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Structural Option
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Wellington at Hershey's Mill
West Chester, Pennsylvania
10/31/2005

Structural Technical Report 2

Executive Summary

Wellington at Hershey's Mill is a retirement community located in West Chester, Pennsylvania. Consisting of 370,000 square feet and a total of 5 stories, Wellington offers 197 independent living apartments on the top three levels, a garage level directly below them, and a section with a lobby and offices for businesses within the building.

Technical report two is a comparison of the current floor system with the alternate systems that will be introduced and examined. At the conclusion of this report, it will be clear what options are viable as an alternate floor system for Wellington and which are not.

The existing floor system consists of a non-composite steel beam and concrete slab system for the lobby level and first level and a wood joist floor system bearing on wood framed walls for the second and third levels. The alternate systems being considered are:

- Pre-cast hollowcore plank system
- Wood Joist system
- One-way concrete joist construction (CRSI)
- Light-gauge steel system

The layouts of the systems were similar to the existing one due to the intended use of each level. Since the layouts are different between the first level and second and third levels, the same section on both the first and second levels will be evaluated for the alternate systems.

The systems were evaluated for cost, depth of the system, susceptibility to vibrations, fireproofing, and weight. The light-gauge steel system was determined to be the most efficient in cost, weight, and depth. The wood joist and hollowcore plank systems were not ruled out as possibilities but are not superior to the light-gauge system. The one-way concrete joist system was determined to not be an advantageous solution due to cost and construction time issues.

Existing Floor System

Wellington at Hershey's Mill is a 370,000 square foot retirement community in West Chester, Pennsylvania. Wellington includes 3 levels of independent living apartments, a garage level below the residential levels with a lobby alongside it, and a lower level containing the offices of doctors and other businesses for Wellington directly below the lobby.

Wellington has an existing system that combines a non-composite steel beam and concrete slab system on the lobby and first levels with a wood joist floor system bearing on wood framed walls on the second and third levels. There is a garage under the residential levels, which makes the first level framing different from the second and third levels. Because of this difference, a full section of the building will be evaluated instead of one typical bay. This evaluation will be of the first floor layout and the second and third floors' layout.

The following figures show the chosen section with the current floor system.

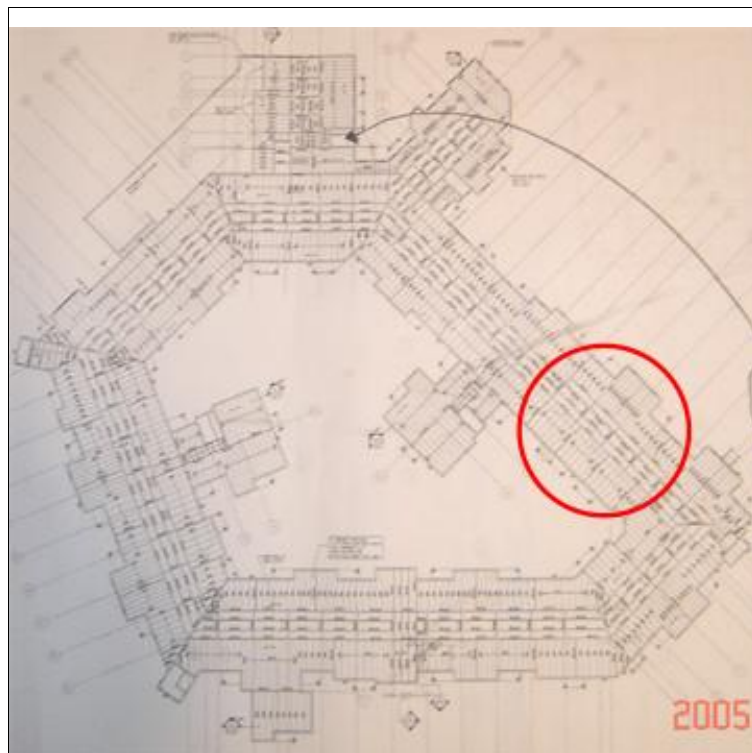


Figure 1

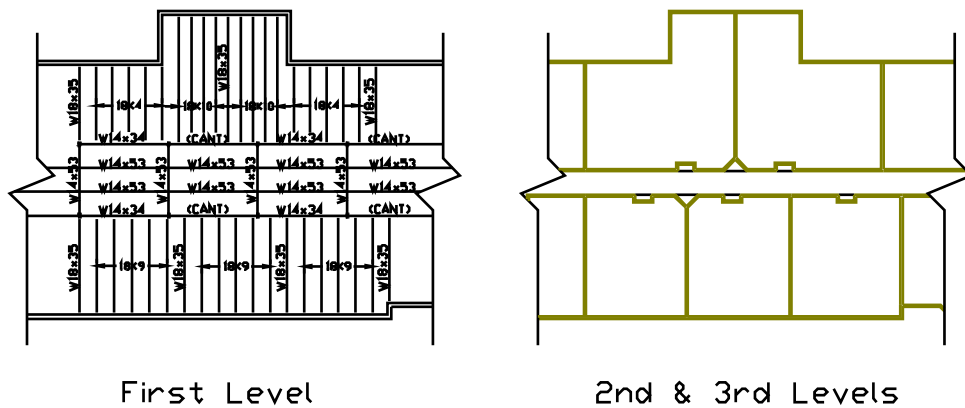


Figure 2

For the alternate systems, the layout will be the same as the existing system. It is important to remember the intended use of the floors when designing the structure. The first level framing has to be designed around the space needed for the maneuvering of cars in the garage. The center bay is 18' wide in the existing system and will remain at this dimension for the alternate systems. For the second and third levels, the existing system has bearing walls separating the apartments and the corridor. In order to keep structural elements from disturbing the apartment layout, the same spacing will be used in the alternate systems again keeping the supporting members on either side of the corridor.

Many systems were considered but eliminated due to the restrictions mentioned above. The range of alternate system is limited due to this, but still shows a variety of options for Wellington.

Floor Loads

Assumed Dead Loads:

MEP = 10 psf
 Carpet = 1 psf
Ceiling = 1 psf
Total = 12 psf

Live Loads:

Private rooms & the corridors serving them: **40 psf**

Alternate System #1 – Pre-cast hollowcore plank system

This system was designed using the Nitterhouse Concrete Products Manual. The 8''-4' Spandek – U.L. – J952 with 2'' topping was chosen for this system. Using a span of 12' in the load table and a 4-1/2'' ϕ strand pattern, it was determined that this plank was more than sufficient to carry the superimposed loads. This system will be bearing on masonry walls which were designed using an empirical design procedure.

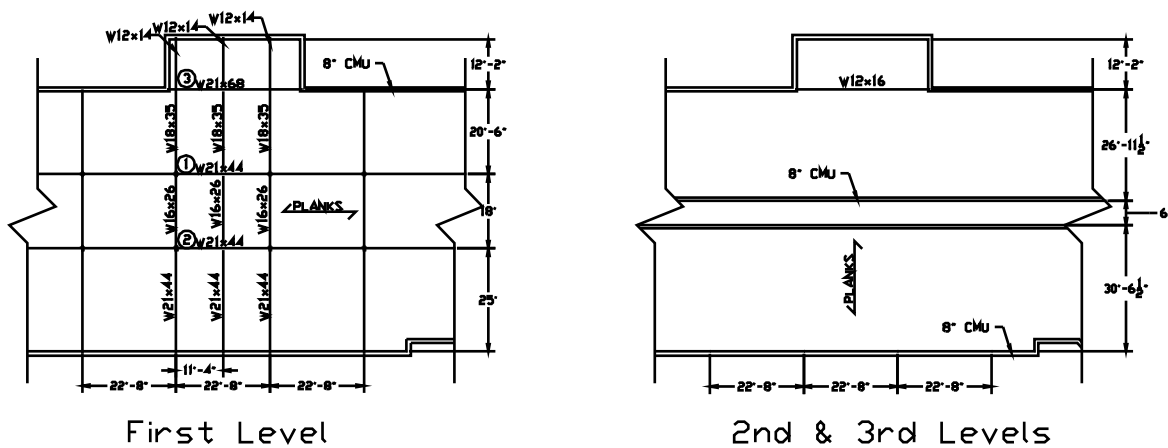


Figure A (1)

Pre-cast hollowcore planks are an excellent alternative for many reasons. Construction time is lessened because the planks are pre-cast and ready for quick installation in any type of weather. Cost is less of an issue when compared to a full concrete slab of the same depth because less concrete is used, which in turn provides a lighter weight floor system. On the second and third levels, the depth is only 10" total, which provides a higher ceiling. Other benefits are that no extra fireproofing is required, vibrations are reduced, and the planks are durable.

Alternate System #2 – Wood Joist Floor System

The wood joist floor system was designed using the TrusJoist TJI® 110, 210, 230, 360 & 560 Joists Beam, Header, and Column Specifier's Guides. The first floor will have wood columns as interior supports instead of interior masonry bearing walls. The second and third floors have the wood joists spanning from bearing wall to bearing wall. The wood columns were designed to be 7"x7" 1.8E Parallam PSL and the floor girder beams 5 1/4"x20" Microllam LVL. The joists were calculated to be 11 7/8" TJI 560 joists at 16" o.c. bearing on 10" ungrouted, unreinforced CMU. The joists for the second and third floors were designed to be 14" TJI 560 joists at 12" o.c. bearing on 10" ungrouted, unreinforced CMU.

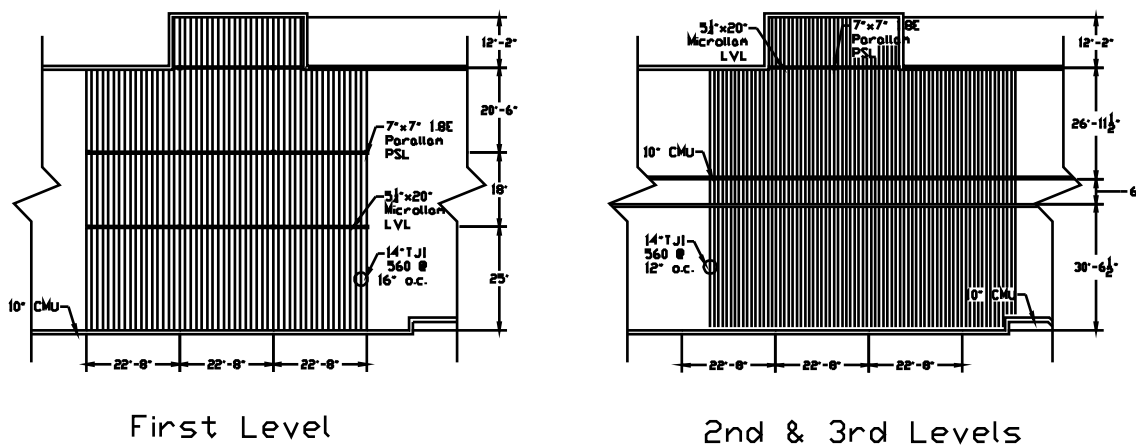


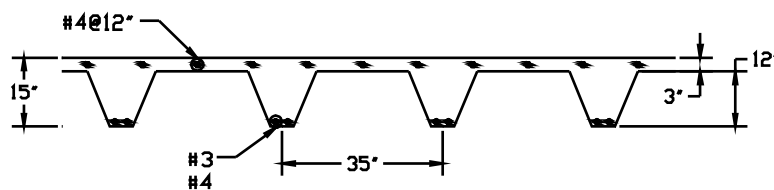
Figure A (2)

This system is an appropriate arrangement for the intended use of the building. The floors are lightweight and allow for faster installation because their components are premanufactured. Since wood is a combustible material and the joists are not manufactured to withstand fire, fireproofing is required by code. A negative aspect of this system is the limited sound proofing the wood provides in the floor. Vibrations can also be a disadvantage because of the flexible quality of wood. The system is also deeper than the other systems.

Alternate System #3 – One-way concrete Joist construction

A one-way concrete joist system consists of a monolithically cast-in-place slab, joist, and girder combination. The joists are evenly spaced spanning in one direction with a thin concrete slab over top. This system is also known as a concrete pan floor system and involves pan forms that are removed after the concrete is cured and finished.

