



SENIOR THESIS SPRING 2006 EARTH AND ENGINEERING SCIENCES BUILDING UNIVERSITY PARK, PA

JUSTIN STRAUSER STRUCTURAL OPTION



Presentation Outline

>Introduction

>Building Statistics

Structural System
Problem Statement
Proposed Solution
Summary of Design
Effects of Design on Breadth Areas
Conclusions



<u>Introduction</u>

≻Location

- Design Team
 - •Owner
 - •Architect
 - •Engineer
 - Contractor
- Construction Dates
- ≻State Funding





Building Statistics

106,000 Square Feet Building Height : **66'-4''** Mean Roof Height : **61'-4''** Floor to Floor Height:

- •1st Floor : 17'-4"
- •2nd 4th Floors : 14' 8"

Educational and Laboratory Facility

Special Features:

- •Cray Supercomputer
- Automated Fire Door
- •Lobby Space
- Auditorium Space





Structural System

Gravity System

- •A36 Grade Steel Frame(50 ksi in specific locations)
- •Fully Composite Slab on Deck
 - 20 gauge galvanized steel deck 3" deep with 3 ¼" lightweight concrete topping

Lateral System

- Concrete Shear Walls
 - 12" thick reinforced concrete shear walls, #5 @ 8" EW EF
- Location of Walls and Connection Methods
- Moment Frame



Problem Statement

Nechanical Equipment Location
Height Restrictions
Architectural Appearance
Lateral Considerations
Full Basement Added to Accommodate Equipment
Delayed Construction
Increased Cost



Proposed Solution

- •Eliminate the Basement Space
- •Reduce Mean Roof Height
 - Change to a more shallow floor system
 - Increase steel strength to 50 ksi steel
 - Maintain same floor to ceiling height
- •Place Air Handling Units on the Roof
- •Increase the Height of the Parapet Walls to Mask the Units
- •Alter the façade as needed



Summary of Design

•Pre-stressed Hollow Core Plank design for 10' to 20' spans

(Nitterhouse Concrete Products)

- Steel Design by RAM Structural
- •Lateral Analysis in concordance with ASCE 7-05

•Parapet Design in concordance with Masonry Design Guide





Hollow Core Plank

- •Design Tables
- Loads Applied
- Connection Method



| STRAND PATTERN | | | | SPAN (FEET) | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 1 B | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 3D | 31 | 32 | |
| Flexure | 4 | _ | 1/ | 2°ø | 610 | 550 | 499 | 457 | 399 | 341 | 294 | 255 | 222 | 195 | 171 | 151 | 133 | 117 | 103 | 92 | 82 | 72 | 66 | 56 | 49 | 43 | \sim |
| Shear | 4 | _ | 1/ | 2 Ø | 441 | 393 | i 354 | 321 | 294 | 270 | Z49 | 231 | 215 | 201 | 188 | 177 | 160 | 145 | 132 | 120 | 110 | 101 | 95 | 90 | 82 | 75 | \sim |
| Flexure | 6 | - | 1/ | 2 0 | 885 | 800 | 726 | 667 | 586 | 509 | 437 | 382 | 334 | 296 | 263 | 234 | 208 | 167 | 168 | 151 | 1.36 | 122 | 111 | 100 | 90 | B1 | 73 |
| Shear | б | _ | 1/ | ΖØ | 459 | 411 | 37D | 337 | 3DB | 283 | 26Z | 243 | 228 | 211 | 197 | 185 | 174 | 184 | 155 | 147 | 139 | 131 | 120 | 111 | 102 | 94 | 87 |
| NITTERHOUSE <u>CONCRETE</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUCTS</u> <u>PRODUC</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | |



<u>Steel Frame</u>

•General Changes Made to Steel Frame

•Loads Applied (specifically at roof level)

•Summary of Differences between New and Existing

| Summary of Beam and Girder Sizes Typical to Each Story | | | | | | | | | | | |
|--------------------------------------------------------|-------|--------|--------|--------|--------|--|--|--|--|--|--|
| | Story | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | Roof | | | | | | |
| Beam 1 | X | W18x35 | W18x40 | W18x40 | W21x44 | | | | | | |
| Beam 2 | Х | W18x40 | W21x44 | W21x44 | W21x44 | | | | | | |
| Beam 3 | Х | W21x48 | W21x48 | W21x48 | W21x44 | | | | | | |
| Girder | X | W24x55 | W24x55 | W24x55 | W24x55 | | | | | | |
| Column 1 | X | W10x49 | W10x49 | W10x33 | W10x33 | | | | | | |
| Column 2 | X | W12x58 | W12x58 | W12x40 | W12x40 | | | | | | |





Lateral System

- •Lateral Analysis Performed According to ASCE 7-05
- •Higher Shear Forces Found at Roof Level
- •Shear Walls analyzed to be reused
- •Shear Walls found Acceptable
- •Moment Frame in Southern Wall left as well
- Problems at Roof level



Parapet Design

- •Design Height : 8'-6"
- Analyzed as a Cantilevered Wall
- •8" CMU fully grouted
- •Found to need #6 @ 40" to resist wind loading
- Seismic Loads at roof level



