## Overlook Towers

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Technical Assignment 1

October 5, 2006

Anthony Perrotta - Structural Option
Overlook Towers - Herndon, VA
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## Table of Contents

Executive Summary: ..... 2 -
Structural System ..... 3 -
Building Codes: ..... - 4 -
Foundation: ..... - 4 -
Elevated Floor System: ..... - 4 -
Columns: ..... - 4 -
Lateral System: ..... - 5 -
Appendix A - Dead Load ..... $6-$
Appendix B - Wind Load ..... 8 -
Appendix C - Snow Load. ..... -9-
Appendix D - Seismic Load ..... -9-
Appendix E - Spot Checks ..... - 10 -


## Executive Summary:

This assignment takes a look at the structural system of Overlook Towers. This nine story office building is one of three buildings in the complex. There are two nine story office buildings and a five story parking deck. The flooring is a lightweight concrete composite deck system which is supported by a steel structure. The exterior of the building is a curtain wall and precast concrete panel system. Wind loads are carried and transferred by a central lateral bracing system.

Wind, seismic and snow loads are calculated in the appendices. These calculations follow the building codes used for designing the structure, IBC 2000. Spot checks are also performed at various places in the building. Included in the spot check is a typical beam and girder check along with lateral loading due to wind forces on a column.

October 5, 2006


## Structural System:

Overlook Towers is a nine story steel office building located just outside of Washington D.C. The superstructure is composed mostly of structural steel with composite deck and slab system. The general layout of each office building is eight bays spaced approximately thirty feet on center in the east-west direction. In the opposite direction are four bays spaced from about fourteen feet through thirty-three feet. The central core of the building is where the major lateral supporting frames are located. These frames contain the elevators and stairways. The roofing system is a series of flat steel trusses supporting a rooftop penthouse, which is where all of the major mechanical equipment is located. The overall dimensions of the building are about $220^{\prime}$ by $125^{\prime}$.

## Typical Framing Plan:




## Building Codes:

The building loads are designed in accordance with the 2000 International Building Code with local adjustments.

Live Loads: Flat Roof Snow Load - 21 psf
Ground Snow Load - 30 psf
Office Load - 100 psf
Permanent Corridor - 100 psf
Lobbies/stairs - 100 psf
Mechanical - 125 psf
Storage Space - 125 psf
Dead Loads: Mechanical and Ceiling - 5 psf
Single-ply roof - 11 psf

## Foundation:

The foundation uses normal weight 3,000 psi concrete for the footings and pilasters and normal weight 4,000 psi concrete for the five inch thick slab on grade. The foundation has been designed for $20,000 \mathrm{psf}$ at a bearing depth of $2^{\prime}-6^{\prime \prime}$. Below the slab is a vapor barrier lying on top of a 4 " layer of crushed stones. Expansion joints for the slab are to be at every column line. The steel reinforcing is grade 60 ASTM A 615 bars.

## Elevated Floor System:

Elevated floor slabs are made of $6 \frac{1}{4}$ " thick structural lightweight concrete. The slab is reinforced with $6 \times 6-\mathrm{W} 1.4 \times \mathrm{W} 1.4$ welded wire fabric. Working with the slab is an 18 gauge three inch deep composite steel deck. The slab is designed so that no shoring is required for construction. The concrete is required to have a design strength of 4000 psi after curing. Supporting the decks are ASTM 992 wide flange beams. The typical interior beam size is a W24x55 which has a span of $46^{\prime}$. The beams are spaced at a typical distance of $12^{\prime}-6^{\prime \prime}$. The floors are designed to carry a load of 100 psf for the office space and is also designed for a concentrated load of 2000 pounds on a $21 / 2$ foot square area.

## Columns:

The columns around the exterior of the building have an average spacing of 30 feet. The largest columns stand 40 feet. This size column is used up to the sixth floor where the height changes to about 25 feet. The columns are spliced at a typical height of three feet above the floor slab.


## Lateral System:

The lateral system of Overlook Towers is a series of braced frames located in the center of the building. Inside of the frames forms a core of the building where there are four elevator shafts, each leading to the ninth floor.