The CRSI Design Handbook 2002 was used for the design of this system. 30" pans with a 12" rib depth and 3" top slab were selected. For a clear span of 22', a 5" rib at 35" c.c. was found to be sufficient. The system self weight is 63 psf. Deflection calculations were not necessary because the system thickness was greater than $l_n/18.5$ for the end span and greater than $l_n/21$ for the interior span. The girders were designed using the width calculated for the girder with the longest span and then used for the other girders to maintain a recurring system. The width of the girders was found to be 22" with a depth of 15" to equal the joist depth.



One-way joist section

Figure A (3)

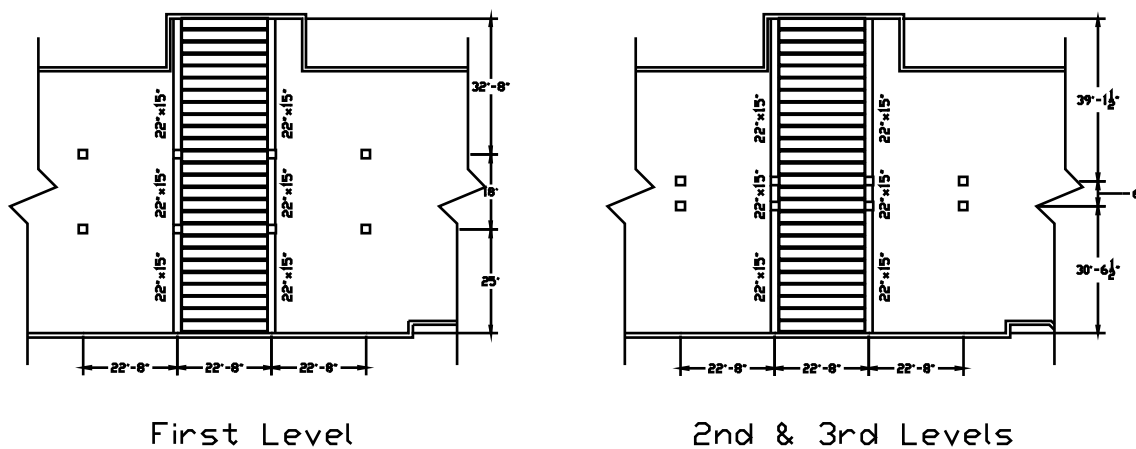


Figure B (4)

A repetitive structure and no requirement of additional fireproofing are advantages for the one-way joist system. However, cast-in-place construction often costs more in time and money and is a heavier structure altogether. This system will also require the re-design of the foundations because of the overall weight.

Alternate System #4 – Light-Gauge Steel system

The light-gauge steel system was designed using the Marino Lightweight Steel Framing Catalogue. The first level has exterior 10" CMU bearing walls; ungrouted and unreinforced. The joists chosen are Marino's 12J14 joists at 16" o.c. The columns were spaced at 11'-4", half the original spacing, because the headers could just support the load at the original spacing. The headers were designed to be the 16SW12. The second and third floors have 14JE10 joists @ 24" o.c. over the apartments and 6SW18 joists @ 24" o.c. in the corridor. The joists rest on metal stud bearing walls designed to have 3-5/8" studs @ 16" o.c.

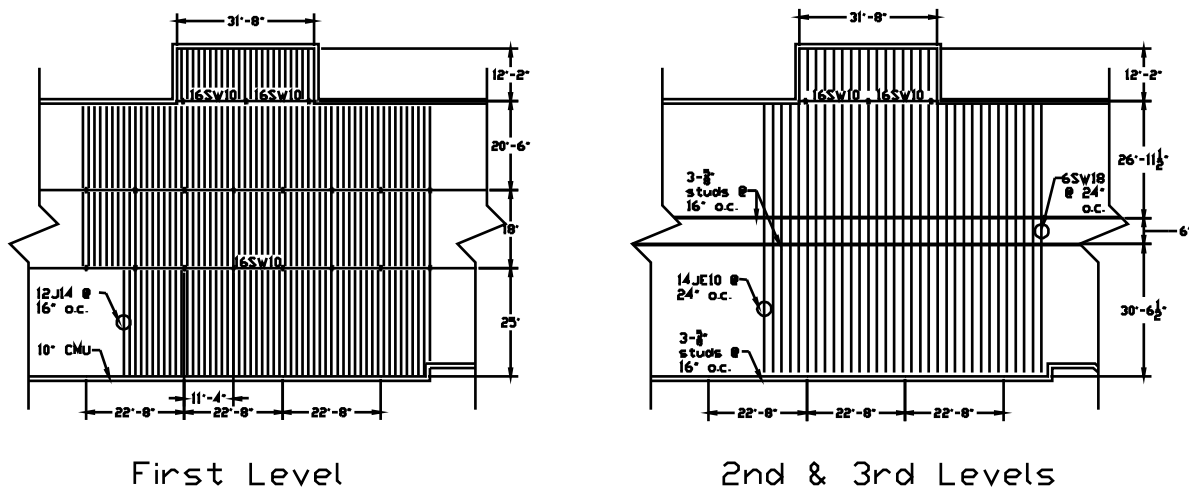


Figure A (4)

For the parts of the building that include a juttied-out section (see Figure B (4) below), a header was placed to break up the span of the joists. Because the headers do not take the applied loads at the full span, a column was placed at the midspan as well as one foot away from the exterior wall. The placement of the columns one foot distance from the wall was necessary to decrease the header span to 14' so it was able to take the applied load. The header was designed as a 16SW10.

The member positions are awkward and will be altered if this system is chosen as the alternative to the present system.

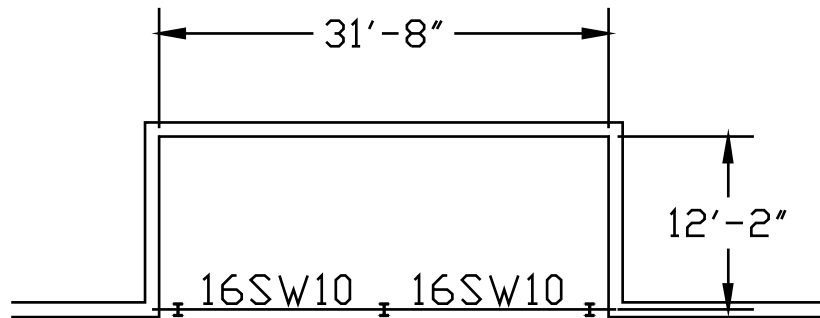


Figure B (4)

A light-gauge steel system is a good alternative for this building because of the low cost and non-combustible construction. The system is lightweight and not very deep. Prefabrication of the members allows for faster, easier installation. A shallow foundation, like the existing one, will work with this system because of the light weight.

Conclusion

After the examination of the four alternate systems, it was determined that the light-gauge steel system would be the best alternative to the existing one. Although the layout of the example system is awkward, this can be remedied with further investigations. The wood joist and the hollowcore plank systems cannot be ruled out as alternatives, but they are not considered superior to the light-gauge system because of a few disadvantages such as sound proofing. The one way joist system is not a good alternative due to cost, construction time, and weight issues.

Floor System	Weight	Depth (Approx.)	Cost	Fireproofing	Vibration	Conclusion
Wood Joist System	Light	34" + plywood	Efficient	Necessary	Increased vibration	Not ruled out
Pre-cast Hollowcore Planks	Moderate	29" + 2" topping = 31"	Efficient	Not necessary for planks	Reduced vibration	Not ruled out
One-way Joist System	Heavy	15"	Not Efficient	Not necessary	Reduced vibration	Too costly
Light-gauge Steel System	Light	16" + slab	Efficient	Necessary	Increased vibration	Most efficient

Appendix 1 – Alternate System #1

Hollowcore Plank floor system - Reference: Nitterhouse Guide

Live load: private rooms & the corridors serving them
40psf

Superimposed dead loads: MEP - 10psf
ceiling - 1psf
carpet - 1psf
12psf

$$W_u = 1.2(12\text{psf}) + 1.6(40\text{psf}) = 78.4\text{psf}$$

Use 8" x 4' Spandeck w/ 2" topping (U.L. - J952)

Span - 11'-4" → use 12' span

Allowable Superimposed Load (psf):

$$\text{flexure } 4\text{-}1/2\text{' } \phi = 611\text{psf} > 78.4\text{psf}$$

$$\text{shear } 4\text{-}1/2\text{' } \phi = 421\text{psf} > 78.4\text{psf}$$

Design beams w/ LRFD:

$$W_u = 1.2(12\text{psf} + 82.5\text{psf}) + 1.6(40\text{psf}) = 177.4\text{psf}$$

(plank self wt)

1st floor

25' span Beam

$$W_u = 177.4\text{psf}(11.33') = 2009.94\text{lb/ft} = 2.01\text{k/ft}$$

$$M_u = \frac{WL^2}{8} = \frac{(2.01\text{k/ft})(25')^2}{8} = 157.03\text{k}$$

$$V_u = \frac{WL}{2} = \frac{(2.01\text{k/ft})(25')}{2} = 25.13\text{k}$$

$$\text{For } \Delta_{\max} = \frac{l}{360}, I_{\text{req'd}} = \frac{5(2.01\text{k/ft})(25')^4 \times (12\text{in/ft})^3}{384(29,000\text{ksi})(0.833\text{'})}$$

$$= 731.3\text{in}^4$$

Try W21x44

$$I = 847\text{in}^4 > 731.3\text{in}^4$$

$$\phi M_p = 359\text{k} > 157.03\text{k}$$

$$\phi V_n = 196\text{k} > 25.13\text{k}$$

18' Span beam

$$w_u = 2.01 \text{ k/ft}$$

$$M_u = \frac{wL^2}{8} = \frac{(2.01 \text{ k/ft})(18')^2}{8} = 81.41 \text{ k}$$

$$V_u = \frac{wL}{2} = \frac{(2.01 \text{ k/ft})(18')}{2} = 18.09 \text{ k}$$

$$\text{For } \Delta_{\max} = \frac{l}{300}, I_{\text{req'd}} = \frac{5(2.01 \text{ k/ft})(18')^4 \times (12 \text{ in/ft})^3}{384(29,000 \text{ ksi})(0.6'')} = 272.85 \text{ in}^4$$

Try W16x26

$$I = 301 \text{ in}^4 > 272.85 \text{ in}^4$$

$$\phi M_p = 160 \text{ k} > 81.41 \text{ k}$$

$$\phi V_n = 100 \text{ k} > 18.09 \text{ k}$$

20'-6" Span Beam

$$w_u = 2.01 \text{ k/ft}$$

$$M_u = \frac{wL^2}{8} = \frac{(2.01 \text{ k/ft})(20.5')^2}{8} = 105.59 \text{ k}$$

$$V_u = \frac{wL}{2} = \frac{(2.01 \text{ k/ft})(20.5')}{2} = 20.6 \text{ k}$$

$$\text{For } \Delta_{\max} = \frac{l}{300}, I_{\text{req'd}} = \frac{5(2.01 \text{ k/ft})(20.5')^4 \times (12 \text{ in/ft})^3}{384(29,000 \text{ ksi})(0.683'')} = 403.25 \text{ in}^4$$

Try W18x35

$$I = 510 \text{ in}^4 > 403.25 \text{ in}^4$$

$$\phi M_p = 249 \text{ k} > 105.59 \text{ k}$$

$$\phi V_n = 143 \text{ k} > 20.6 \text{ k}$$

12'-2" Span Beam

$$w_u = 2.01 \text{ k/ft}$$

$$M_u = \frac{wL^2}{8} = \frac{(2.01 \text{ k/ft})(12.17')^2}{8} = 37.21' \text{ k}$$

$$V_u = \frac{wL}{2} = \frac{(2.01 \text{ k/ft})(12.17')}{2} = 12.23 \text{ k}$$

$$\text{For } \Delta_{\max} = \frac{l}{360}, I_{\text{req'd}} = \frac{5(2.01 \text{ k/ft})(12.17')^4 \times (12 \text{ in/ft})^3}{384(29,000 \text{ ksi})(0.41'')} \\ = 83.44 \text{ in}^4$$

