text{ IN}^2 \rightarrow \#6 @ 6" A_s = 0.88 \text{ IN}^2$
 $d = 12.875$ $a = 0.88(60) / 0.85(4)(12) = 1.294$
 $\phi M_N = 0.9(60)(0.88)(12.875 - 0.5(1.294)) = 581 \text{ IN-K}$

Direct Design Method, Office Flat Plate, 25'-0" Maximum Span Condition



Direct Design Method, Office Flat Plate, 25'-0" Maximum Span Condition, Cont'd



(MAX MOMENT COND - TWT PLATE)

$$M = 298(12)/10.625 = 337 \text{ IN-K/FT} \quad d \approx 9''$$

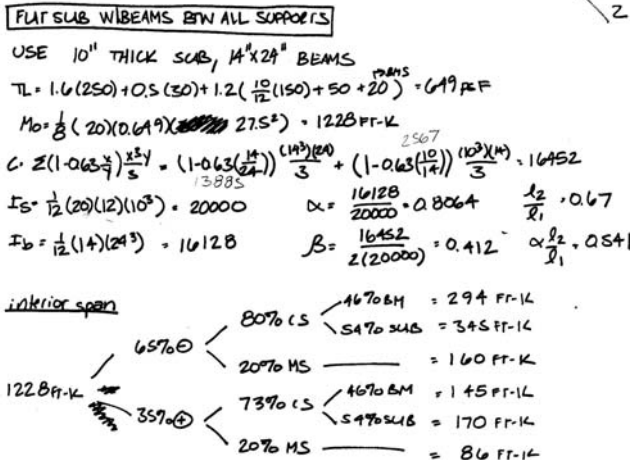
$$A_s = \frac{337}{0.9(60)(0.9)(9)} = 0.77 \text{ IN}^2 \quad \text{USE } \boxed{\#4 @ 3''}$$

$$d = 10 - 0.75 - 0.5(0.5) = 9''$$

$$a = \frac{0.80(60)}{0.85(4)(12)} = 1.17 \text{ IN}$$

$$\phi M_n = 0.9(60)(0.80)(9 - 0.5(1.17)) = 364 \text{ IN-K/FT} \checkmark$$

Direct Design Method, Parking Slab with Beams Between All Columns



(BEAMS)

$$M = 345(12)/8.375 = 495 \text{ IN-K/FT} \quad d \approx 10 - 0.75 - 0.5 = 8.75''$$

$$A_s = \frac{495}{0.9(60)(0.9)(8.75)} = 1.16 \text{ IN}^2 \rightarrow \boxed{\#5 @ 3''} \quad A_s = 1.24''$$

$$d = 10 - 0.75 - 0.5(0.625) = 8.9375 \quad a = \frac{1.24(60)}{0.85(4)(12)} = 1.83$$

$$\phi M_n = 0.9(1.24)(60)(8.9375 - 0.5(1.83)) = 537 \text{ IN-K/FT}$$

→ BEAM $M = 294(12) = 3528 \text{ IN-K} \quad d \approx 24 - 1.5 - 0.5 = 22 \text{ IN}$

$$A_s = \frac{3528}{0.9(60)(0.9)(22)} = 3.3 \text{ IN}^2 \rightarrow \boxed{\text{USE } 4 \#9} \quad A_s = 4.0$$

$$d = 21.936 \quad a = \frac{4(60)}{0.85(4)(14)(4)} = 5.04$$

$$\phi M_n = 0.9(4)(60)(21.936 - \frac{1}{2}(5.04)) = 4194 \text{ IN-K}$$

Selected ADOSS Results, Alternative #2 Office Flat Slab with Drops

```

FILE NAME          P:\ODROPSFA.ADS
PROJECT ID.       Office Final Drops
SPAN ID.          BC
ENGINEER          Henry
DATE              02/09/06
TIME              09:11:02
UNITS             U.S. in-lb
CODE              ACI 318-89
SLAB SYSTEM       FLAT SLAB SYSTEM
FRAME LOCATION    INTERIOR
DESIGN METHOD      STRENGTH DESIGN
MOMENTS AND SHEARS NOT PROPORTIONED
    
```

NUMBER OF SPANS 7

SOLID HEAD DIMENSIONS : COMPUTED BY PROGRAM

```

CONCRETE FACTORS      SLABS          BEAMS          COLUMNS
DENSITY(pcf )         150.0          150.0          150.0
TYPE                  NORMAL WGT     NORMAL WGT     NORMAL WGT
f'c (ksi)             4.0            4.0            4.0
fct (psi)              423.7          423.7          423.7
fr (psi)               474.3          474.3          474.3
    
```

```

REINFORCEMENT DETAILS: NON-PRESTRESSED
YIELD STRENGTH Fy = 60.00 ksi
DISTANCE TO RF CENTER FROM TENSION FACE:
  AT SLAB TOP = 1.50 in OUTER LAYER
  AT SLAB BOTTOM = 1.50 in OUTER LAYER
MINIMUM FLEXURAL BAR SIZE:
  AT SLAB TOP = # 4
  AT SLAB BOTTOM = # 4
MINIMUM SPACING:
  IN SLAB = 6.00 in
    
```

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 12:15:29 PM Licensed to: ae, university park, PA

SPAN/LOADING DATA

SPAN NUMBER	LENGTH		WIDTH		SLAB SYSTEM	DESIGN STRIP (ft)	COLUMN STRIP** (ft)	UNIFORM LOADS	
	L1 (ft)	Tslab (in)	LEFT (ft)	L2*** RIGHT (ft)				S. DL (psf)	LIVE (psf)
1*	1.3	10.0	11.3	15.0	2	26.3	.0	10.0	100.0
2	30.0	10.0	11.3	15.0	2	26.3	13.1	10.0	100.0
3	30.0	10.0	11.3	15.0	2	26.3	13.1	10.0	100.0
4	25.0	10.0	11.3	15.0	2	26.3	11.9	10.0	100.0
5	30.0	10.0	11.3	15.0	2	26.3	13.1	10.0	100.0
6	30.0	10.0	11.3	15.0	2	26.3	13.1	10.0	100.0
7*	1.3	10.0	11.3	15.0	2	26.3	.0	10.0	100.0

* -Indicates cantilever span information.
 ** -Strip width used for positive flexure.
 ***-L2 widths are 1/2 dist. to transverse column.
 "E"-Indicates exterior strip.

LATERAL LOAD/OUTPUT DATA

LATERAL LOADS ARE SPECIFIED AS BEING CAUSED BY WIND

JOINT NO.	SLAB MOMENTS		COLUMN MOMENTS	
	LEFT (ft-k)	RIGHT (ft-k)	ABOVE (ft-k)	BELOW (ft-k)
1	.00	-71.00	.00	.00
2	-71.00	-65.00	.00	.00
3	-63.00	-71.00	.00	.00
4	-71.00	-63.00	.00	.00
5	-64.00	-70.00	.00	.00
6	-61.00	.00	.00	.00