Façade Al terations





Effects of Design on Breadth Areas

- •New AHU's needed
- •Placement of Equipment
- Impact on Ductwork
- •Cost

| AHU | Supply Air (cfm) | Total Cooling Capacity (MBH) | Ton |
|-----|---------------------|---------------------------------------|-----|
| 1 | 30,245 | 1741 | 145 |
| 2 | 21,990 | 1266 | 106 |
| 3 | 16,895 | 1219 | 102 |
| 4 | 18,960 | 1093 | 91 |
| 5 | 14,255 | 997 | 83 |





Selection Guide

| QUICK | QUICK SELECT TOOL – OPTIMAL SIZES | | | | | | | | | |
|-------|-----------------------------------|-----|--------------|----------------------|-------------------------|------------------|------------------|--------------------|--|--|
| CFM | н | w | COIL AREA | AF SQ. FT AREA | RF/FF SQ. FT AREA | MAX FC FAN | MAX AF FAN | MAX Swsi Fan | | |
| 900 | 27 | 27 | 1.8 | 4.4 | - | 7x7 | - | - | | |
| 1500 | 30 | 33 | 2.9 | 4.0 | 3.3 | 9x9 | - | - | | |
| 2000 | 36 | 33 | 4.0 | 8.0 | 4.0 | 12x9 | - | - | | |
| 2500 | 33 | 45 | 5.2 | 8.9 | 6.D | 10x10 | - | 12 | | |
| 3500 | 36 | 48 | 6.9 | 11.1 | 6.D | 12x12 | 12 | 12 | | |
| 4500 | 36 | 60 | 9.2 | 16.0 | 8.D | 12x12 | 12 | 14 | | |
| 5500 | 42 | 60 | 10.8 | 16.0 | 10.7 | 15x15 | 15 | 18 | | |
| 6000 | 42 | 66 | 12.2 | 18.7 | 10.7 | 15x15 | 15 | 18 | | |
| 7000 | 42 | 72 | 13.5 | 26.7 | 13.3 | 15x15 | 15 | 18 | | |
| 8000 | 48 | 72 | 15.6 | 26.7 | 15.0 | 18x18 | 18 | 25 | | |
| 9000 | 48 | 78 | 17.9 | 35.6 | 15.0 | 18x18 | 18 | 25 | | |
| 10000 | 51 | 78 | 19.5 | 35.6 | 18.9 | 20x20 | 20 | 25 | | |
| 11500 | 57 | 78 | 21.8 | 35.6 | 22.7 | 22x22 | 22 | 28 | | |
| 13500 | 60 | 84 | 26.5 | 36.0 | 24.0 | 22x22 | 22 | 28 | | |
| 16500 | 66 | 96 | 32.1 | 53.3 | 31.1 | 28x28 | 28 | 35 | | |
| 19500 | 66 | 114 | 39.0 | 57.8 | 38.9 | 28x28 | 28 | 35 | | |
| 22500 | 72 | 120 | 45.0 | 62.2 | 45.0 | 32x32 | 32 | 39 | | |
| 26500 | 78 | 126 | 53.4 | 80.0 | 48.3 | 32x32 | 32 | 44 | | |
| 30500 | 90 | 120 | 60.0 | 93.3 | 60.0 | 36x36 | 36 | 49 | | |
| 34500 | 96 | 125 | 67.3 | 106.7 | 64.4 | 40x40 | 40 | 49 | | |
| 38500 | 108 | 125 | 75.2 | 106.7 | 77.3 | 40x40 | 40 | 49 | | |
| 42500 | 108 | 138 | 83.1 | 110.0 | 85.3 | 40x40 | 40 | 49 | | |
| 46500 | 114 | 144 | 94.0 | 151.1 | 91.7 | 40x40 | 40 | 49 | | |
| 50500 | 120 | 144 | 98.5 | 151.1 | 91.7 | 40x40 | 40 | 49 | | |
| 51500 | 126 | 144 | 103.0 | 151.1 | 104.7 | 40x40 | 40 | 49 | | |

State College Wind Rose





Cost Analysis

| Eliminated Items | | |
|--------------------|-------------|-------------|
| Steel | 1,346 LF | \$34,589 |
| Excavation-Backhoe | 7,826 CY | \$10,956 |
| Excavation-Hauling | 7,827 CY | \$17,295 |
| Slab on Deck | 70,308 SF | \$735,737 |
| Roof Deck | 19,034 SF | \$22,269 |
| 12" CMU wall | 8,704 SF | \$49,265 |
| Original Steel | 12,570.5 LF | \$283,018 |
| | | \$1,153,129 |
| | | |
| | Net = | \$216.848 |

| Added Items | | |
|------------------|-------------|--|
| Slab on Grade | 13,206.5 SF | |
| Hollowcore Plank | 76,136 SF | |
| 8" CMU Wall | 2,952 SF | |
| Steel | 10,135.5 LF | |
| | | |
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| | | |

(According to R.S. Means and Costworks)



Concl usi ons

- •Solution is feasible
- •May not have been the most practical
- •Created additional problems to fix the original problem
- •Overall an educational experience