Try W12x14

$$I = 88.5 \text{ in}^4 > 83.44 \text{ in}^4$$

$$\phi M_p = 65.2' \text{ k} > 37.21' \text{ k}$$

$$\phi V_n = 64.3 \text{ k} > 12.23 \text{ k}$$

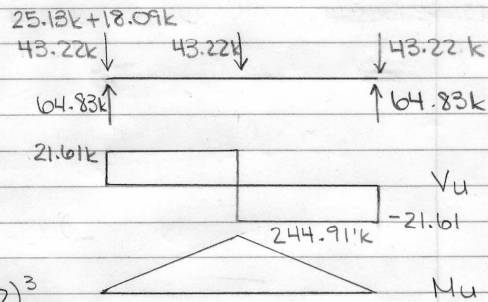
Design Girders:

1st floor

$$\textcircled{1} V_u = 21.61 \text{ k} \\ M_u = 21.61 \text{ k}(11.33') \\ = 244.91' \text{ k}$$

$$\text{For } \Delta_{\max} = \frac{l}{360},$$

$$I_{\text{req'd}} = \frac{43.22 \text{ k}(22.67' \times 12)^3}{48(29,000 \text{ ksi})(22.67' \times 12 / 360)} \\ = 827.21 \text{ in}^4$$



Try W21x44

$$I = 847 \text{ in}^4 > 827.21 \text{ in}^4$$

$$\phi M_p = 359 > 244.91' \text{ k}$$

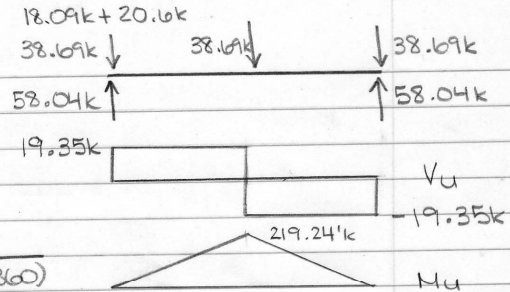
$$\phi V_n = 196 \text{ k} > 21.61 \text{ k}$$

② $V_u = 19.35k$
 $M_u = 219.24'k$

For $\Delta_{max} = \frac{l}{360}$

$$I_{req'd} = \frac{38.69k(22.67' \times 12)^3}{48(29,000ksi)(22.67' \times 12/360)}$$

$$= 740.5 in^4$$



Try W21x44

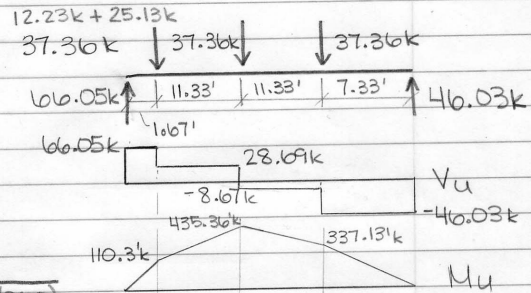
$I = 847 in^4 > 740.5 in^4$
 $\phi M_p = 359'k > 219.24'k$
 $\phi V_n = 196k > 19.35k$

③ 31'-8" span
 $V_u = 66.05k$
 $M_u = 435.36'k$

For $\Delta_{max} = \frac{l}{360}$

$$I_{req'd} = \frac{37.36k(31.67' \times 12)^3}{48(29,000ksi)(31.67' \times 12/360)}$$

$$= 1395.5 in^4$$



Try W21x68

$I = 1480 in^4 > 1395.5 in^4$
 $\phi M_p = 600'k > 435.36'k$
 $\phi V_n = 245k > 66.05k$

2nd & 3rd floors - Plank span direction changed

Longest span = $30' - 6\frac{1}{2}" \rightarrow$ use $31'$
 $w_u = 78.4 \text{ psf}$

Use $8" \times 4'$ Spandeck w/ $2"$ topping (U.L.-J917)

Allowable Superimposed Load (psf):

flexure $b - \frac{1}{2}" \phi = 90 \text{ psf} > 78.4 \text{ psf}$

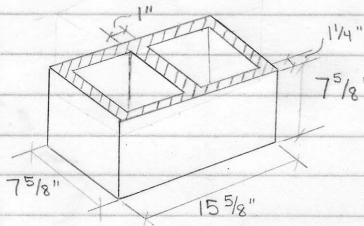
shear $b - \frac{1}{2}" \phi = 110 \text{ psf} > 78.4 \text{ psf}$

Masonry Bearing Walls

Floor Height = $40' \cdot 12"/1' = 120"$

Height to thickness ratio = $120"/8"(\text{trial}) = 15$

Use $8"$ CMU, ungrouted, unreinforced



Gross cross-sectional area =
 $(15\frac{5}{8} \times 7\frac{5}{8}) - 2(5.125 \times 6.0625)$
 $= 119.14 \text{ in}^2 - 62.14 \text{ in}^2$
 $= \underline{57 \text{ in}^2}$

Design Load = $78.4 \text{ psf} + 82.5 \text{ psf} = 160.9 \text{ psf} \cdot \frac{144 \text{ in}^2}{\text{ft}^2} = 23169.6 \text{ psi}$

$23169.6 \text{ psi} / 57 = 406.5 \text{ psi} \therefore$ Use grouted

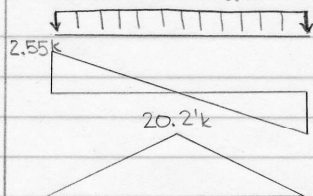
Gross cross-sectional area = 119.14 in^2

$23169.6 \text{ psi} / 119.4 = 194.05 \text{ psi} \therefore$

Use $8"$ CMU, grouted, unreinforced @ 4500 psi or greater
compressive strength, Type N mortar
 $200 \text{ psi} > 194.05 \text{ psi}$

Design Steel Beam - LRFD 31'-8" span

$$w_u = 78.4 \text{ psf} + 82.5 \text{ psf} = 160.9 \text{ psf}$$



$$V_u = 2.55 \text{ k}$$

$$M_u = 20.2 \text{ k}$$

$$\text{For } \Delta_{\max} = \frac{l}{360}$$

$$I_{\text{req'd}} = \frac{2.55 \text{ k} (31.67' \times 12)^3}{48(29,000 \text{ ksi})(31.67' \times 12 / 360)} = 95.25 \text{ in}^4$$

Try W12x16

$$I = 103 \text{ in}^4 > 95.25 \text{ in}^4$$

$$\phi M_p = 75.4 \text{ k} > 20.2 \text{ k}$$

$$\phi V_n = 71.3 \text{ k} > 2.55 \text{ k}$$

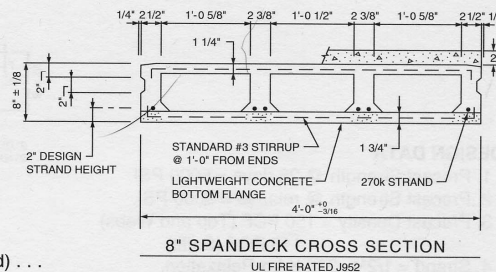
Prestressed Concrete 8" x 4' SpanDeck – U.L. – J952

(2" C.I.P. TOPPING)

PHYSICAL PROPERTIES			
Composite			
A' = 295 in. ²		S _b = 468 in. ³	
I' = 2624 in. ⁴		S _t = 1096 in. ³ (At Top of SpanDeck)	
Y _b ' = 5.61 in.		S _{tt} = 597 in. ³ (At Top of Topping)	
Y _t ' = 2.39 in. (To Top of SpanDeck)		Wt.' = 330 PLF	
Y _{tt} ' = 4.39 in. (To Top of Topping)		Wt.' = 82.5 PSF	

DESIGN DATA

1. Precast Strength @ 28 days = 5000 PSI.
2. Precast Strength @ release = 3000 PSI.
3. Precast Density = 150 PCF (Top and Webs)
= 115 PCF (Soffit)
4. Strand = 1/2"Ø, 270K Lo-Relaxation.
5. Composite Strength = 3000 PSI.
6. Composite Density = 150 PCF.
7. Strand Height = 2.00 in.
8. Ultimate moment capacities (when fully developed) . . .
4 – 1/2"Ø, 270K = 88.3'K
6 – 1/2"Ø, 270K = 124.0'K
9. Maximum bottom tensile stress is $6\sqrt{f_c} = 424$ PSI.
10. All superimposed load is treated as live load in the strength analysis of flexure and shear.
11. Flexural strength capacity is based on stress/strain strand relationships.
12. Shear values are the maximum allowable before shear reinforcement is required.
13. Deflection limits were not considered when determining allowable loads in this table.
14. Load values to the left of the solid line are controlled by ultimate strength. Load values to the right are controlled by service stress.
15. All loads shown refer to allowable loads applied after topping has hardened.



8" SPANDECK W/2" TOPPING		ALLOWABLE SUPERIMPOSED LOAD (PSF)																																													
		SPAN (FEET)																																													
STRAND PATTERN		10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
Flexure	4 – 1/2"Ø	750	675	611	546	462	394	338	291	252	218	191	167	146	128	112	98	85	74	63	51	41	31	21	750	675	611	546	462	394	338	291	252	218	191	167	146	128	112	98	85	74	63	51	41	31	21
Shear	4 – 1/2"Ø	527	469	421	382	348	317	294	272	252	235	219	197	176	157	140	129	122	110	98	88	78	70	63	527	469	421	382	348	317	294	272	252	235	219	197	176	157	140	129	122	110	98	88	78	70	63
Flexure	6 – 1/2"Ø	1098	900	898	794	676	580	502	437	382	336	296	262	233	207	185	165	147	132	116	101	87	74	63	1098	900	898	794	676	580	502	437	382	336	296	262	233	207	185	165	147	132	116	101	87	74	63
Shear	6 – 1/2"Ø	542	483	434	393	359	329	303	280	261	243	227	212	199	188	178	167	152	137	124	112	101	91	86	542	483	434	393	359	329	303	280	261	243	227	212	199	188	178	167	152	137	124	112	101	91	86



This table is for simple spans and uniform loads. Design data for any of these span-load conditions is available on request. Individual designs may be furnished to satisfy unusual conditions of heavy loads, concentrated loads, cantilevers, flange or stem openings and narrow widths.

2655 Molly Pitcher Hwy. South, Box N
Chambersburg, PA 17201-0813
717-267-4505 • FAX: 717-267-4518

REVISED 12/93

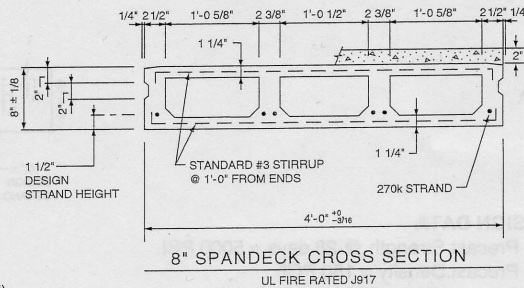
Prestressed Concrete 8" x 4' SpanDeck – U.L. – J917

(2" C.I.P. TOPPING)

PHYSICAL PROPERTIES	
Composite	
$A' = 254 \text{ in.}^2$	$S'_b = 547 \text{ in.}^3$
$I' = 2944 \text{ in.}^4$	$S'_t = 1124 \text{ in.}^3$ (At Top of SpanDeck)
$Y_{b'} = 5.38 \text{ in.}$	$S'_{tt} = 637 \text{ in.}^3$ (At Top of Topping)
$Y_{t'} = 2.62 \text{ in.}$ (To Top of SpanDeck)	$Wt.' = 330 \text{ PLF}$
$Y'_{tt} = 4.62 \text{ in.}$ (To Top of Topping)	$Wt.' = 82.5 \text{ PSF}$

DESIGN DATA

1. Precast Strength @ 28 days = 5000 PSI.
2. Precast Density = 150 PCF
3. Strand = 1/2"Ø, 270K Lo-Relaxation.
4. Composite Strength = 3000 PSI.
5. Composite Density = 150 PCF.
6. Strand Height = 1.5 in.
7. Ultimate moment capacities (when fully developed) . . .
 - 4 – 1/2"Ø, 270K = 94.6'K
 - 6 – 1/2"Ø, 270K = 133.3'K
8. Maximum bottom tensile stress is $6\sqrt{f'_c} = 424 \text{ PSI}$.
9. All superimposed load is treated as live load in the strength analysis of flexure and shear.
10. Flexural strength capacity is based on stress/strain strand relationships.
11. Load values to the left of the solid line are controlled by ultimate strength. Load values to the right are controlled by service stress.
12. Shear values are the maximum allowable before shear reinforcement is required.
13. Deflection limits were not considered when determining allowable loads in this table.
14. All loads shown refer to allowable loads applied after topping has hardened.