DISTRIBUTION OF DESIGN MOMENTS AT SUPPORTS

COL NUM	CROSS SECTN	TOTAL MOMENT (ft-k)	TOTAL-VERT DIFFERENCE (ft-k) (%)	COLUMN STRIP MOMENT (ft-k) (%)	BEAM MOMENT (ft-k) (%)	MIDDLE STRIP MOMENT (ft-k) (%)
1	LEFT TOP	-6.7	.0 (0)	-6.5 (95)	.0 (0)	-.3 (4)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	399.1	.0 (0)	382.8 (95)	.0 (0)	16.3 (4)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
2	LEFT TOP	-775.0	.0 (0)	-581.2 (75)	.0 (0)	-193.7 (25)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	742.1	.0 (0)	556.6 (75)	.0 (0)	185.5 (25)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
3	LEFT TOP	-555.5	.0 (0)	-416.6 (75)	.0 (0)	-138.9 (25)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	487.3	.0 (0)	365.5 (75)	.0 (0)	121.8 (25)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
4	LEFT TOP	-487.3	.0 (0)	-365.5 (75)	.0 (0)	-121.8 (25)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	555.5	.0 (0)	416.6 (75)	.0 (0)	138.9 (25)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
5	LEFT TOP	-742.1	.0 (0)	-556.6 (75)	.0 (0)	-185.5 (25)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	775.0	.0 (0)	581.2 (75)	.0 (0)	193.7 (25)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
6	LEFT TOP	-399.1	.0 (0)	-382.8 (95)	.0 (0)	-16.3 (4)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	6.7	.0 (0)	6.5 (95)	.0 (0)	.3 (4)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)

DISTRIBUTION OF DESIGN MOMENTS IN SPANS

SPAN NUM	CROSS SECTN	TOTAL MOMENT (ft-k)	TOTAL-VERT DIFFERENCE (ft-k) (%)	COLUMN STRIP MOMENT (ft-k) (%)	BEAM MOMENT (ft-k) (%)	MIDDLE STRIP MOMENT (ft-k) (%)
2	14.25 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	374.3	.0 (0)	224.6 (60)	.0 (0)	149.7 (40)
	14.25 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	374.3	.0 (0)	224.6 (60)	.0 (0)	149.7 (40)
3	15.75 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	322.6	.0 (0)	193.5 (60)	.0 (0)	129.0 (40)
	15.75 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	322.6	.0 (0)	193.5 (60)	.0 (0)	129.0 (40)
4	11.88 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	210.7	.0 (0)	126.4 (60)	.0 (0)	84.3 (39)
	11.88 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	210.7	.0 (0)	126.4 (60)	.0 (0)	84.3 (40)
5	14.25 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	322.6	.0 (0)	193.5 (60)	.0 (0)	129.0 (40)
	14.25 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	322.6	.0 (0)	193.5 (60)	.0 (0)	129.0 (39)
6	15.75 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	374.3	.0 (0)	224.6 (60)	.0 (0)	149.7 (40)
	15.75 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	BOT	374.3	.0 (0)	224.6 (60)	.0 (0)	149.7 (40)

S H E A R A N A L Y S I S

NOTE--Allowable shear stress in slabs = 252.96 psi when ratio of col. dim. (long/short) is less than 2.0.

--Wide beam shear (see "CODE") is not computed, check manually.

--After the column numbers, C = Corner, E = Exterior, I = Interior.

D I R E C T S H E A R W I T H T R A N S F E R O F M O M E N T - - - - - A R O U N D C O L U M N - - - - -									
COL. NO.	ALLOW. STRESS (psi)	PATT NO.	REACTION (kips)	SHEAR STRESS (psi)	PATT NO.	REACTION (kips)	UNBAL. MOMENT (ft-k)	SHEAR TRANSFR (ft-k)	SHEAR STRESS (psi)
1E	252.96	4	148.2	116.20	4	148.2	422.6	159.8	250.55
2I	252.96	4	305.0	233.61	4	305.0	-38.5	-15.4	246.43
3I	252.96	4	254.5	194.92	4	254.5	-82.7	-33.1	222.46
4I	252.96	4	254.5	194.92	4	254.5	82.7	33.1	222.46
5I	252.96	4	305.0	233.61	4	305.0	38.5	15.4	246.43
6E	252.96	4	148.2	116.20	4	148.2	-422.6	-159.8	250.55

- - AROUND DROP/SOLID HEAD - -				
COLUMN NUMBER	ALLOW. STRESS (psi)	PATT NO.	REACTION (kips)	SHEAR STRESS (psi)
1E	185.35	4	124.5	62.93
2I	170.90	4	266.1	76.10
3I	172.82	4	218.9	65.29
4I	172.82	4	218.9	65.29
5I	170.90	4	266.1	76.10
6E	185.35	4	124.5	62.93

DESIGN RESULTS

NOTE--The schedule given below is a guide for proper reinforcement placement and is based on reasonable engineering judgement. Unusual boundary and/or loading conditions may require modification of this schedule.

NEGATIVE REINFORCEMENT

COLUMN NUMBER	COLUMN				STRIP				MIDDLE STRIP			
	NO	SIZE	LEFT	RIGHT	NO	SIZE	LEFT	RIGHT	NO	SIZE	LEFT	RIGHT
	(ft)		(ft)		(ft)		(ft)		(ft)		(ft)	
1	11	# 5	1.33	10.18	11	# 5	1.33	6.50	14	# 4	1.33	7.77
2	10	# 7	10.77	10.77	10	# 7	6.50	6.50	17	# 5	10.77	10.77
3	10	# 6	10.18	11.77	9	# 6	6.50	6.77	19	# 4	9.27	11.77
4	10	# 6	11.77	10.18	9	# 6	6.77	6.50	19	# 4	11.77	9.27
5	10	# 7	10.77	10.77	10	# 7	6.50	6.50	17	# 5	10.77	10.77
6	11	# 5	10.18	1.33	11	# 5	6.50	1.33	14	# 4	7.77	1.33

POSITIVE REINFORCEMENT

SPAN NUMBER	COLUMN				STRIP				MIDDLE STRIP			
	NO	SIZE	LENGTH	NO	SIZE	LENGTH	NO	SIZE	LENGTH	NO	SIZE	LENGTH
	(ft)		(ft)		(ft)		(ft)		(ft)		(ft)	
2	10	# 5	25.92	10	# 5	25.92	10	# 4	29.92	10	# 4	25.17
3	9	# 5	22.50	8	# 5	22.50	9	# 4	30.50	9	# 4	21.00
4	9	# 4	18.75	8	# 4	18.75	8	# 4	25.50	8	# 4	17.50
5	9	# 5	22.50	8	# 5	22.50	9	# 4	30.50	9	# 4	21.00
6	10	# 5	25.92	10	# 5	25.92	10	# 4	29.92	10	# 4	25.17

DEFLECTION ANALYSIS

NOTES--The deflections below must be combined with those of the analysis in the perpendicular direction. Consult users manual for method of combination and limitations.

--Spans 1 and 7 are cantilevers.

--Time-dependent deflections are in addition to those shown and must be computed as a multiplier of the dead load(DL) deflection. See "CODE" for range of multipliers.

--Deflections due to concentrated or partialloads may be larger at the point of application than those shown at the centerline. Deflections are computed as from an average uniform loading derived from the sum of all loads applied to the span.