As you can see in the illustration to the right, the frames consist of W -shapes for the column support and HSS shapes are used for the lateral bracing. This layout is similar in all four of the frame types. Most of the differences from frame to frame is the size of the members.

- 1 of 4 Interior Frames



## Appendices:

A. Dead Load Calculations<br>B. Wind Calculations<br>C. Snow Load<br>D. Seismic Load<br>E. Spot Check

## Appendix A - Dead Load

Floor Slab Weight: Lightweight concrete - $112 \mathrm{pcf} \times 31 / 4$ " slab $=31.1 \mathrm{psf}$ 18 gauge steel decking -4 psf Mechanical \& Ceiling - 5 psf
Allowance - 15 psf
Total: $55.1 \mathrm{psf} \rightarrow 60 \mathrm{psf}$ dead load for floor slab alone.
The following calculation takes into account the dead load for the structural system of the building along with some mechanical allowances. Items such as the mechanical equipment and lighting system were omitted because these weights are relatively small compared to the total weight of the building. Also the roof trusses were omitted for the fact that not enough information was available at this time.

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## Dead Load Calculations

## Second Floor



Floors 3-9

| Member | Weight (plf) | Length(ft) | Qty/fl. | Floors | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
| W21x44 | 44 | 30 | 10 | 7 | 92.40 kip |
| W24x55 | 55 | 46 | 26 | 7 | 460.46 kip |
| W24x55 | 55 | 30 | 25 | 7 | 288.75 kip |
| W18x35 | 35 | 30 | 14 | 7 | 102.90 kip |
| W18x40 | 40 | 30 | 2 | 7 | 16.80 kip |
| W16x26 | 26 | 13 | 4 | 7 | 9.46 kip |
| W12x14 | 14 | 8 | 4 | 7 | 3.14 kip |
| W10x15 | 15 | 7.75 | 4 | 7 | 3.26 kip |
| W24x68 | 68 | 45 | 4 | 7 | 85.68 kip |
|  |  |  | SUM |  | 1,062.85 kip |

## Floor Slab

| area(sf) | weight(psf) | Floors |  | Total | 14,000 kip |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 25000 | 70 | 8 |  |  |  |
| Columns |  |  |  |  |  |
| Member | Weight(plf) | Length (ft) | Qty. |  | Total |
| W12x58 | 58 | 40.5 | 4 |  | 9 kip |
| W12x65 | 65 | 40.5 | 4 |  | 11 kip |
| W12x96 | 96 | 40.5 | 4 |  | 16 kip |
| W12x106 | 106 | 40.5 | 4 |  | 17 kip |
| W12x87 | 87 | 40.5 | 8 |  | 28 kip |
| W12x136 | 136 | 40.5 | 1 |  | 6 kip |
| W12x40 | 40 | 27 | 4 |  | 4 kip |
| W12x50 | 50 | 27 | 4 |  | 5 kip |
| W12x65 | 65 | 27 | 7 |  | 12 kip |
| W12x53 | 53 | 27 | 8 |  | 11 kip |
| W12x87 | 87 | 27 | 1 |  | 2 kip |
| W12x40 | 40 | 24 | 24 |  | 23 kip |
| W12x65 | 65 | 37.5 | 1 |  | 2 kip |
|  |  |  |  | SUM | 148 kip |
|  |  |  |  |  |  |
|  | Total Dead Load: |  |  |  | 15,354 kip |