8" SPANDECK W/2" TOPPING		ALLOWABLE SUPERIMPOSED LOAD (PSF)																											
		SPAN (FEET)																											
STRAND PATTERN		10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32					
Flexure	4 – 1/2"Ø	795	718	650	590	500	426	366	317	275	240	210	184	162	142	125	110	96	84	73	60	49	39	X					
Shear	4 – 1/2"Ø	571	509	458	415	378	347	320	296	275	257	240	222	199	178	160	145	133	126	115	103	93	84	X					
Flexure	6 – 1/2"Ø	1155	1040	945	859	732	629	544	474	416	366	324	287	256	228	204	183	164	147	132	118	103	90	77					
Shear	6 – 1/2"Ø	589	525	472	428	391	360	331	308	286	266	249	235	220	207	195	184	175	160	145	132	120	110	100					



This table is for simple spans and uniform loads. Design data for any of these span-load conditions is available on request. Individual designs may be furnished to satisfy unusual conditions of heavy loads, concentrated loads, cantilevers, flange or stem openings and narrow widths.

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REVISED 12/93

Appendix 2 – Alternate System #2

Wood Joist System - Reference: Trus Joist TJI Joists
& Beam, Header, & Column
Specifier's Guides

1st Floor

Longest Span = 25'

Try 11 $\frac{7}{8}$ " TJI 560 @ 16" o.c. (span = 26'-3" > 25') [Floor span tables]

Floor Load Table

LL = 40 psf \rightarrow 54 plf (conversion table)

DL = 12 psf

Total Load = 52 psf \rightarrow 69.8 plf (conversion table)

Interpolation in Floor load table \therefore try 14" TJI 560 @ 16"

LL \cong 62 plf > 54 plf

TL \cong 95 plf > 69.8 plf

Use 14" TJI 560 joists @ 16" o.c.

Floor Girder Beams (Sizing tables)

Floor Load (psf): 40 LL + 12 DL table notes

Longest floor framing length = 40' x 0.8 = 32'

Column spacing = 22'-8" use 24'

Use 5 $\frac{1}{4}$ " x 20" Microllam LVL

Columns

Largest trib area = 22'-8" x 20' = 453.33 ft²

w_u = 12 psf + 40 psf = 52 psf

P = 52 psf (453.33 ft²) = 23,573.16 lbs

Effective column length = 15 ft

Try 7" x 7" 1.8E Parallam PSL

31,333 lbs > 23,573.16 lbs

Use 7" x 7" 1.8E Parallam PSL

(1)

Masonry Exterior Bearing Walls

$$\text{Joist weight} = 4.0 \text{ plf} / (10'' \cdot \frac{1}{12}'') = 4.8 \text{ psf}$$

$$\text{Floor Height} = 15' \cdot 12''/1' = 180''$$

$$\text{Height to thickness ratio} = 180''/8'' (\text{trial}) = 22.5 \text{ NG}$$
$$180''/10'' = 18$$

Try 10" CMU, ungrouted, unreinforced

$$\text{Gross cross-sectional area} = (15\frac{7}{8}'' \times 9\frac{7}{8}'') - 2(4.875'' \times 11.75'')$$
$$= 150.4 \text{ in}^2 - 57.3 \text{ in}^2$$
$$= 93.1 \text{ in}^2$$

$$\text{Design Load} = 52 \text{ psf} + 4.8 \text{ psf} = 56.8 \text{ psf} \cdot \frac{144 \text{ in}^2}{\text{ft}^2} = 8179.2 \text{ psi}$$
$$8179.2 \text{ psi} / 93.1 = 87.9 \text{ psi}$$

Use 10" CMU, ungrouted, unreinforced @ 1500 psi
compressive strength, type N mortar
100 psi > 87.9 psi

2nd & 3rd floors

$$\text{Longest span} = 30' - 6\frac{1}{2}''$$

Try 14" TJI 560 @ 12" o.c. (span = 32' - 8" > 30' - 6\frac{1}{2}")

Floor Load Table

$$\text{LL} = 40 \text{ psf} \rightarrow 40 \text{ plf (conversion table)}$$

$$\text{TL} = 52 \text{ psf} \rightarrow 52 \text{ plf} \quad "$$

Interpolation: TL \approx 80 plf > 52 plf

Use 14" TJI 560 @ 12" o.c.

Masonry Bearing walls

$$\text{Joist weight} = 4.2 \text{ plf} / (8'' \cdot \frac{1}{12}'') = 6.3 \text{ psf}$$

$$\text{Floor height} = 10' \cdot (12'' \cdot 1') = 120''$$

$$\text{Height to thickness ratio} = 120''/8'' = 15$$

Try 8" CMU, ungrouted, unreinforced

$$\text{Gross cross-sectional area} = 57 \text{ in}^2 \text{ (calculated in Appendix 2)}$$

$$\text{Design Load} = 52 \text{ psf} + 6.3 \text{ psf} = 58.3 \text{ psf} \cdot \frac{144 \text{ in}^2}{\text{ft}^2} = 8395.2 \text{ psi}$$
$$8395.2 \text{ psi} / 57 = 147.3 \text{ psi} < 140 \text{ psi}$$

\therefore Increase CMU size

(2)

Try 10" CMU, ungrouted, unreinforced

Gross cross-sectional area = 93.1 in^2 (previously calculated)

$$8395.2 \text{ psi} / 93.1 = 90.17 \text{ psi}$$

Use 10" CMU, ungrouted, unreinforced @ 1500 psi

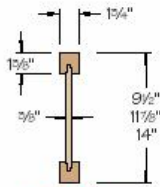
Compressive strength, type N mortar

$$100 \text{ psi} > 90.17 \text{ psi}$$

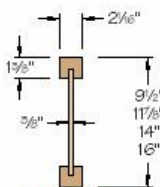
4 Floor Span Tables

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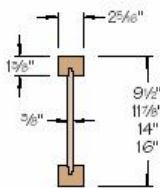
Not all products are available in all markets. Contact your Trus Joist representative for information.



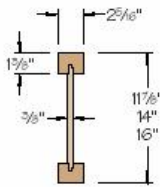
TJI® 110 joists



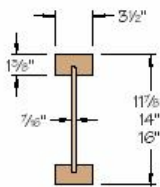
TJI® 210 joists



TJI® 230 joists



TJI® 360 joists



TJI® 560 joists

L/480 Live Load Deflection

Depth	TJI®	40 PSF Live Load / 10 PSF Dead Load				40 PSF Live Load / 20 PSF Dead Load			
		12" o.c.	16" o.c.	19.2" o.c.	24" o.c.	12" o.c.	16" o.c.	19.2" o.c.	24" o.c.
9 1/2"	110	16'-5"	15'-0"	14'-2"	13'-2"	16'-5"	15'-0"	13'-11"	12'-5"
	210	17'-3"	15'-9"	14'-10"	13'-10"	17'-3"	15'-9"	14'-10"	13'-8"
	230	17'-8"	16'-2"	15'-3"	14'-2"	17'-8"	16'-2"	15'-3"	14'-2"
11 1/8"	110	19'-6"	17'-10"	16'-10"	15'-5" ⁽¹⁾	19'-6"	17'-3"	15'-8"	14'-0" ⁽¹⁾
	210	20'-6"	18'-8"	17'-8"	16'-5"	20'-6"	18'-8"	17'-3"	15'-5" ⁽¹⁾
	230	21'-0"	19'-2"	18'-1"	16'-10"	21'-0"	19'-2"	18'-1"	16'-3" ⁽¹⁾
14"	360	22'-11"	20'-11"	19'-8"	18'-4"	22'-11"	20'-11"	19'-8"	17'-10" ⁽¹⁾
	560	26'-1"	23'-8"	22'-4"	20'-9"	26'-1"	23'-8"	22'-4"	20'-9" ⁽¹⁾
	110	22'-2"	20'-3"	18'-9"	16'-9" ⁽¹⁾	21'-8"	18'-9"	17'-1" ⁽¹⁾	14'-7" ⁽¹⁾
16"	210	23'-3"	21'-3"	20'-0"	18'-4" ⁽¹⁾	23'-3"	20'-7"	18'-9" ⁽¹⁾	16'-2" ⁽¹⁾
	230	23'-10"	21'-9"	20'-6"	19'-1"	23'-10"	21'-8"	19'-9"	17'-1" ⁽¹⁾
	360	26'-0"	23'-8"	22'-4"	20'-9" ⁽¹⁾	26'-0"	23'-8"	22'-4" ⁽¹⁾	17'-10" ⁽¹⁾
16"	560	29'-6"	26'-10"	25'-4"	23'-6"	29'-6"	26'-10"	25'-4" ⁽¹⁾	20'-11" ⁽¹⁾
	210	25'-9"	23'-6"	22'-0" ⁽¹⁾	19'-5" ⁽¹⁾	25'-5"	22'-0" ⁽¹⁾	20'-1" ⁽¹⁾	16'-2" ⁽¹⁾
	230	26'-5"	24'-1"	22'-9"	20'-7" ⁽¹⁾	26'-5"	23'-2"	21'-2" ⁽¹⁾	17'-1" ⁽¹⁾
16"	360	28'-9"	26'-3"	24'-8" ⁽¹⁾	21'-5" ⁽¹⁾	28'-9"	26'-3" ⁽¹⁾	22'-4" ⁽¹⁾	17'-10" ⁽¹⁾
	560	32'-8"	29'-8"	28'-0"	25'-2" ⁽¹⁾	32'-8"	29'-8"	26'-3" ⁽¹⁾	20'-11" ⁽¹⁾

L/360 Live Load Deflection (Minimum Criteria per Code)

Depth	TJI®	40 PSF Live Load / 10 PSF Dead Load				40 PSF Live Load / 20 PSF Dead Load			
		12" o.c.	16" o.c.	19.2" o.c.	24" o.c.	12" o.c.	16" o.c.	19.2" o.c.	24" o.c.
9 1/2"	110	18'-2"	16'-7"	15'-3"	13'-8"	17'-8"	15'-3"	13'-11"	12'-5"
	210	19'-1"	17'-5"	16'-6"	15'-0"	19'-1"	16'-9"	15'-4"	13'-8"
	230	19'-7"	17'-11"	16'-11"	15'-9"	19'-7"	17'-8"	16'-1"	14'-5"
11 1/8"	110	21'-7"	18'-11"	17'-3"	15'-5" ⁽¹⁾	19'-11"	17'-3"	15'-8"	14'-0" ⁽¹⁾
	210	22'-8"	20'-8"	18'-11"	16'-10"	21'-10"	18'-11"	17'-3"	15'-5" ⁽¹⁾
	230	23'-3"	21'-3"	19'-11"	17'-9"	23'-0"	19'-11"	18'-2"	16'-3" ⁽¹⁾
14"	360	25'-4"	23'-2"	21'-10"	20'-4" ⁽¹⁾	25'-4"	23'-2"	21'-10"⁽¹⁾	17'-10" ⁽¹⁾
	560	28'-10"	26'-3"	24'-9"	23'-0"	28'-10"	26'-3"	24'-9"	20'-11" ⁽¹⁾
	110	23'-9"	20'-6"	18'-9"	16'-9" ⁽¹⁾	21'-8"	18'-9"	17'-1" ⁽¹⁾	14'-7" ⁽¹⁾
16"	210	25'-8"	22'-6"	20'-7"	18'-4" ⁽¹⁾	23'-9"	20'-7"	18'-9" ⁽¹⁾	16'-2" ⁽¹⁾
	230	26'-4"	23'-9"	21'-8"	19'-4" ⁽¹⁾	25'-0"	21'-8"	19'-9"	17'-1" ⁽¹⁾
	360	28'-9"	26'-3"	24'-9" ⁽¹⁾	21'-5" ⁽¹⁾	28'-9"	26'-3"⁽¹⁾	22'-4" ⁽¹⁾	17'-10" ⁽¹⁾
16"	560	32'-8"	29'-9"	28'-0"	25'-2" ⁽¹⁾	32'-8"	29'-9"	26'-3"⁽¹⁾	20'-11" ⁽¹⁾
	210	27'-10"	24'-1"	22'-0" ⁽¹⁾	19'-5" ⁽¹⁾	25'-5"	22'-0" ⁽¹⁾	20'-1" ⁽¹⁾	16'-2" ⁽¹⁾
	230	29'-2"	25'-5"	23'-2"	20'-7" ⁽¹⁾	26'-9"	23'-2"	21'-2" ⁽¹⁾	17'-1" ⁽¹⁾
16"	360	31'-10"	29'-0"	26'-10" ⁽¹⁾	21'-5" ⁽¹⁾	31'-10"	26'-10"⁽¹⁾	22'-4" ⁽¹⁾	17'-10" ⁽¹⁾
	560	36'-1"	32'-11"	31'-0" ⁽¹⁾	25'-2" ⁽¹⁾	36'-1"	31'-6"⁽¹⁾	26'-3" ⁽¹⁾	20'-11" ⁽¹⁾

Long term deflection under dead load, which includes the effect of creep, has not been considered. **Bold italic** spans reflect initial dead load deflection exceeding 0.33".