--Modulus of elasticity of concrete, Ec = 3834. ksi

SPAN NUMBER	DEAD LOAD Ieff. (in^4)	COLUMN STRIP			MIDDLE STRIP		
		DEAD	LIVE	TOTAL	DEAD	LIVE	TOTAL
	(in)	(in)	(in)	(in)	(in)	(in)	(in)
1	48644.	-.015	-.011	-.026	-.015	-.011	-.026
2	32569.	.208	.262	.470	.108	.120	.229
3	31470.	.155	.236	.392	.078	.116	.194
4	33935.	.050	.083	.133	.011	.028	.039
5	31470.	.155	.236	.392	.078	.116	.194
6	32569.	.208	.262	.470	.108	.120	.229
7	48644.	-.015	-.011	-.026	-.015	-.011	-.026

Selected ADOSS Results, Alternative #2 Parking Flat Slab with Drops

```

FILE NAME           P:\PDROPSFA.ADS
PROJECT ID.         Parking Final Drops
SPAN ID.            BC
ENGINEER            Henry
DATE                02/09/06
TIME                10:51:12
UNITS               U.S. in-lb
CODE                ACI 318-89
SLAB SYSTEM         FLAT SLAB SYSTEM
FRAME LOCATION      INTERIOR
DESIGN METHOD        STRENGTH DESIGN
MOMENTS AND SHEARS NOT PROPORTIONED
    
```

NUMBER OF SPANS 9

SOLID HEAD DIMENSIONS : COMPUTED BY PROGRAM

```

CONCRETE FACTORS      SLABS          BEAMS          COLUMNS
DENSITY(pcf )        150.0          150.0          150.0
TYPE                  NORMAL WGT     NORMAL WGT     NORMAL WGT
f'c (ksi)             4.0            4.0            4.0
fct (psi)              423.7          423.7          423.7
fr (psi)               474.3          474.3          474.3
    
```

```

REINFORCEMENT DETAILS: NON-PRESTRESSED
YIELD STRENGTH Fy = 60.00 ksi
DISTANCE TO RF CENTER FROM TENSION FACE:
  AT SLAB TOP = 1.50 in  OUTER LAYER
  AT SLAB BOTTOM = 1.50 in  OUTER LAYER
MINIMUM FLEXURAL BAR SIZE:
  AT SLAB TOP = # 4
  AT SLAB BOTTOM = # 4
MINIMUM SPACING:
  IN SLAB = 6.00 in
    
```

SPAN/LOADING DATA

SPAN NUMBER	LENGTH		WIDTH		SLAB SYSTEM	DESIGN STRIP (ft)	COLUMN STRIP** (ft)	UNIFORM LOADS	
	L1 (ft)	Tslab (in)	LEFT (ft)	L2*** RIGHT (ft)				S. DL (psf)	LIVE (psf)
1*	1.3	11.0	15.0	11.3	2	26.3	.0	10.0	100.0
2	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
3	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
4	25.0	11.0	15.0	11.3	2	26.3	11.9	10.0	100.0
5	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
6	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
7	27.3	11.0	15.0	11.3	2	26.3	12.5	50.0	280.0
8	17.0	11.0	15.0	11.3	2	26.3	8.5	50.0	280.0
9*	1.3	11.0	15.0	11.3	2	26.3	.0	50.0	280.0

COLUMN/TORSIONAL DATA

COLUMN NUMBER	COLUMN ABOVE SLAB			COLUMN BELOW SLAB			CAPITAL**		COLUMN STRIP* (ft)	MIDDLE STRIP* (ft)
	C1 (in)	C2 (in)	HGT (ft)	C1 (in)	C2 (in)	HGT (ft)	EXTEN. (in)	DEPTH (in)		
1	20.0	24.0	13.3	20.0	30.0	13.3	.0	.0	13.1	13.1
2	20.0	20.0	13.3	24.0	20.0	13.3	.0	.0	13.1	13.1
3	20.0	20.0	13.3	24.0	20.0	13.3	.0	.0	11.9	14.4
4	20.0	20.0	13.3	24.0	20.0	13.3	.0	.0	11.9	14.4
5	20.0	20.0	13.3	24.0	20.0	13.3	.0	.0	13.1	13.1
6	20.0	24.0	13.3	24.0	24.0	13.3	.0	.0	12.5	13.8
7	.0	.0	13.3	24.0	24.0	13.3	.0	.0	8.5	17.8
8	.0	.0	13.3	20.0	20.0	13.3	.0	.0	8.5	17.8

Columns with zero "C2" are round columns.
* -Strip width used for negative flexure.
**-Capital extension distance measured from face of column.

COLUMN NUMBER	TRANSVERSE BEAM			DROP PANEL/SOLID HEAD				SUPPORT FIXITY* %
	WIDTH (in)	DEPTH (in)	ECCEN (in)	LEFT (ft)	RIGHT (ft)	WIDTH (ft)	THICK (in)	
1	20.0	20.0	.0	1.3	5.0	8.8	3.5	100%
2	.0	.0	.0	5.0	5.0	8.8	3.5	100%
3	.0	.0	.0	5.0	4.2	8.8	3.5	100%
4	.0	.0	.0	4.2	5.0	8.8	3.5	100%
5	.0	.0	.0	5.0	5.0	8.8	3.5	100%
6	24.0	32.0	.0	5.0	4.6	8.8	7.0	100%
7	.0	.0	.0	4.6	2.8	8.8	7.0	100%
8	20.0	20.0	.0	2.8	1.3	8.8	3.5	100%

* -Support fixity of 0% denotes pinned condition.
Support fixity of 999% denotes fixed end condition.

LATERAL LOAD/OUTPUT DATA

LATERAL LOADS ARE SPECIFIED AS BEING CAUSED BY WIND

JOINT NO.	SLAB MOMENTS		COLUMN MOMENTS	
	LEFT (ft-k)	RIGHT (ft-k)	ABOVE (ft-k)	BELOW (ft-k)
1	.00	-71.00	.00	.00
2	-71.00	-65.00	.00	.00
3	-63.00	-70.00	.00	.00
4	-70.00	-63.00	.00	.00
5	-65.00	-67.00	.00	.00
6	-66.00	-40.00	.00	.00
7	-26.00	-26.00	.00	.00
8	-32.00	.00	.00	.00

LATERAL LOADS DISTRIBUTED TO THE COLUMN AND MIDDLE STRIPS ACCORDING TO CODE DISTRIBUTION FACTORS.

DISTRIBUTION OF DESIGN MOMENTS AT SUPPORTS

COL NUM	CROSS SECTN	TOTAL MOMENT (ft-k)	TOTAL-VERT DIFFERENCE (ft-k) (%)	COLUMN STRIP MOMENT (ft-k) (%)	BEAM MOMENT (ft-k) (%)	MIDDLE STRIP MOMENT (ft-k) (%)
1	LEFT TOP	-6.8	.0 (0)	-6.6 (96)	.0 (0)	-.2 (3)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RIGHT TOP	377.3	.0 (0)	365.6 (96)	.0 (0)	11.6 (3)
	RIGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
2	LEFT TOP	-794.5	.0 (0)	-595.9 (74)	.0 (0)	-198.6 (25)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)

	RGHT	TOP	750.8	.0 (0)	563.1 (75)	.0 (0)	187.7 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
3	LEFT	TOP	-555.8	.0 (0)	-416.9 (75)	.0 (0)	-139.0 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT	TOP	478.8	.0 (0)	359.1 (75)	.0 (0)	119.7 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
4	LEFT	TOP	-504.9	.0 (0)	-378.7 (75)	.0 (0)	-126.2 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT	TOP	597.4	.0 (0)	448.0 (75)	.0 (0)	149.3 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
5	LEFT	TOP	-653.6	.0 (0)	-490.2 (75)	.0 (0)	-163.4 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT	TOP	603.5	.0 (0)	452.6 (75)	.0 (0)	150.9 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
6	LEFT	TOP	-889.6	.0 (0)	-667.2 (75)	.0 (0)	-222.4 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT	TOP	1099.9	.0 (0)	824.9 (75)	.0 (0)	275.0 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
7	LEFT	TOP	-1023.3	.0 (0)	-767.4 (75)	.0 (0)	-255.8 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT	TOP	851.3	.0 (0)	638.5 (75)	.0 (0)	212.8 (25)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)

DISTRIBUTION OF DESIGN MOMENTS AT SUPPORTS

COL NUM	CROSS SECTN	TOTAL MOMENT (ft-k)	TOTAL-VERT DIFFERENCE (ft-k) (%)	COLUMN STRIP MOMENT (ft-k) (%)	BEAM MOMENT (ft-k) (%)	MIDDLE STRIP MOMENT (ft-k) (%)	
8	LEFT	TOP	-41.7	.0 (0)	-40.4 (96)	.0 (0)	-1.3 (3)
		BOT	36.0	.0 (0)	34.9 (96)	.0 (0)	1.1 (3)
	RGHT	TOP	12.6	.0 (0)	12.2 (96)	.0 (0)	.4 (3)
		BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)

DISTRIBUTION OF DESIGN MOMENTS IN SPANS

SPAN NUM	CROSS SECTN	TOTAL MOMENT (ft-k)	TOTAL-VERT DIFFERENCE (ft-k) (%)	COLUMN STRIP MOMENT (ft-k) (%)	BEAM MOMENT (ft-k) (%)	MIDDLE STRIP MOMENT (ft-k) (%)
2	12.75	TOP	.0	.0 (0)	.0 (0)	.0 (0)
		BOT	410.8	.0 (0)	246.5 (60)	164.3 (40)
	12.75	TOP	.0	.0 (0)	.0 (0)	.0 (0)
		BOT	410.8	.0 (0)	246.5 (60)	164.3 (40)
3	15.75	TOP	.0	.0 (0)	.0 (0)	.0 (0)
		BOT	337.5	.0 (0)	202.5 (60)	135.0 (40)
	15.75	TOP	.0	.0 (0)	.0 (0)	.0 (0)
		BOT	337.5	.0 (0)	202.5 (60)	135.0 (40)
4	11.88	TOP	.0	.0 (0)	.0 (0)	.0 (0)
		BOT	215.9	.0 (0)	129.6 (60)	86.4 (40)
	11.88	TOP	.0	.0 (0)	.0 (0)	.0 (0)
		BOT	215.9	.0 (0)	129.6 (60)	86.4 (39)
5	14.25	TOP	.0	.0 (0)	.0 (0)	.0 (0)
		BOT	355.1	.0 (0)	213.0 (60)	142.0 (40)

DISTRIBUTION OF DESIGN MOMENTS IN SPANS

SPAN NUM	CROSS SECTN	TOTAL MOMENT (ft-k)	TOTAL-VERT DIFFERENCE (ft-k) (%)	COLUMN STRIP MOMENT (ft-k) (%)	BEAM MOMENT (ft-k) (%)	MIDDLE STRIP MOMENT (ft-k) (%)
	14.25 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	14.25 BOT	355.1	.0 (0)	213.0 (60)	.0 (0)	142.0 (40)
6	14.25 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	14.25 BOT	296.4	.0 (0)	177.8 (60)	.0 (0)	118.6 (39)
	14.25 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	14.25 BOT	296.4	.0 (0)	177.8 (60)	.0 (0)	118.6 (40)
7	14.35 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	14.35 BOT	502.4	.0 (0)	301.5 (60)	.0 (0)	201.0 (40)
	14.35 TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	14.35 BOT	502.4	.0 (0)	301.5 (60)	.0 (0)	201.0 (40)
8	9.77 TOP	-29.9	.0 (0)	-18.0 (60)	.0 (0)	-12.0 (39)
	9.77 BOT	257.9	.0 (0)	154.8 (60)	.0 (0)	103.2 (40)
	9.77 TOP	-29.9	.0 (0)	-18.0 (60)	.0 (0)	-12.0 (39)
	9.77 BOT	257.9	.0 (0)	154.8 (60)	.0 (0)	103.2 (40)

S H E A R A N A L Y S I S

NOTE--Allowable shear stress in slabs = 252.96 psi when ratio of col. dim. (long/short) is less than 2.0.

--Wide beam shear (see "CODE") is not computed, check manually.

--After the column numbers, C = Corner, E = Exterior, I = Interior.

D I R E C T		S H E A R		W I T H		T R A N S F E R		O F		M O M E N T	
C O L U M N		A R O U N D		C O L U M N		C O L U M N		C O L U M N		C O L U M N	
COL. NO.	ALLOW. STRESS (psi)	PATT NO.	REACTION (kips)	SHEAR STRESS (psi)	PATT NO.	REACTION (kips)	UNBAL. MOMENT (ft-k)	SHEAR TRANSFR (ft-k)	SHEAR TRANSFR (ft-k)	SHEAR STRESS (psi)	
1E	252.96	4	151.1	111.67	4	151.1	397.4	144.0	220.02	220.02	
2I	252.96	4	320.8	207.35	4	320.8	-52.3	-21.7	220.91	220.91	
3I	252.96	4	264.9	171.20	4	264.9	-97.1	-40.2	196.38	196.38	
4I	252.96	4	272.1	175.92	4	272.1	114.5	47.4	205.59	205.59	
5I	252.96	4	289.8	187.33	4	289.8	-71.4	-29.5	205.83	205.83	
6I	252.96	4	446.6	157.08	4	446.6	314.0	125.6	195.73	195.73	
7I	252.96	4	482.4	212.30	4	482.4	-213.3	-85.3	244.35	244.35	
8E	252.96	4	135.6	109.14	1	135.5	-52.1	-20.5	127.29	127.29	

- - AROUND DROP/SOLID HEAD - -

COLUMN NUMBER	ALLOW. STRESS (psi)	PATT NO.	REACTION (kips)	SHEAR STRESS (psi)
1E	191.80	4	127.5	57.23
2I	175.72	4	280.2	71.09
3I	177.83	4	227.7	60.25
4I	177.83	4	235.0	62.18
5I	175.72	4	249.2	63.23
6I	176.82	4	389.4	101.02
7I	182.98	4	426.1	124.07
8E	206.97	1	111.2	61.49

D E S I G N R E S U L T S

NOTE--The schedule given below is a guide for proper reinforcement placement and is based on reasonable engineering judgement. Unusual boundary and/or loading conditions may require modification of this schedule.

NEGATIVE REINFORCEMENT

COLUMN NUMBER	COLUMN LONG BARS				STRIP SHORT BARS				MIDDLE STRIP LONG BARS			
	NO	SIZE	LEFT (ft)	RIGHT (ft)	NO	SIZE	LEFT (ft)	RIGHT (ft)	NO	SIZE	LEFT (ft)	RIGHT (ft)
1	11	# 5	1.33	10.13	10	# 5	1.33	6.47	16	# 4	1.33	7.76
2	10	# 7	10.76	10.76	9	# 7	6.63	6.63	24	# 4	10.76	10.76
3	9	# 6	10.24	11.75	8	# 6	6.60	6.75	17	# 4	9.25	11.75
4	10	# 6	11.75	10.24	9	# 6	6.75	6.60	18	# 4	11.75	9.25
5	11	# 6	10.75	10.75	10	# 6	6.60	6.60	20	# 4	10.75	10.75
6	10	# 7	12.25	10.24	10	# 7	7.00	6.60	22	# 5	12.25	9.95
7	7	# 8	9.78	9.36	7	# 8	6.07	6.07	31	# 4	9.78	8.38
8**	7	# 4	7.03	1.33	7	# 4	4.06	1.33	21	# 4	6.90	1.33

** - Positive reinforcement required, design manually.

POSITIVE REINFORCEMENT

SPAN NUMBER	COLUMN LONG BARS			STRIP SHORT BARS			MIDDLE STRIP LONG BARS			STRIP SHORT BARS		
	NO	SIZE	LENGTH (ft)	NO	SIZE	LENGTH (ft)	NO	SIZE	LENGTH (ft)	NO	SIZE	LENGTH (ft)
2	10	# 5	25.92	10	# 5	25.92	10	# 4	29.92	10	# 4	25.17
3	8	# 5	22.50	8	# 5	22.50	8	# 4	30.50	8	# 4	21.00
4	8	# 4	18.75	8	# 4	18.75	9	# 4	25.50	8	# 4	17.50
5	9	# 5	22.50	8	# 5	22.50	9	# 4	30.50	8	# 4	21.00
6	11	# 4	22.50	11	# 4	22.50	8	# 4	30.50	8	# 4	21.00
7	9	# 6	21.22	8	# 6	21.22	12	# 4	27.83	12	# 4	19.13
8**	6	# 5	15.08	6	# 5	15.08	11	# 4	16.92	10	# 4	14.12

DEFLECTION ANALYSIS

NOTES--The deflections below must be combined with those of the analysis in the perpendicular direction. Consult users manual for method of combination and limitations.