(1) Web stiffeners are required at intermediate supports of continuous-span joists when the intermediate bearing length is less than 5 1/4" and the span on either side of the intermediate bearing is greater than the following spans:

TJI®	40 PSF Live Load / 10 PSF Dead Load				40 PSF Live Load / 20 PSF Dead Load			
	12" o.c.	16" o.c.	19.2" o.c.	24" o.c.	12" o.c.	16" o.c.	19.2" o.c.	24" o.c.
110	N.A.	N.A.	N.A.	15'-4"	N.A.	N.A.	16'-0"	12'-9"
210	N.A.	N.A.	21'-4"	17'-0"	N.A.	21'-4"	17'-9"	14'-2"
230	N.A.	N.A.	N.A.	19'-2"	N.A.	N.A.	19'-11"	15'-11"
360	N.A.	N.A.	24'-5"	19'-6"	N.A.	24'-5"	20'-4"	16'-3"
560	N.A.	N.A.	29'-10"	23'-10"	N.A.	29'-10"	24'-10"	19'-10"

How to Use These Tables

1. Determine the appropriate live load deflection criteria.
2. Identify the live and dead load condition.
3. Select on-center spacing.
4. Scan down the column until you meet or exceed the span of your application.
5. Select TJI® joist and depth.

Live load deflection is not the only factor that affects how a floor will perform. To more accurately predict floor performance, use our TJI-Pro™ Rating system.

General Notes

- Tables are based on:
 - Uniform loads.
 - More restrictive of simple or continuous span.
 - Clear distance between supports (1 3/4" minimum end bearing).
- Assumed composite action with a single layer of 24" on-center span-rated, glue-nailed floor panels for deflection only. **Spans shall be reduced 6" when floor panels are nailed only.**
- Spans generated from Trus Joist software may exceed the spans shown in these tables because software reflects actual design conditions.
- For loading conditions not shown, refer to software or to load tables on page 5.

Floor Load Table

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Floor—100% (PLF)

Depth	TJI®	Joist Clear Span																	
		8'		10'		12'		14'		16'		18'		20'		22'		24'	
		Live Load L/480	Total Load	Live Load L/480	Total Load	Live Load L/480	Total Load	Live Load L/480	Total Load	Live Load L/480	Total Load	Live Load L/480	Total Load	Live Load L/480	Total Load	Live Load L/480	Total Load		
9½"	110	* 190	127 162	77 127	50 95														
	210	* 210	147 169	90 141	59 114	40 81													
	230	* 236	159 190	98 158	64 125	44 88													
11½"	110	* 190	* 162	* 127	89 109	57 92													
	210	* 210	* 169	* 141	97 121	67 106	48 97												
	230	* 236	* 190	* 158	105 136	73 119	52 97	39 79											
14"	110	* 190	* 236	* 197	* 169	138 148	101 132	76 119	58 108	45 91									
	210	* 210	* 169	* 141	* 121	96 106	69 94	51 84	43 77										
	230	* 236	* 190	* 158	* 136	104 119	75 106	56 93	49 77										
16"	110	* 190	* 236	* 197	* 169	* 148	* 132	107 119	83 108	65 99									
	210	* 210	* 169	* 141	* 121	* 106	93 94	69 85	53 77										
	230	* 236	* 190	* 158	* 136	* 119	100 106	75 95	57 87										
16"	110	* 190	* 236	* 197	* 169	* 148	* 132	* 119	* 108	89 81									
	210	* 210	* 169	* 141	* 121	* 121	* 108	* 97	75 88	69 81									
	230	* 236	* 190	* 158	* 136	* 121	* 108	* 97	75 88	69 81									

*Includes TOTAL DEAD value controls.

How to Use This Table

1. Calculate actual total and live load in pounds per linear foot (plf).
2. Select appropriate Joist Clear Span.
3. Scan down the column to find a TJI® joist that meets or exceeds actual total and live loads.



General Notes

- Table is based on:
 - Uniform loads.
 - No composite action provided by sheathing.
 - More restrictive of simple or continuous span.
- Total Load limits joist deflection to L/240.
- Live Load is based on joist deflection of L/480.
- If a live load deflection limit of L/360 is desired, multiply value in Live Load column by 1.33. The resulting live load shall not exceed the Total Load shown.

PSF to PLF Conversions

O.C. Spacing	Load in Pounds Per Square Foot (PSF)					
	20	25	30	35	40	45
12"	20	25	30	35	40	45
16"	27	34	40	47	54	60
19.2"	32	40	48	56	64	72
24"	40	50	60	70	80	90

Design Properties (100% Load Duration)

Depth	TJI®	Basic Properties				Reaction Properties		
		Joist Weight (lbs/ft)	Maximum Resistive Moment ⁽¹⁾ (ft-lbs)	Joist Only EI x 10 ⁶ (in. ² -lbs)	Maximum Vertical Shear (lbs)	1¾" End Reaction (lbs)	3½" Intermediate Reaction (lbs)	
						No Web Stiffeners	With Web Stiffeners	
9½"	110	2.3	2,380	140	1,220	885	1,935	N.A.
	210	2.6	2,860	167	1,330	980	2,145	N.A.
	230	2.7	3,175	183	1,330	1,035	2,410	N.A.
11½"	110	2.5	3,015	238	1,560	885	1,935	2,295
	210	2.8	3,620	283	1,655	980	2,145	2,505
	230	3.0	4,015	310	1,655	1,035	2,410	2,765
	360	3.0	6,180	419	1,705	1,080	2,460	2,815
14"	560	4.0	9,500	636	2,050	1,265	3,000	3,475
	110	2.8	3,565	351	1,860	885	1,935	2,295
	210	3.1	4,280	415	1,945	980	2,145	2,505
	230	3.3	4,755	454	1,945	1,035	2,410	2,765
16"	360	3.3	7,335	612	1,955	1,080	2,460	2,815
	560	4.2	11,275	926	2,390	1,265	3,000	3,475
	210	3.3	4,895	566	2,190	980	2,145	2,505
16"	230	3.5	5,440	618	2,190	1,035	2,410	2,765
	360	3.5	8,405	830	2,190	1,080	2,460	2,815
	560	4.5	12,925	1,252	2,710	1,265	3,000	3,475

⁽¹⁾ Caution: Do not increase joist moment design properties by a repetitive member use factor.

General Notes

- Table is based on:
 - Uniform loads.
 - More restrictive of simple or continuous beam span. Ratio of short span to long span should be greater than 0.4 to prevent uplift.
 - Deflection criteria of L/360 live load and L/240 total load.

Also see General Assumptions on page 5.

Bearing Requirements

Minimum beam supports to be 2 trimmers (3") at each end and 7½" at continuous-span supports.

(3) Requires 3 trimmers (4½") at each end and 11¼" at continuous-span supports.

Floor Girder Beams *continued*

Floor Load (PSF)	Floor Framing Length	Column Spacing																
		18'			20'			22'			24'							
40LL + 12DL	24'	3½" x 18"	M	P	3½" x 18"	M	P	3½" x 20 ⁽³⁾	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P		
		5¼" x 14"	T	M	P	3½" x 20"	M	P	5¼" x 18"	M	P	7" x 18"	M	P				
		5¼" x 16"	T	M	P	5¼" x 16"	M	P	7" x 16"	M	P							
	28'	3½" x 18"	M	P	3½" x 20 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P		
		5¼" x 16"	T	M	P	5¼" x 16"	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P	
		7" x 14"	T	M	P	5¼" x 18"	M	P										
	30'	3½" x 18 ⁽³⁾	M	P	3½" x 20 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P		
		5¼" x 16"	T	M	P	5¼" x 18"	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P	
		7" x 14"	T	M	P	7" x 16"	M	P										
	32'	3½" x 18 ⁽³⁾	M	P	3½" x 20 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P		
		3½" x 20 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	7" x 18"	M	P	7" x 18"	M	P		
		5¼" x 16"	T	M	P	7" x 16"	M	P										
	34'	3½" x 18 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P		
		3½" x 20 ⁽³⁾	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P	7" x 18"	M	P		
		5¼" x 16"	M	P														
	36'	3½" x 18 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P	7" x 18"	M	P		
		3½" x 20 ⁽³⁾	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P					
		5¼" x 16"	M	P														
	40'	3½" x 20 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20 ⁽³⁾	M	P	5¼" x 20 ⁽³⁾	M	P					
		5¼" x 16"	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P					
		5¼" x 18"	M	P														
	40LL + 20DL	24'	3½" x 18 ⁽³⁾	M	P	3½" x 20 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P	
			5¼" x 16"	T	M	P	5¼" x 16"	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P
			7" x 14"	T	M	P												
28'		3½" x 18 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P		
		3½" x 20 ⁽³⁾	M	P	7" x 16"	M	P	5¼" x 20"	M	P	7" x 18"	M	P	7" x 18"	M	P		
		5¼" x 16"	T	M	P													
30'		3½" x 18 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20"	M	P	5¼" x 20"	M	P	7" x 18"	M	P		
		3½" x 20 ⁽³⁾	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P					
		5¼" x 16"	M	P														
32'		3½" x 20 ⁽³⁾	M	P	5¼" x 18"	M	P	5¼" x 20 ⁽³⁾	M	P	5¼" x 20 ⁽³⁾	M	P					
		5¼" x 16"	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P					
		7" x 14"	T	M	P													
34'		5¼" x 16"	M	P	5¼" x 18"	M	P	5¼" x 20 ⁽³⁾	M	P	5¼" x 20 ⁽³⁾	M	P					
		5¼" x 18"	M	P	7" x 16"	M	P	7" x 18"	M	P	7" x 18"	M	P					
36'		5¼" x 16"	M	P	5¼" x 18 ⁽³⁾	M	P	7" x 18"	M	P	7" x 18"	M	P					
		5¼" x 18"	M	P	5¼" x 20 ⁽³⁾	M	P	7" x 16"	M	P								
40'		5¼" x 18 ⁽³⁾	M	P	5¼" x 20 ⁽³⁾	M	P	7" x 18"	M	P	7" x 18"	M	P					
		7" x 16"	M	P	7" x 18"	M	P											

T 1.7E TimberStrand® LSL **M** 1.9E Microllam® LVL **P** 2.0E Parallam® PSL

Columns

Allowable Axial Loads (lbs) for 1.3E TimberStrand® LSL

Connection Type	Effective Column Length	Column Size														
		3½" x 3½"			3½" x 4½"			3½" x 5½"			3½" x 7¼"			3½" x 8½"		
		100%	115%	125%	100%	115%	125%	100%	115%	125%	100%	115%	125%	100%	115%	125%
Steel and Column Bearing	3'	10,740	12,140	13,040	13,425	15,175	16,300	16,875	19,075	20,490	22,245	25,145	27,010	26,465	29,910	32,135
	4'	9,785	10,880	11,565	12,230	13,605	14,455	15,375	17,100	18,170	20,270	22,540	23,950	24,115	26,815	28,495
	5'	8,605	9,365	9,810	10,755	11,705	12,260	13,520	14,715	15,415	17,825	19,395	20,320	21,205	23,075	24,175
	6'	7,320	7,800	8,075	9,155	9,755	10,095	11,505	12,260	12,690	15,170	16,160	16,730	18,045	19,230	19,905
	7'	6,130	6,445	6,620	7,665	8,055	8,275	9,635	10,125	10,405	12,700	13,350	13,715	15,110	15,880	16,315
	8'	5,140	5,355	5,475	6,425	6,695	6,845	8,075	8,415	8,610	10,645	11,090	11,345	12,665	13,195	13,500
	9'	4,340	4,500	4,585	5,430	5,620	5,735	6,825	7,070	7,210	8,995	9,315	9,500	10,700	11,085	11,305
	10'	3,705	3,820	3,890	4,630	4,775	4,860	5,820	6,005	6,110	7,675	7,915	8,055	9,130	9,415	9,580
	12'	2,775	2,845	2,885	3,470	3,555	3,610	4,360	4,470	4,535	5,750	5,895	5,980	6,840	7,015	7,115
	14'	2,150	2,195	2,220	2,685	2,745	2,775	3,380	3,450	3,490	4,455	4,550	4,600	5,295	5,410	5,475
Plate Bearing ⁽¹⁾	3'-7'	5,425	5,425	5,425	6,650	6,650	6,650	8,225	8,225	8,225	10,675	10,675	10,675	12,600	12,600	12,600
	8'	5,140	5,355	5,425	6,425	6,650	6,650	8,075	8,225	8,225	10,645	10,675	10,675	12,600	12,600	12,600
	9'	4,340	4,500	4,585	5,430	5,620	5,735	6,825	7,070	7,210	8,995	9,315	9,500	10,700	11,085	11,305
	10'	3,705	3,820	3,890	4,630	4,775	4,860	5,820	6,005	6,110	7,675	7,915	8,055	9,130	9,415	9,580
	12'	2,775	2,845	2,885	3,470	3,555	3,610	4,360	4,470	4,535	5,750	5,895	5,980	6,840	7,015	7,115
	14'	2,150	2,195	2,220	2,685	2,745	2,775	3,380	3,450	3,490	4,455	4,550	4,600	5,295	5,410	5,475

(1) See connection details below.

Allowable Axial Loads (lbs) for 1.8E Parallam® PSL

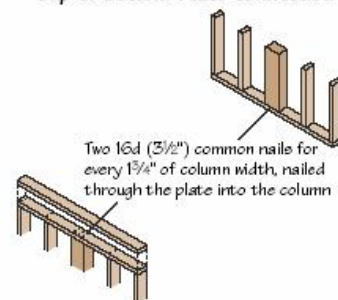
Connection Type	Effective Column Length	Column Size																		
		3½" x 3½"			3½" x 5¼"			3½" x 7"			5¼" x 5¼"			5¼" x 7"			7" x 7"			
		100%	115%	125%	100%	115%	125%	100%	115%	125%	100%	115%	125%	100%	115%	125%	100%	115%	125%	
Steel and Column Bearing	6'	10,598	11,202	11,551	15,897	16,804	17,326	21,196	22,405	23,101	33,300	36,685	38,743							
	7'	8,740	9,143	9,375	13,111	13,715	14,063	17,481	18,287	18,751	30,016	32,551	34,041							
	8'	7,270	7,553	7,716	10,905	11,330	11,574	14,539	15,106	15,432	26,655	28,499	29,565	35,540	37,998	39,420				
	9'	6,115	6,323	6,441	9,173	9,484	9,662	12,231	12,645	12,883	23,484	24,845	25,631	31,312	33,127	34,175				
	10'	5,203	5,359	5,449	7,805	8,039	8,173	10,407	10,718	10,897	20,667	21,703	22,300	27,556	28,937	29,733				
	12'	3,885	3,979	4,033	5,827	5,969	6,050	7,770	7,959	8,067	16,166	16,810	17,180	21,555	22,413	22,907				
	14'	3,003	3,064	3,099	4,504	4,596	4,649	6,005	6,129	6,199	12,893	13,320	13,566	17,190	17,760	18,088	34,168	35,796	36,736	
	16'										10,483	10,781	10,952	13,977	14,375	14,603	28,498	29,648	30,312	
	18'										8,673	8,890	9,013	11,565	11,853	12,018	24,027	24,871	25,356	
	20'										7,286	7,447	7,540	9,715	9,930	10,053	20,481	21,118	21,484	
	22'																17,638	18,131	18,413	
	24'																15,333	15,722	15,944	

General Notes

- Tables are based on:
 - Solid, one-piece column members used in dry-service conditions.
 - Bracing in both directions at column ends.
 - 425 psi for plate bearing.
 - NDS® 2001.
- Allowable loads accommodate axial loads only with ¼ column width/thickness eccentricity.

For Column Allowable Design Stresses see page 5.

Top or Bottom Plate Connection



The column and connector values listed are for dry-service conditions only. When wet-service conditions exist, contact your Trus Joist representative for other product solutions.

Appendix 3 – Alternate System #3

<p><u>Oneway concrete joist construction</u> - Reference: CRSI Design Handbook 2002</p> <p>- 30" Forms Used Span = 22'-8" LL = 40psf $l_n = 21'-8"$ → use 22' span DL = 12psf</p> <p><u>Superimposed Factored Loads</u>: For table use $1.4DL + 1.7LL$ $1.4(12psf) + 1.7(40psf) = 84.8psf$</p> <p><u>From Table on p. 8-22</u>: 12" Deep Rib + 3" top slab = 15" Total depth Endspan, $l_n = 22'$, 5" Rib @ 35" c.c. Tabulated capacity = 103psf Top bars #4@12" Bottom bars 2-#4 Wt of steel = 0.60psf</p> <p><u>From Table 8-1</u>: Slab wt = 63psf $l_n/18.5 = 14.3" < 15"$ No deflection calculation req'd</p> <p><u>From Table on p. 8-22</u>: 12" Deep Rib + 3" top slab = 15" total depth Interior span, $l_n = 22'$, 5" Rib @ 35" c.c. Tabulated capacity = 127psf Top bars #4@12" Bottom bars #3 & #4 Wt. of steel = 0.63psf</p> <p><u>From Table 8-1</u>: Slab wt = 63psf $l_n/21 = 12.57" < 15"$ ∴ No defl. calc. req'd.</p> <p><u>Girder Design</u>: To keep the repetitive design, the girders will be sized by calculating the width of the girder with the longest span and using the dimensions for all girders.</p> <p>$W_u = 1.2(12psf + 63psf) + 1.6(40psf) = 154psf$ $154psf(22') = 3388 lb/ft = 3.4 k/ft$ $M_u = \frac{wL^2}{8} = \frac{3.4k/ft(22')^2}{8} = 205.7'k$</p> <p>(1)</p>
--

$$\text{Assume } \rho = 0.6 \rho_{\max} = 0.6(0.0206) = 0.01236$$

$$\rho = \frac{A_s}{bd} \therefore A_s = \rho bd$$

$$a = \frac{\rho b d f_y}{0.85 f_c}$$

$$M_u = \phi M_n = 0.9 A_s f_y \left(d - \frac{a}{2} \right) = 0.9 \rho b d f_y \left(d - \frac{\rho d f_y}{0.85 f_c} \right)$$

$$205.7'k = 0.9 \rho b d^2 f_y \left(1 - \frac{\rho f_y}{0.85 f_c} \right) = 0.9(0.01236) b (15'')^2 (60 \text{ksi}) \left(1 - \frac{0.01236(60 \text{ksi})}{0.85(4 \text{ksi})} \right)$$

$$2468.4''k = 150.174(1 - 0.218) b$$

$$\therefore b = 21.02'' \rightarrow \text{use } \underline{b = 22''}$$

22x15 Girders

STANDARD ONE-WAY JOISTS (1) MULTIPLE SPANS		30" Forms + 5" Rib @ 35" c.-c. (2) FACTORED USABLE SUPERIMPOSED LOAD (PSF)										$f'_c = 4,000$ psi $f_y = 60,000$ psi	
12" Deep Rib + 3.0" Top Slab = 15.0" Total Depth													
TOP BARS	Size @	# 4 12	# 4 11	# 4 9	# 5 11	# 5 9.5	End Span Defl. Coeff. (3)	# 4 12	# 4 11	# 4 8.5	# 5 10.5	# 5 8.5	Int. Span Defl. Coeff. (3)
BOTTOM BARS	#	# 4 # 4	# 4 # 5	# 5 # 5	# 5 # 6	# 6 # 6		# 3 # 4	# 4 # 4	# 4 # 5	# 5 # 5	# 5 # 6	
Steel (psf)		.60	.72	.89	1.09	1.29		.63	.77	.97	1.22	1.48	
CLEAR SPAN		END SPAN					INTERIOR SPAN						
19'-0"		168	236	291*	301*	311*	1.525	201	285	334*	340*	350*	.939
		0	0	306	385	422*		0	0	384	485	532*	
20'-0"		143	205	267*	275*	283*	1.873	173	248	309*	314*	322*	1.153
		0	0	0	339	387*		0	0	338	429	481*	
21'-0"		121	177	234	253*	260*	2.276	149	217	286*	290*	298*	1.401
		0	0	0	299	365		0	0	298	381	432*	
22'-0"		103	154	205	233*	239*	2.742	127	190	264	269*	276*	1.687
		0	0	0	265	325		0	0	0	339	391*	
23'-0"		86	133	180	215*	221*	3.276	109	166	234	250*	257*	2.016
		0	0	0	235	290		0	0	0	303	357*	
24'-0"		72	115	158	199*	204*	3.884	93	145	208	233*	239*	2.390
		0	0	0	208	259		0	0	0	271	327*	
25'-0"		60	99	139	185*	189*	4.572	79	127	184	218*	223*	2.814
		0	0	0	0	232		0	0	0	243	301*	
26'-0"		48	85	122	164	176*	5.349	66	111	164	204*	209*	3.292
		0	0	0	0	207		0	0	0	218	278*	
27'-0"			72	107	146	164*	6.221	55	96	145	192*	196*	3.828
			0	0	0	186		0	0	0	195	253	
28'-0"			61	93	129	153*	7.195	45	83	129	175	184*	4.428
			0	0	0	167		0	0	0	0	229	
29'-0"			51	81	115	143*	8.279		72	114	158	173*	5.095
			0	0	0	149			0	0	0	207	
30'-0"			42	69	101	134	9.481		61	101	141	163*	5.835
			0	0	0	0			0	0	0	188	
31'-0"				59	89	120	10.810		52	89	127	153*	6.652
				0	0	0			0	0	0	170	
32'-0"				50	78	107	12.274		43	78	114	145*	7.553
				0	0	0			0	0	0	154	

(1) For gross section properties, see Table 8-1.
 (2) First load is for standard square joist ends; second load is for special tapered joist ends.
 (3) Computation of deflection is not required above horizontal line (thickness $\geq \ell_n/18.5$ for end spans, $\ell_n/21$ for interior spans).
 (4) Exclusive of bridging joists and tapered ends.
 *Controlled by shear capacity. +Capacity at elastic deflection = $\ell_n/360$.

PROPERTIES FOR DESIGN (CONCRETE .42 CF/SF) (4)												
NEGATIVE MOMENT												
STEEL AREA (SQ. IN.)	.58	.64	.78	.99	1.14		.58	.64	.82	1.03	1.28	
STEEL % (UNIFORM)	.69	.75	.92	1.17	1.36		.69	.75	.97	1.23	1.52	
(TAPERED)	.38	.42	.51	.65	.75		.38	.42	.54	.68	.84	
EFF. DEPTH, IN.	13.8	13.8	13.8	13.7	13.7		13.8	13.8	13.8	13.7	13.7	
-ICR/IGR	.176	.188	.220	.259	.287		.176	.188	.229	.268	.310	
POSITIVE MOMENT												
STEEL AREA (SQ. IN.)	.40	.51	.62	.75	.88		.31	.40	.51	.62	.75	
STEEL %	.08	.11	.13	.16	.18		.06	.08	.11	.13	.16	
EFF. DEPTH, IN.	13.8	13.7	13.7	13.6	13.6		13.8	13.8	13.7	13.7	13.6	
+ICR/IGR	.165	.205	.245	.288	.332		.130	.165	.205	.245	.288	

Appendix 4 – Alternate System #4

Light-Gauge Steel system - Reference: Marino Lightweight Steel Framing Catalog

First floor

Joists

Longest span = 25'

LL = 40 psf, TL = 52 psf

Try 12J14 joists @ 16" o.c.

LL = 46 psf > 40 psf

TL = 69 psf > 52 psf

Use 12J14 joists @ 16" o.c.