--Spans 1 and 9 are cantilevers.

--Time-dependent deflections are in addition to those shown and must be computed as a multiplier of the dead load(DL) deflection. See "CODE" for range of multipliers.

--Deflections due to concentrated or partial loads may be larger at the point of application than those shown at the centerline. Deflections are computed as from an average uniform loading derived from the sum of all loads applied to the span.

--Modulus of elasticity of concrete, Ec = 3834. ksi

SPAN NUMBER	DEAD LOAD (in^4)	COLUMN DEFLECTION DUE TO:			STRIP DEFLECTION DUE TO:			MIDDLE STRIP DEFLECTION DUE TO:		
		DEAD (in)	LIVE (in)	TOTAL (in)	DEAD (in)	LIVE (in)	TOTAL (in)	DEAD (in)	LIVE (in)	TOTAL (in)
1	52778.	-.014	-.009	-.023	-.014	-.009	-.023			
2	40937.	.181	.186	.367	.095	.087	.182			
3	42290.	.125	.175	.301	.062	.086	.149			
4	43859.	.042	.052	.094	.009	.016	.025			
5	43859.	.132	.194	.326	.071	.101	.172			
6	52428.	.098	.121	.218	.044	.044	.088			
7	60998.	.089	.392	.481	.049	.207	.256			
8	52428.	.020	.039	.059	.002	.003	.005			
9	52778.	-.003	-.003	-.006	-.003	-.004	-.006			

Selected ADOSS Results, First Floor Slab with Superimposed Vault Load

PROJECT ID. Parking Final Drops

 SPAN ID. BC

 ENGINEER Henry
 DATE 02/09/06
 TIME 10:51:12
 UNITS U.S. in-lb
 CODE ACI 318-89
 SLAB SYSTEM FLAT SLAB SYSTEM
 FRAME LOCATION INTERIOR
 DESIGN METHOD STRENGTH DESIGN
 MOMENTS AND SHEARS NOT PROPORTIONED

NUMBER OF SPANS 9

SOLID HEAD DIMENSIONS : COMPUTED BY PROGRAM

CONCRETE FACTORS	SLABS	BEAMS	COLUMNS
DENSITY(pcf)	150.0	150.0	150.0
TYPE	NORMAL WGT	NORMAL WGT	NORMAL WGT
f'c (ksi)	4.0	4.0	4.0
fct (psi)	423.7	423.7	423.7
fr (psi)	474.3	474.3	474.3

REINFORCEMENT DETAILS: NON-PRESTRESSED
 YIELD STRENGTH Fy = 60.00 ksi
 DISTANCE TO RF CENTER FROM TENSION FACE:
 AT SLAB TOP = 1.50 in OUTER LAYER
 AT SLAB BOTTOM = 1.50 in OUTER LAYER
 MINIMUM FLEXURAL BAR SIZE:
 AT SLAB TOP = # 4
 AT SLAB BOTTOM = # 4
 MINIMUM SPACING:
 IN SLAB = 6.00 in

SPAN/LOADING DATA

SPAN NUMBER	LENGTH		WIDTH		SLAB SYSTEM	DESIGN STRIP (ft)	COLUMN STRIP** (ft)	UNIFORM LOADS	
	L1 (ft)	Tslab (in)	LEFT (ft)	RIGHT (ft)				S. DL (psf)	LIVE (psf)
1*	1.3	11.0	15.0	11.3	2	26.3	.0	10.0	100.0
2	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
3	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
4	25.0	11.0	15.0	11.3	2	26.3	11.9	10.0	100.0
5	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
6	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
7	27.3	11.0	15.0	11.3	2	26.3	12.5	50.0	280.0
8	17.0	11.0	15.0	11.3	2	26.3	8.5	50.0	280.0
9*	1.3	11.0	15.0	11.3	2	26.3	.0	50.0	280.0

* -Indicates cantilever span information.
 ** -Strip width used for positive flexure.
 ***-L2 widths are 1/2 dist. to transverse column.
 "E"-Indicates exterior strip.

PARTIAL LOADING DATA

SPAN No.	LOAD No.	TYPE	PARTIAL DEAD LOADS				LOAD No.	TYPE	PARTIAL LIVE LOADS				
			Wa	Wb	La	Lb			Wa	Wb	La	Lb	
1*													
2	1	UNIF	702.5	.0	20.0	30.0	1	UNIF	850.0	.0	20.0	30.0	
3	1	UNIF	702.5	.0	.0	10.0	1	UNIF	850.0	.0	.0	10.0	
4													
5													
6	1	UNIF	6111.0	.0	6.7	15.7							
7													
8													
9*													

DESIGN RESULTS

NOTE--The schedule given below is a guide for proper reinforcement placement and is based on reasonable engineering judgement. Unusual boundary and/or loading conditions may require modification of this schedule.

NEGATIVE REINFORCEMENT

COLUMN NUMBER	* NO	* LONG BARS		* RIGHT (ft)	* STRIP SHORT BARS	* NO	* SHORT BARS		* RIGHT (ft)	* MIDDLE LONG BARS	* NO	* LONG BARS		* RIGHT (ft)
		SIZE	LEFT (ft)				SIZE	LEFT (ft)				SIZE	RIGHT (ft)	
1**	10	# 6	1.33	10.13	9	# 6	1.33	6.47	16	# 4	1.33	9.26		
2	10	# 7	12.26	12.26	10	# 7	7.01	7.01	17	# 5	12.26	12.26		
3**	10	# 6	10.75	11.75	9	# 6	6.60	6.75	19	# 4	10.75	11.75		
4**	10	# 6	11.75	10.75	9	# 6	6.75	6.60	18	# 4	11.75	10.75		
5	10	# 7	12.25	10.24	9	# 7	7.00	6.60	16	# 5	12.25	9.25		
6	11	# 7	12.25	11.32	10	# 7	7.00	6.60	23	# 5	12.25	11.32		
7	7	# 8	9.36	9.36	7	# 8	6.07	6.07	30	# 4	8.42	9.23		
8**	7	# 4	7.03	1.33	7	# 4	4.06	1.33	21	# 4	6.90	1.33		

** - Positive reinforcement required, design manually.

POSITIVE REINFORCEMENT

SPAN NUMBER	* NO	* LONG BARS		* LENGTH (ft)	* STRIP SHORT BARS	* NO	* SHORT BARS		* LENGTH (ft)	* MIDDLE LONG BARS	* NO	* LONG BARS		* LENGTH (ft)
		SIZE	LENGTH (ft)				SIZE	LENGTH (ft)				SIZE	LENGTH (ft)	
2	10	# 5	25.92	10	# 5	25.92	10	# 4	29.92	10	# 4	25.17		
3	9	# 5	22.50	8	# 5	22.50	9	# 4	30.50	8	# 4	21.00		
4	8	# 4	18.75	8	# 4	18.75	9	# 4	25.50	8	# 4	17.50		
5	12	# 4	22.50	12	# 4	22.50	8	# 4	30.50	8	# 4	21.00		
6	9	# 6	23.00	8	# 6	23.00	12	# 4	30.50	12	# 4	21.00		
7	9	# 6	21.22	8	# 6	21.22	12	# 4	27.83	12	# 4	19.13		
8**	7	# 5	15.08	6	# 5	15.08	11	# 4	16.92	10	# 4	14.12		

** - Negative reinforcement required, design manually.

DEFLECTION ANALYSIS

NOTES--The deflections below must be combined with those of the analysis in the perpendicular direction. Consult users manual for method of combination and limitations.

--Spans 1 and 9 are cantilevers.

--Time-dependent deflections are in addition to those shown and must be computed as a multiplier of the dead load(DL) deflection. See "CODE" for range of multipliers.

--Deflections due to concentrated or partial loads may be larger at the point of application than those shown at the centerline. Deflections are computed as from an average uniform loading derived from the sum of all loads applied to the span.

--Modulus of elasticity of concrete, $E_c = 3834$. ksi

SPAN NUMBER	DEAD LOAD Ieff. (in ⁴)	C O L U M N S T R I P			M I D D L E S T R I P		
		DEAD (in)	LIVE (in)	TOTAL (in)	DEAD (in)	LIVE (in)	TOTAL (in)
1	52778.	-.014	-.009	-.023	-.014	-.009	-.023
2	39764.	.194	.230	.424	.100	.104	.204
3	40837.	.136	.193	.329	.067	.095	.162
4	43859.	.046	.050	.096	.013	.015	.027
5	39442.	.115	.178	.293	.047	.094	.142
6	41495.	.219	.144	.363	.124	.053	.177
7	60998.	.070	.370	.440	.030	.199	.229
8	52428.	.023	.038	.061	.005	.002	.007
9	52778.	-.003	-.003	-.007	-.003	-.003	-.007

Selected ADOSS Results, Torsion Beam between Office Floor and Parking Deck

FILE NAME P:\PDROPSFA.ADS
 PROJECT ID. Parking Final Drops
 SPAN ID. BC
 ENGINEER Henry
 UNITS U.S. in-lb
 CODE ACI 318-89
 SLAB SYSTEM FLAT SLAB SYSTEM
 FRAME LOCATION INTERIOR
 DESIGN METHOD STRENGTH DESIGN
 MOMENTS AND SHEARS NOT PROPORTIONED
 NUMBER OF SPANS 9

CONCRETE FACTORS SLABS BEAMS COLUMNS
 DENSITY(pcf) 150.0 150.0 150.0
 TYPE NORMAL WGT NORMAL WGT NORMAL WGT
 f'c (ksi) 4.0 4.0 4.0
 fct (psi) 423.7 423.7 423.7
 fr (psi) 474.3 474.3 474.3

REINFORCEMENT DETAILS: NON-PRESTRESSED
 YIELD STRENGTH F_y = 60.00 ksi
 DISTANCE TO RF CENTER FROM TENSION FACE:
 AT SLAB TOP = 1.50 in OUTER LAYER
 AT SLAB BOTTOM = 1.50 in OUTER LAYER
 MINIMUM FLEXURAL BAR SIZE:
 AT SLAB TOP = # 4
 AT SLAB BOTTOM = # 4
 MINIMUM SPACING:
 IN SLAB = 6.00

SPAN/LOADING DATA

SPAN NUMBER	LENGTH L1 (ft)	Tslab (in)	WIDTH L2***		SLAB SYSTEM	DESIGN STRIP (ft)	COLUMN STRIP** (ft)	UNIFORM LOADS	
			LEFT (ft)	RIGHT (ft)				S. DL (psf)	LIVE (psf)
1*	1.3	11.0	15.0	11.3	2	26.3	.0	10.0	100.0
2	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
3	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
4	25.0	11.0	15.0	11.3	2	26.3	11.9	10.0	100.0
5	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
6	30.0	11.0	15.0	11.3	2	26.3	13.1	10.0	100.0
7	27.3	11.0	15.0	11.3	2	26.3	12.5	50.0	280.0
8	17.0	11.0	15.0	11.3	2	26.3	8.5	50.0	280.0
9*	1.3	11.0	15.0	11.3	2	26.3	.0	50.0	280.0

TRANSVERSE BEAM SHEAR AND TORSION REQUIREMENTS (kips, ft-k, SQ.in, /,in.)

BEAM No.	PATT. NO.	LEFT SIDE							
		Vu@d SHEAR	Vc@d SHEAR	Tu@d TORSION	Tc@d TORSION	Av/s @d	At/s @d	Atot/s @d	Al @d
1	4	49.5	15.5	157.9	49.3	.039	.101	.241	6.68
2	*			Transverse beam not specified					**
3	*			Transverse beam not specified					**
4	*			Transverse beam not specified					**
5	*			Transverse beam not specified					**
6	2	90.1	54.7	148.1	89.9	.028	.026	.080	2.53
7	*			Transverse beam not specified					**
8	3	68.1	41.5	39.8	24.2	.035	.017	.068	1.11

BEAM No.	PATT. NO.	RIGHT SIDE		RIGHT SIDE		Av/s @d	At/s @d	Atot/s @d	Al @d
		Vu@d SHEAR	Vc@d SHEAR	Tu@d TORSION	Tc@d TORSION				
1	4	28.2	6.8	213.3	51.6	.024	.148	.319	9.76
2	* *			Transverse beam not specified					* *
3	* *			Transverse beam not specified					* *
4	* *			Transverse beam not specified					* *
5	* *			Transverse beam not specified					* *
6	2	49.0	27.4	190.4	106.4	.020*	.036	.088	3.53
7	* *			Transverse beam not specified					* *
8	3	40.2	29.1	56.4	40.8	.017*	.019	.054	1.40

DISTRIBUTION OF DESIGN MOMENTS AT SUPPORTS

COL NUM	CROSS SECTN	TOTAL MOMENT (ft-k)	TOTAL-VERT DIFFERENCE (ft-k) (%)	COLUMN STRIP MOMENT (ft-k) (%)	BEAM MOMENT (ft-k) (%)	MIDDLE STRIP MOMENT (ft-k) (%)
1	LEFT TOP	-13.6	.0 (0)	-2.0 (14)	-11.1 (81)	-.6 (4)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	104.2	.0 (0)	15.0 (14)	85.0 (81)	4.3 (4)
	RGHT BOT	-45.2	.0 (0)	-6.5 (14)	-36.9 (81)	-1.8 (4)
2	LEFT TOP	-1203.3	.0 (0)	-112.2 (9)	-635.6 (52)	-455.5 (37)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	1285.3	.0 (0)	146.5 (11)	830.0 (64)	308.9 (24)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
3	LEFT TOP	-1262.2	.0 (0)	-143.8 (11)	-815.1 (64)	-303.3 (24)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	1179.3	.0 (0)	116.5 (9)	660.3 (55)	402.5 (34)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
4	LEFT TOP	-534.9	.0 (0)	-52.9 (9)	-299.5 (55)	-182.6 (34)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	520.2	.0 (0)	390.2 (75)	.0 (0)	130.1 (25)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
5	LEFT TOP	-523.0	.0 (0)	-392.2 (75)	.0 (0)	-130.7 (25)
	LEFT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
	RGHT TOP	523.5	.0 (0)	392.6 (75)	.0 (0)	130.9 (25)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
6	LEFT TOP	-34.2	.0 (0)	-33.8 (99)	.0 (0)	-.3 (0)
	LEFT BOT	1.0	.0 (0)	1.0 (99)	.0 (0)	.0 (0)
	RGHT TOP	12.5	.0 (0)	12.4 (99)	.0 (0)	.1 (0)
	RGHT BOT	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)