Header - Girder

Span 11'-4" → use 12'

LL = 40 psf · 21.5' (largest trib width) = 860 plf

TL = [52 psf + [(9 joists · 4.057 plf) / (16" · 1/12")]] · 21.5'

= 1706.77 plf

Try 16SW12 : TL = 1856 plf > 1706.77 plf

Use 16SW12

Masonry exterior bearing walls

Joist weight = 4.057 plf / (10" · 1/12") = 3.38 psf

Floor Height = 15' · 12"/1' = 180"

Height to thickness ratio = 180"/10" = 18

Try 10" CMU, ungrouted, unreinforced

Gross cross-sectional area = 93.1 in² (previously calculated in Appendix 2)

Design Load = 52 psf + 3.38 psf = 55.38 psf · $\frac{144 \text{ in}^2}{\text{ft}^2}$ = 7974.84 psi

7974.84 psi / 93.1 = 85.66 psi

Use 10" CMU, ungrouted, unreinforced @ 1500 psi compressive strength, type N mortar

100 psi > 87.9 psi

(1)

2nd & 3rd Floors

Joists

Longest Span = $30' - 6\frac{1}{2}'' \rightarrow$ use $31'$

LL = 40psf , TL = 52psf

Try 14JE10 @ $24''\text{o.c.}$

LL = $45\text{psf} > 40\text{psf}$

TL = $67\text{psf} > 52\text{psf}$

IN CORRIDOR

Use 6SN18 @ $24''\text{o.c.}$

Use 14JE10 joists @ $24''\text{o.c.}$

Studs of bearing walls use Wind Load = 20psf

Assume: $16''$ spacing & $18' - 4''$ tributary area (largest used)

Joist weight = $8.344\text{plf} / (24'' \cdot \frac{1}{12}'') = 4.172\text{psf}$

TL = $52\text{psf} + 4.172\text{psf} = 56.172\text{psf} \cdot [(16'' \cdot \frac{1}{12}'') (18.33')]$

= $1373.11\text{lb.} = 1.4\text{k}$

Floor Ht = $15'$

From Stud table (Axial Loads)

Try $3 - \frac{5}{8}''$ @ $16''\text{o.c.}$ (10 gauge)

interpolation: $3.4\text{k} > 1.4\text{k}$

Use $3 - \frac{5}{8}''$ studs @ $16''\text{o.c.}$

Header on all floors

Span: $31' - 8''$ Place column @ midspan where partition wall is & one $1'$ outside of wall to shorten span to $14'$

1st floor: TL = $[52\text{psf} + (11\text{ joists} \cdot 4.057\text{plf}) / (16'' \cdot \frac{1}{12}'')] \cdot 16.33'$

= 1395.7plf

Use 16SN10: $1766\text{plf} > 1395.7\text{plf}$

2nd & 3rd floors: TL = $[52\text{psf} + (7\text{ joists} \cdot 8.344\text{plf}) / (24'' \cdot \frac{1}{12}'')] \cdot 19.6'$

= 1591.6plf

Use 16SN10: $1766\text{plf} > 1591.6\text{plf}$



JOIST SPAS.F.

Floor and Roof Applications

Member MW Type (SMA)	Spans																														
	23'-0"	24'-0"	25'-0"	26'-0"	27'-0"	28'-0"	29'-0"	30'-0"	31'-0"	32'-0"	33'-0"	34'-0"	35'-0"	36'-0"																	
12" Members	ers																														
12J14 (1200S200-68)	121	118	79	104	69	92	61	82	55	73	49	66	44	59	39	12*	148	99	134	89	122	81	111	74	102	68	83	62	86	57	
12J12 (1200S200-97)	24*	59	59	78	52	69	46	61	41	55	37	49	33	44	29	16*	111	74	100	67	91	61	81	56	37	51	40	47	31	43	29
12J10 (1200S200-118)	12*	184	109	144	96	128	85	113	76	101	68	91	61	82	55	12*	100	67	91	61	83	55	75	50	69	46	63	42	58	39	
12JE16*	12*	133	82	108	72	96	64	85	67	76	51	68	45	61	41	18*	75	50	68	45	62	41	56	38	52	34	47	32	43	29	
12JE14	24*	62	55	72	48	64	43	57	38	51	34	45	30	41	27	24*	50	33	45	30	41	28	38	34	23	32	21	29	19		
12JE12	12*	200	153	176	117	156	104	138	92	123	82	111	74	100	66	12*	140	93	127	84	115	77	105	70	95	64	88	59	81	54	
12JE10	16*	150	100	132	88	117	78	104	69	93	62	83	55	75	50	18*	106	70	95	63	86	58	72	48	66	44	61	40	40	27	
12JE10	24*	100	67	88	59	78	52	69	46	62	41	55	37	50	33	24*	70	47	63	42	58	38	53	35	48	32	44	29	40	27	
12JE10	12*	84	71	78	62	71	65	66	49	61	44	57	39	53	35	12*	172	114	155	104	141	94	129	86	118	79	108	72	99	68	
12JE10	16*	63	53	58	47	54	41	50	37	46	33	43	29	40	28	16*	129	86	117	78	109	71	97	64	88	59	81	54	74	50	
12JE10	24*	42	35	39	31	36	28	33	24	31	22	28	20	25	18	24*	85	67	78	52	71	47	64	43	59	39	54	38	50	33	
12JE10	12*	123	88	113	77	103	68	91	61	82	54	72	49	66	44	12*	104	72	98	69	99	60	82	54	75	50	65	46	43	42	
12JE10	16*	92	66	85	58	77	61	88	46	61	41	55	37	49	33	18*	76	54	73	49	67	45	61	41	56	37	51	34	47	31	
12JE10	24*	62	44	47	39	51	34	46	30	41	27	37	24	33	22	24*	36	49	33	45	30	41	27	37	25	34	23	31	21		
12JE12	12*	183	122	161	108	143	95	127	85	113	76	102	68	91	61	12*	152	101	138	82	125	83	114	76	104	70	95	64	88	59	
12JE12	16*	137	92	121	81	107	71	99	48	16	114	76	103	69	94	53	86	57	78	52	72	48	66	44	62	48	36	44	29		
12JE10	24*	92	61	81	54	71	48	63	42	57	38	51	34	46	30	24*	76	51	69	46	63	42	57	38	52	35	48	32	44	29	
12JE10	12*	224	149	197	131	174	116	155	103	138	92	124	83	112	74	12*	186	124	169	113	154	102	140	93	128	85	117	78	108	72	
12JE10	16*	188	112	148	98	131	87	116	77	104	69	93	62	84	66	16*	140	83	127	84	115	77	105	70	96	64	88	59	81	54	
12JE10	24*	112	76	98	68	87	68	77	52	69	46	62	41	56	37	24*	83	62	84	60	77	51	70	47	64	43	59	39	54	38	
14" Members	bers																														
14J14 (1400S200-68)	12*	142	116	130	102	120	90	111	80	103	72	96	64	87	58	12*	84	71	88	65	83	59	78	54	73	49	67	45	62	41	
14J12 (1400S200-97)	16*	106	87	98	77	90	68	83	60	77	54	72	48	65	43	16*	71	63	80	48	62	44	58	40	55	37	50	34	46	31	
14J10 (1400S200-118)	24*	71	58	65	51	60	45	56	40	51	36	48	32	43	29	24*	47	36	44	32	41	29	39	27	37	24	34	22	31	21	
14JE12	12*	242	161	213	142	189	125	167	112	149	100	134	89	121	82	12*	153	102	139	92	126	84	115	77	105	70	96	64	89	59	
14JE10	16*	181	121	160	109	141	94	125	84	112	75	100	67	90	60	16*	115	77	104	69	95	63	86	58	70	53	72	48	66	44	
14JE10	24*	131	81	106	71	94	63	84	66	75	50	67	45	60	40	24*	77	51	69	46	63	42	58	38	53	35	46	32	44	30	
14J10	12*	285	197	260	173	230	153	204	136	182	122	164	108	147	98	12*	187	125	170	113	164	103	141	94	128	86	118	79	108	72	
14JE12	16*	221	149	195	130	172	115	153	102	137	91	123	82	110	74	16*	140	84	127	85	116	77	106	70	96	64	88	59	81	54	
14JE12	24*	148	98	130	87	115	77	102	68	91	61	82	55	74	49	24*	84	62	85	67	77	51	70	47	64	43	59	39	54	38	
14JE10	12*	280	179	236	157	209	139	186	124	166	110	149	99	134	89	12*	186	112	153	102	138	93	127	84	116	77	106	71	98	65	
14JE10	16*	195	134	177	118	157	104	139	93	124	83	111	74	100	67	16*	127	84	115	76	104	69	95	63	87	58	80	53	73	49	
14JE10	24*	130	89	118	79	104	70	93	62	83	55	74	50	67	45	24*	84	66	76	51	69	46	63	42	58	39	53	48	33	49	
14JE10	12*	328	219	289	192	255	170	227	151	203	135	182	121	184	109	12*	207	138	187	125	170	114	165	104	142	95	130	87	120	80	
14JE10	16*	246	164	217	144	192	128	170	114	152	101	136	91	123	82	16*	156	103	140	94	128	85	116	78	106	71	98	65	90	60	
14JE10	24*	184	109	144	96	128	85	114	76	101	68	91	61	82	55	24*	103	69	94	62	85	57	76	52	71	47	65	43	60	40	
14JX12	12*	307	207	272	182	242	161	215	143	192	128	172	115	165	103	12*	194	129	176	117	160	106	148	97	133	89	122	81	112	75	
14JX10	16*	230	155	205	137	181	121	161	107	144	96	129	86	116	77	16*	145	97	132	88	120	80	109	73	100	67	92	61	84	56	
14JX10	24*	153	103	137	91	121	81	107	72	95	64	88	57	77	52	24*	87	65	88	59	80	53	73	49	67	44	61	41	56	37	
14JXW10	12*	381	254	335	223	296	198	263	176	232	148	188	132	178	118	165	105	142	95	169	119	164	109	150	100	138	92	126	86		
14JXW10	16*	285	190	251	167	222	148	188	132	178	118	165	105	142	95	16*	119	108	142	98	134	86	123	82	112	75	103	69	90	60	
14JXW10	24*	190	127	187	112	148	99	132	88	118	78	105	70	95	63	24*	79	108	127	88	120	85	115	80	92	55	75	50	68	46	
14JXW10	12*	309	225	284	188	262	175	233	155	208	139	187	124	188	112	12*	204	140	190	127	173	115	167	105	144	96	132	88	121	81	
14JXW10	16*	232	168	213	148	196	131	175	117	156	104	140	93	126	84	16*	153	105	142	95	129	86	118	79	108	72	99	68	91	61	
14JXW10	24*	165	112	142	98	131	87	117	76	104	69	93	62	84	66	24*	70	95	63	86	56	70	52	72	48	66	44	61	40		
14JXW10	12*	414	276	368	243	322	215	288	191	268	170	239	163	208	138	12*	257	172	233	156	212	141	193	129	177	118	162	108	149	99	
14JXW10	16*	310	207	272	182	242	161	215	143	192	128	172	115	165	103	16*	193	130	175	117	160	106	145	97	133	89	122	81	112	74	
14JXW10	24*	207	138	182	121	161	107	143	95	125	85	115	76	103	68	24*	126	86	117	78	108	71	97	64	88	59	81	54	74	50	

* = Exceeds the H/T ratio of 200

L = Live Load



HEADERS, P.L.F.