FILE NAME P:\PDROPSF9.ADS
CODE ACI 318-89

SLAB SYSTEM BEAM-SUPPORTED SLAB
FRAME LOCATION INTERIOR

DESIGN METHOD STRENGTH DESIGN
MOMENTS AND SHEARS NOT PROPORTIONED

NUMBER OF SPANS 7

CONCRETE FACTORS	SLABS	BEAMS	COLUMNS
DENSITY(pcf)	150.0	150.0	150.0
TYPE	NORMAL WGT	NORMAL WGT	NORMAL WGT
f'c (ksi)	4.0	4.0	4.0
fct (psi)	423.7	423.7	423.7
fr (psi)	474.3	474.3	474.3

REINFORCEMENT DETAILS: NON-PRESTRESSED
YIELD STRENGTH (flexural) Fy = 60.00 ksi
YIELD STRENGTH (stirrups) Fyv = 60.00 ksi

DISTANCE TO RF CENTER FROM TENSION FACE:
 AT SLAB TOP = 1.50 in OUTER LAYER
 AT SLAB BOTTOM = 1.50 in OUTER LAYER
 AT BEAM TOP = 1.50 in OUTER LAYER
 AT BEAM BOTTOM = 1.50 in
 FLEXURAL BAR SIZES: MINIMUM | MAXIMUM
 AT SLAB TOP = # 4
 AT SLAB BOTTOM = # 4
 AT BEAM TOP = # 4 #14
 IN BEAM BOTTOM = # 4 #14
 MINIMUM SPACING:
 IN SLAB = 6.00 in
 IN BEAM = 1.00 in

SPAN/LOADING DATA

SPAN NUMBER	LENGTH L1 (ft)	Tslab (in)	WIDTH		L2*** (ft)	SLAB SYSTEM	DESIGN STRIP (ft)	COLUMN STRIP** (ft)	UNIFORM LOADS	
			LEFT (ft)	RIGHT (ft)					S. DL (psf)	LIVE (psf)
1*	1.3	11.0	15.0	15.0	4	30.0	.0	60.0	250.0	
2	21.0	11.0	15.0	15.0	4	30.0	8.5	60.0	250.0	
3	31.0	11.0	15.0	15.0	4	30.0	13.0	60.0	250.0	
4	23.0	11.0	15.0	15.0	4	30.0	9.5	60.0	250.0	
5	20.0	11.0	15.0	15.0	4	30.0	10.0	60.0	250.0	
6	17.5	11.0	15.0	15.0	4	30.0	8.8	60.0	250.0	
7*	1.3	11.0	15.0	15.0	4	30.0	.0	60.0	250.0	

BEAMS ALONG SPAN DATA

SPAN NUMBER	BEAM WIDTH (in)	BEAM DEPTHS			HAUNCH LENGTHS	
		LEFT (in)	CENTER (in)	RIGHT (in)	LEFT (ft)	RIGHT (ft)
1	24.0	32.0	32.0	32.0	.0	.0
2	24.0	32.0	32.0	32.0	.0	.0
3	24.0	32.0	32.0	32.0	.0	.0
4	24.0	32.0	32.0	32.0	.0	.0
5	.0	.0	.0	.0	.0	.0
6	.0	.0	.0	.0	.0	.0
7	.0	.0	.0	.0	.0	.0

DISTRIBUTION OF DESIGN MOMENTS IN SPANS

SPAN NUM	CROSS SECTN		TOTAL MOMENT	TOTAL-VERT DIFFERENCE	COLUMN STRIP MOMENT	BEAM STRIP MOMENT	MIDDLE STRIP MOMENT
			(ft-k)	(ft-k) (%)	(ft-k) (%)	(ft-k) (%)	(ft-k) (%)
2	8.93	TOP	-11.1	.0 (0)	-1.0 (9)	-5.9 (52)	-4.2 (37)
		BOT	512.1	.0 (0)	47.7 (9)	270.5 (52)	193.9 (37)
3	16.27	TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
		BOT	1016.3	.0 (0)	115.8 (11)	656.3 (64)	244.3 (24)
4	12.07	TOP	-96.1	.0 (0)	-9.5 (9)	-53.8 (55)	-32.8 (34)
		BOT	575.5	.0 (0)	56.9 (9)	322.2 (55)	196.4 (34)
5	10.50	TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
		BOT	357.6	.0 (0)	214.6 (60)	.0 (0)	143.1 (40)
6	10.06	TOP	.0	.0 (0)	.0 (0)	.0 (0)	.0 (0)
		BOT	384.4	.0 (0)	230.6 (60)	.0 (0)	153.7 (39)

Sample Spreadsheet Used to Size Torsion Beam

Tu= 151
Vu= 96

BEAM DIMENSIONS

SIZE
OK?