Header	MW / Type	3MA	4FT	5FT	6FT	7F	8T	5FT	0FT	11FT	12FT	13T	1FT	5FT	16FT	17F	18T	1FT	10FT	21FT	22F	23T	2FT	5FT	26FT	27FT	28T	2FT	10FT													
3-5/8" Members																																										
358	SW20	36	5102	42	233	106	137	9	47	35	27	2	7	14	11																											
358	SW18	36	5102	14	303	273	175	19	81	46	35	2	7	18	15																											
358	SW16	36	5102	110	502	349	225	17	103	76	57	44	3	22	18																											
358	SW14	36	5102	158	741	429	271	31	177	93	70	54	4	48	42																											
358	SW12	36	5102	285	1093	577	354	25	313	125	64	72	6	87	80																											
358	SW10	36	5102	539	1754	885	432	27	553	148	111	85	6	164	159																											
6" Members																																										
6	W20	60	5102	3	36	608	422	310	27	88	152	118	91	40	38																											
6	W18	60	5102	3	36	609	657	415	379	51	202	152	117	4	40																											
6	W16	60	5102	3	36	608	1028	628	461	43	250	188	145	1	4																											
6	W14	60	5102	3	36	607	1415	795	511	53	300	211	126	12	12																											
6	W12	60	5102	3	36	607	1923	1123	616	53	305	211	126	12	12																											
6	W10	60	5102	3	36	605	2727	1446	691	60	353	218	25	13	13																											
8" Members																																										
8	W20	80	5102	3	36	609	654	407	37	48	200	165	136	1	89																											
8	W18	80	5102	3	36	609	1077	472	46	72	305	252	212	1	85																											
8	W16	80	5102	3	36	607	1511	626	46	72	420	328	212	1	85																											
8	W14	80	5102	3	36	607	2020	733	46	72	531	400	305	2	85																											
8	W12	80	5102	3	36	607	2837	1005	46	72	642	460	305	2	85																											
8	W10	80	5102	3	36	605	3877	2553	197	145	865	481	313	50	252																											
8	W10	80	5102-1	3	36	600	4878	3348	238	187	1024	770	595	41	73																											
10" Members																																										
10	W18	100	5102	3	36	609	657	472	47	72	324	297	225	2	80																											
10	W16	100	5102	3	36	609	1105	507	46	72	454	397	297	2	80																											
10	W14	100	5102	3	36	607	1511	626	46	72	554	400	297	2	80																											
10	W12	100	5102	3	36	607	2020	733	46	72	642	460	305	2	80																											
10	W10	100	5102	3	36	605	2837	1005	46	72	800	518	305	2	80																											
10	W10	100	5102-1	3	36	600	3877	2553	197	145	1041	770	595	2	80																											
12" Members																																										
12	W18	120	5102	3	36	609	657	472	47	72	324	297	225	2	80																											
12	W16	120	5102	3	36	609	1105	507	46	72	454	397	297	2	80																											
12	W14	120	5102	3	36	607	1511	626	46	72	554	400	297	2	80																											
12	W12	120	5102	3	36	607	2020	733	46	72	642	460	305	2	80																											
12	W10	120	5102	3	36	605	2837	1005	46	72	800	518	305	2	80																											
12	W10	120	5102-1	3	36	600	3877	2553	197	145	1041	770	595	2	80																											
14" Members																																										
14	W14	140	5102	3	36	609	657	472	47	72	324	297	225	2	80																											
14	W12	140	5102	3	36	609	1105	507	46	72	454	397	297	2	80																											
14	W10	140	5102	3	36	607	1511	626	46	72	554	400	297	2	80																											
14	W10	140	5102-1	3	36	600	2837	1005	46	72	800	518	305	2	80																											
16" Members																																										
16	W14	160	5102	3	36	609	657	472	47	72	324	297	225	2	80																											
16	W12	160	5102	3	36	609	1105	507	46	72	454	397	297	2	80																											
16	W10	160	5102	3	36	607	1511	626	46	72	554	400	297	2	80																											
16	W10	160	5102-1	3	36	600	2837	1005	46	72	800	518	305	2	80																											

The values presented in this chart are calculated for (C) of eoc (member) standard. * = E exceeds the H/T ratio of 200

AXIAL LOAKIPS



Allowable Axial Loads		Wind Load = 5psf												Wind Load = 15psf																							
		Members												Members																							
Height	Spacing	MarinoWare - (SSMA)												MarinoWare - (SSMA)																							
		3-5/8SW-gauge - (362S162-mils)			3-5/8J-gauge - (362S200-mils)			10-(118)			14-(68)			16-(54)			20-(33)			3-5/8SW-gauge - (362S162-mils)			3-5/8J-gauge - (362S200-mils)			10-(118)			14-(68)			16-(54)			20-(33)		
		20-(33)	33ksi	50ksi	16-(54)	33ksi	50ksi	14-(68)	33ksi	50ksi	10-(118)	33ksi	50ksi	12-(97)	33ksi	50ksi	10-(118)	33ksi	50ksi	12-(97)	33ksi	50ksi	16-(54)	33ksi	50ksi	14-(68)	33ksi	50ksi	16-(54)	33ksi	50ksi	14-(68)	33ksi	50ksi			
8ft.	12"	2.09	2.85	4.25	5.45	7.82	9.85	2.49	3.51	5.34	6.76	9.49	11.75	1.69	2.50	4.28	5.45	7.82	9.85	2.11	3.33	5.34	6.76	9.49	11.75	1.69	2.50	4.28	5.45	7.82	9.85	2.11	3.33	5.34	6.76	9.49	11.75
	16"	2.09	2.85	4.25	5.45	7.82	9.85	2.49	3.51	5.34	6.76	9.49	11.75	1.69	2.50	4.28	5.45	7.82	9.85	2.11	3.33	5.34	6.76	9.49	11.75	1.69	2.50	4.28	5.45	7.82	9.85	2.11	3.33	5.34	6.76	9.49	11.75
	24"	2.09	2.85	4.25	5.45	7.82	9.85	2.49	3.51	5.34	6.76	9.49	11.75	1.69	2.50	4.28	5.45	7.82	9.85	2.11	3.33	5.34	6.76	9.49	11.75	1.69	2.50	4.28	5.45	7.82	9.85	2.11	3.33	5.34	6.76	9.49	11.75
	12"	2.02	2.75	4.05	5.12	7.32	9.18	2.41	3.37	5.03	6.33	8.85	10.92	1.63	2.50	4.06	5.12	7.32	9.18	2.04	3.19	5.03	6.33	8.85	10.92	1.63	2.50	4.06	5.12	7.32	9.18	2.04	3.19	5.03	6.33	8.85	10.92
9ft.	12"	1.98	2.72	4.05	5.12	7.32	9.18	2.32	3.37	5.03	6.33	8.85	10.92	1.63	2.50	4.06	5.12	7.32	9.18	2.04	3.19	5.03	6.33	8.85	10.92	1.63	2.50	4.06	5.12	7.32	9.18	2.04	3.19	5.03	6.33	8.85	10.92
	16"	1.92	2.65	3.79	4.79	6.76	8.44	2.25	3.22	4.68	5.85	8.15	10.33	1.37	2.17	3.85	4.76	6.76	8.44	1.71	2.80	4.30	5.45	7.82	9.85	1.37	2.17	3.85	4.76	6.76	8.44	1.71	2.80	4.30	5.45	7.82	9.85
	24"	1.87	2.54	3.79	4.79	6.76	8.44	2.25	3.22	4.68	5.85	8.15	10.33	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	12"	1.79	2.51	3.48	4.35	6.15	7.65	2.21	3.05	4.31	5.35	7.43	9.11	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
10ft.	12"	1.69	2.44	3.48	4.35	6.15	7.65	2.09	3.05	4.31	5.35	7.43	9.11	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	16"	1.60	2.39	3.43	4.35	6.15	7.65	1.80	2.79	4.31	5.35	7.43	9.11	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	24"	1.50	2.33	3.17	4.05	5.63	6.83	1.82	2.74	4.31	5.35	7.43	9.11	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	12"	1.45	2.17	3.17	3.95	5.53	6.83	1.82	2.74	4.31	5.35	7.43	9.11	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
12ft.	16"	1.30	1.89	2.95	3.65	5.33	6.53	1.54	2.43	3.75	4.52	6.87	8.15	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	24"	1.20	1.80	2.85	3.55	5.23	6.43	1.54	2.43	3.75	4.52	6.87	8.15	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	12"	1.21	1.61	2.59	3.23	4.47	5.44	1.53	2.29	3.18	3.92	5.39	6.54	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	16"	1.09	1.60	2.44	3.17	4.47	5.44	1.35	2.10	3.09	3.92	5.39	6.54	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
14ft.	12"	0.80	1.35	2.17	2.80	3.64	4.39	1.12	1.74	2.48	3.21	4.39	5.30	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	16"	0.73	1.20	1.84	2.41	3.52	4.37	0.95	1.52	2.32	3.06	4.39	5.30	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	24"	0.81	1.21	1.84	2.41	3.52	4.37	0.95	1.52	2.32	3.06	4.39	5.30	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	12"	0.91	1.21	1.84	2.41	3.52	4.37	0.95	1.52	2.32	3.06	4.39	5.30	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
16ft.	12"	1.11	1.60	2.44	3.17	4.47	5.44	1.35	2.10	3.09	3.92	5.39	6.54	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	16"	1.09	1.60	2.44	3.17	4.47	5.44	1.35	2.10	3.09	3.92	5.39	6.54	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	24"	1.09	1.60	2.44	3.17	4.47	5.44	1.35	2.10	3.09	3.92	5.39	6.54	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78
	12"	1.11	1.60	2.44	3.17	4.47	5.44	1.35	2.10	3.09	3.92	5.39	6.54	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78	1.11	1.93	3.24	4.15	6.14	7.78	1.00	1.80	3.19	4.15	6.14	7.78

(2) = L/240 (3) = /600

Appendix 5 – Tables used in Masonry design

Table 1—Wall Lateral Support Requirements (ref. 1)		Table 3—Allowable Compressive Stress for Empirical Design of Masonry (ref. 1)		
Construction	Maximum wall length-to thickness or height-to thickness ratio ^(a)	Allowable compressive stresses based on gross cross-sectional area, psi (MPa) ^(a)		
		Gross area compressive strength of unit, psi (MPa)	Type M or S mortar	Type N mortar
Bearing walls		Solid concrete brick:		
Solid or solid grouted	20	8000 (55) or greater	350 (2.41)	300 (2.07)
All other	18	4500 (31)	225 (1.55)	200 (1.38)
Nonbearing walls		Grouted concrete masonry:		
Exterior	18	2500 (17)	160 (1.10)	140 (0.97)
Interior	36	1500 (10)	115 (0.79)	100 (0.69)
Cantilever Walls^(b)		Solid concrete masonry units:		
Solid	6	4500 (31) or greater	225 (1.55)	200 (1.38)
Hollow	4	2500 (17)	160 (1.10)	140 (0.97)
Parapets (8-in. (203-mm) thick min.)^(b)		1500 (10)	115 (0.79)	100 (0.69)
		Hollow concrete masonry units:		
		2000 (14) or greater	140 (0.97)	120 (0.83)
		2000 (14)	115 (0.79)	100 (0.69)
		1200 (8.3)	75 (0.52)	70 (0.48)
		700 (4.8)	60 (0.41)	55 (0.38)
		Hollow walls (noncomposite masonry bonded^(b))		
		solid units:		
		2500 (17) or greater	160 (1.10)	140 (0.97)
		1500 (10)	115 (0.79)	100 (0.69)
		hollow units		
			75 (0.52)	70 (0.48)
		^(a) Linear interpolation for intermediate values of compressive strength is permitted.		
		^(b) Where floor and roof loads are carried on one wythe, the gross cross-sectional area is that of the wythe under load; if both wythes are loaded, the gross cross-sectional area is that of the wall minus the area of the cavity between the wythes. Walls bonded with metal ties shall be considered as noncomposite walls unless collar joints are filled with mortar or grout.		

Table 2—Maximum Wall Spans, ft (m)				
Wall thickness, in. (mm)	6 (152)	8 (203)	10 (254)	12 (305)
Bearing walls				
Solid or solid grouted	10 (3.0) ^(a)	13.3 (4.1)	16.6 (5.1)	20 (6.1)
All other	9 (2.7) ^(a)	12 (3.7)	15 (4.5)	18 (5.5)
Nonbearing walls				
Exterior	9 (2.7)	12 (3.7)	15 (4.5)	18 (5.5)
Interior	18 (5.5)	24 (7.3)	30 (9.1)	36 (11)
Cantilever Walls^(b)				
Solid	3 (0.9)	4 (1.2)	5 (1.5)	6 (1.8)
Hollow	2 (0.6)	2.6 (0.8)	3.3 (1.0)	4 (1.2)
Parapets ^(b)	1.5 (0.5)	2 (0.6)	2.5 (0.8)	3 (0.9)
^(a) 6-in. (152-mm) thick bearing walls are limited to one story in height.				
^(b) For these cases, spans are maximum wall heights.				

Reference: Beavertown Block Company (www.ncma.org/etek/index.cfm)