H= 24 0.453012 <? 0.474
B= 26.5 assumes f'c=4000 psi

MAX SPACING

Acp= 636
Pcp= 101 10.875
Aoh= 471.5 10.25
Ao= 400.775 24
ph= 87 final: 10

TORSION

SHEAR

At= 0.050236 Vc= 51.53722
Av= 0.048198

LONGITUDINAL REINFORCEMENT

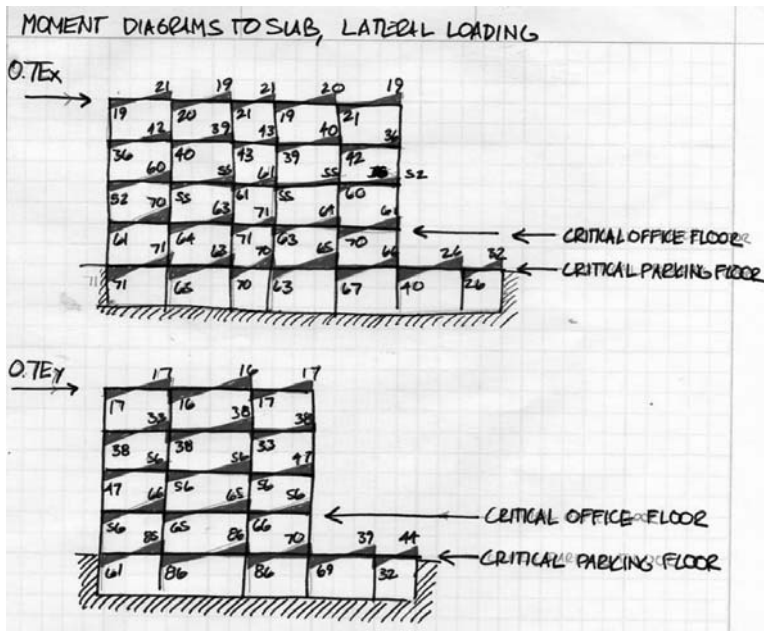
Al= 0.437053
Al= 2.914961

FLEXURAL REINFORCEMENT

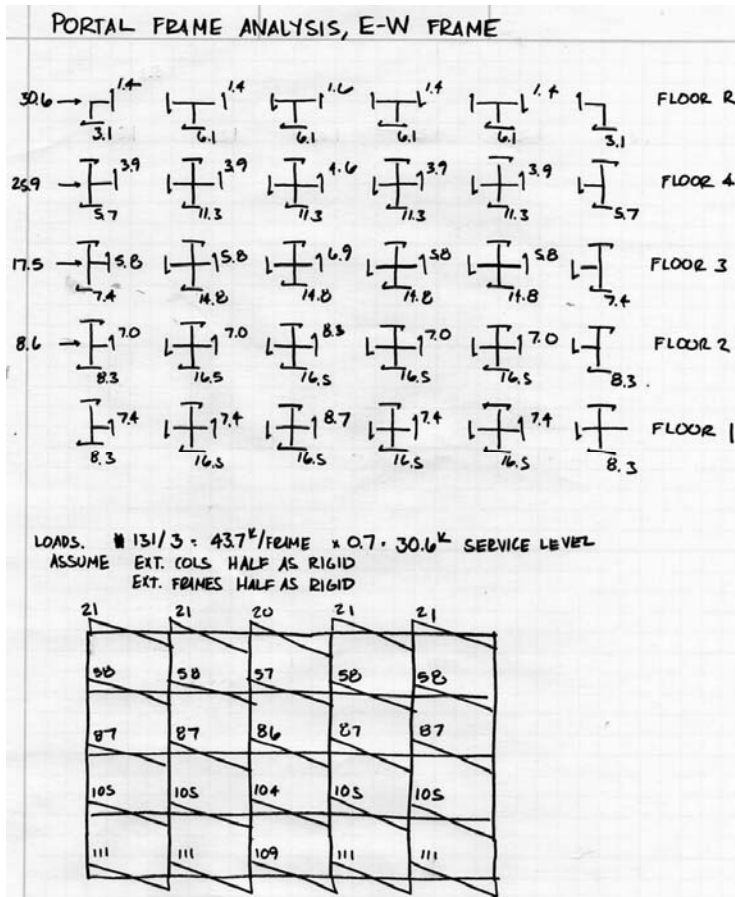
Mmax= 769.1 steel des 8#10
As= 8.929525 AsFinal= 10
phiMn= 840.1665 a= 6.659267

steel des At+Av #4 stirrups @ 10"
steel des long 10-#5 distributed upsize 1,4,5,8 bottom reinf to 11

Slab Moments from Lateral Loads Derived from ETABS



Slab Moments Determined from Portal Frame Analysis



SQUARE TIED COLUMNS 22" X 22"																	
Short columns; no sideways																	
Bars symmetrical in 4 faces																	
BARS	RHO	Max Cap		0% f _y		25% f _y		50% f _y		100% f _y		f _c = 4,000 psi φ M in inch-kips		f _y = 60,000 psi φ P in kips		Zero Axial Load φ H	
		φH	φP	φH	φP	φH	φP	φH	φP	φH	φP	φH	φP	φH	φP	φH	φP
4-#10	1.05	2435	1083	3211	968	3992	814	4430	692	4890	507	3532	194	2535			
4-#11	1.29	2500	1119	3430	982	4231	823	4699	697	5236	501	3882	194	3038			
4-#14	1.86	2671	1207	3891	1031	4789	858	5360	718	6114	494	4765	194	4235			
4-#18	3.31	3044	1429	4998	1157	6136	949	6963	773	8248	478	6910	194	7112			
8-#8	1.31	2374	1122	3133	1006	3919	843	4355	714	4803	516	3887	194	3131			
8-#9	1.65	2455	1175	3356	1038	4190	867	4676	728	5229	514	4407	194	3886			
8-#10	2.10	2556	1244	3638	1080	4532	897	5083	747	5771	511	5012	194	4835			
8-#11	2.58	2641	1317	3942	1118	4880	924	5484	763	6293	504	5569	194	5772			
8-#14	3.72	2880	1492	4618	1226	5708	1002	6472	811	7611	497	6969	194	8017			
8-#18	6.61	3437	1936	6245	1500	7714	1201	8871	934	10618	476	10253	194	12476			
12-#10	3.15	2799	1405	4192	1191	5222	980	5891	808	6848	510	6326	194	6633			
12-#11	3.87	2938	1515	4605	1254	5705	1025	6450	836	7583	500	7188	194	7998			
12-#14	5.58	3298	1777	5557	1421	6875	1147	7839	916	9436	489	9173	194	10859			
16-#10	4.20	3050	1566	4779	1303	5923	1070	6749	863	7988	514	7627	194	8755			
16-#11	5.16	3223	1713	5306	1391	6543	1134	7477	902	8947	503	8693	194	10231			
20-#10	5.25	3262	1727	5372	1414	6659	1153	7618	924	9143	512	8912	194	10541			
SQUARE TIED COLUMNS 24" X 24"																	
4-#11	1.08	3180	1294	4199	1158	5228	973	5810	827	6432	604	4668	230	3394			
4-#14	1.56	3381	1382	4723	1205	5859	1007	6556	847	7422	597	5663	230	4746			
4-#18	2.78	3829	1604	5983	1330	7390	1097	8374	902	9841	581	8096	230	8010			
8-#8	1.10	3032	1297	3853	1183	4870	994	5416	846	5939	622	4664	230	3491			
8-#9	1.39	3126	1350	4106	1215	5174	1018	5776	860	6416	620	5266	230	4341			
8-#10	1.76	3243	1419	4424	1257	5559	1048	6233	879	7023	617	6000	230	5412			
8-#11	2.17	3344	1492	4773	1295	5955	1075	6689	895	7616	610	6649	230	6481			
8-#14	3.13	3625	1667	5339	1402	6891	1154	7905	944	9103	603	8261	230	9039			
8-#18	5.56	4267	2111	7389	1677	9168	1354	10526	1088	12737	585	12056	230	14554			
12-#10	2.65	3522	1580	5045	1369	6332	1133	7138	941	8231	617	7433	230	7803			
12-#11	3.25	3673	1690	5319	1432	6863	1178	7775	970	9066	608	8420	230	9143			
12-#14	4.69	4100	1952	6596	1599	8207	1300	9345	1051	11159	598	10835	230	12407			
16-#10	3.53	3796	1741	5703	1462	7118	1223	8101	998	9510	623	8927	230	9907			
16-#11	4.33	4009	1888	6308	1569	7826	1288	8931	1037	10600	613	10160	230	11732			
16-#14	6.25	4544	2238	7714	1796	9543	1458	10982	1147	13333	604	13189	230	15832			
20-#10	4.41	4049	1902	6360	1592	7945	1307	9076	1060	10895	622	10387	230	12008			
20-#11	5.42	4297	2086	7104	1705	8817	1390	10100	1112	12153	611	11873	230	14121			

(1) "0% f_y" indicates zero tension in bars on the tension side, "50% f_y" indicates 50% f_y stress in bars on the tension side, and "100% f_y" indicates 100% f_y stress (i.e., balance point) in bars on the tension side.

Sample Footing Spreadsheet

LOADING

DL=	54	q(given)=	5000
LL=	49		
Pcn=	103	Pce=	54
TL=	143.2		

COLUMN

Cdx(big)=	20	Afootingexst=	36
Cdy(sm)=	20		
Ratio=	1		

FSexst= 3.333333 <2? *CHANGED FS TO 3.5

FOOTING SIZE

B=	8.577379	Bfinal=	9
L=	8.577379	Lfinal=	9

DIRECT SHEAR

q= 12.27709 <164? $\phi^4 * (3000\text{psi})^{0.5}$

TWO WAY SHEAR

328+q=	340.2771	d=	7.441323
Cdx+Cdy=	40	dfinalL=	8.625
656+q=	668.2771	dfinalS=	7.875
BL=	11664	hfinal=	12
CdxCdy=	400		

WIDE BEAM SHEAR

Q=	1.767901		
$\phi VnL=$	8.503388 >?	VL=	5.211626
$\phi VnS=$	7.763963 >?	VS=	5.322119

REINFORCEMENT

AsL=	0.436482 <?	AsLfinal=	0.44
aL=	0.862745		
MuL=	14.73865 <?	$\phi Mn=$	16.22338