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## Appendix B - Wind Load

| Basic Wind Speed Importance Factor | $\begin{aligned} \mathrm{V} & =90 \mathrm{mph} \\ \mathrm{I} & =1.0 \end{aligned}$ |  |  | Exposure B |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wal | alculation |  |  |
| Height | k | q | Windward | Leeward | Net Load |
| 0-15 | 0.57 | 10.08 | 8.82 | 5.08 | 13.90 |
| 20 | 0.62 | 10.96 | 9.35 | 5.21 | 14.56 |
| 25 | 0.66 | 11.67 | 9.77 | 5.32 | 15.09 |
| 30 | 0.7 | 12.38 | 10.19 | 5.42 | 15.61 |
| 40 | 0.76 | 13.44 | 10.82 | 5.59 | 16.41 |
| 50 | 0.81 | 14.32 | 11.35 | 5.72 | 17.07 |
| 60 | 0.85 | 15.03 | 11.77 | 5.83 | 17.59 |
| 70 | 0.89 | 15.74 | 12.19 | 5.93 | 18.12 |
| 80 | 0.93 | 16.44 | 12.61 | 6.04 | 18.65 |
| 90 | 0.96 | 16.97 | 12.93 | 6.12 | 19.05 |
| 100 | 0.99 | 17.50 | 13.24 | 6.20 | 19.44 |
| 120 | 1.04 | 18.39 | 13.77 | 6.34 | 20.10 |
| 140 | 1.09 | 19.27 | 14.29 | 6.47 | 20.76 |

13.98



## Appendix C-Snow Load

$\mathrm{p}_{\mathrm{f}}=0.7\left(\mathrm{C}_{\mathrm{e}} \mathrm{C}_{\mathrm{t}} \mathrm{I} \mathrm{p}_{\mathrm{g}}\right)=0.7(30)=21 \mathrm{psf}$ roof load

$$
\mathrm{C}_{\mathrm{e}}=1.0 \quad \mathrm{C}_{\mathrm{t}}=1.0 \quad \mathrm{I}=1.0 \quad \mathrm{p}_{\mathrm{g}}=30 \mathrm{psf}
$$



## Appendix D-Seismic Load

Section 1613.0 IBC 2000
$\mathrm{S}_{\mathrm{s}}=0.20 \mathrm{~g}$
$\mathrm{S}_{1}=0.08 \mathrm{~g}$
$\mathrm{S}_{\mathrm{DS}}=0.16 \mathrm{~g}$
$S_{D 1}=0.09 \mathrm{~g}$
Site Class:
C
Seismic Use Group: I
Importance Factor:
1.0
Design Category:
B

Calculations based on the equivalent lateral force method.

$$
\begin{aligned}
& C_{s}=\frac{S_{D S}}{R / I}=\frac{0.160}{3.0 / 1.0}=0.053 \\
& C_{s}>0.044 S_{D S} I=0.044(0.16) 1.0=0.00704 \\
& C_{s} \leq \frac{S_{D 1}}{T(R / I)}=\frac{0.09}{0.864(3.0 / 1.0)}=0.0347
\end{aligned}
$$

$$
\therefore C_{s}=0.0347
$$

$$
\mathrm{V}=\mathrm{C}_{\mathrm{s}} * \mathrm{~W}=0.0347\left(15,354^{\mathrm{k}}\right)=533.1^{\mathrm{k}}
$$



## Appendix E-Spot Checks



## Typical Frame Check:

> L.L. $=100 \mathrm{psf}$ (office space)
> D.L. $=60 \mathrm{psf}$

Beam: W18x35

$$
\begin{aligned}
& \mathrm{w}_{\mathrm{u}}=1.6(100)+1.2(60)=232 \mathrm{psf} \\
& M_{u}=\frac{.232(10) 30^{2}}{8}=261^{\mathrm{ft}-\mathrm{k}} \\
& V_{u}=\frac{.232(10) 30}{2}=34.8^{\mathrm{k}}
\end{aligned}
$$

Girder: W24x55 (tributary width $=38^{\prime}$ )

$$
\begin{aligned}
& M_{u}=\frac{.232(38) 30^{2}}{8}=992^{\mathrm{ft}-\mathrm{k}} \\
& V_{u}=\frac{.232(38) 30}{2}=132^{\mathrm{k}}
\end{aligned}
$$

Composite Deck: 18 Ga. $61 / 4$ "Lightweight Concrete Steel Decking
$\mathrm{w}_{\mathrm{uL}}=120 \mathrm{psf}$
$\mathrm{f}_{\mathrm{c}}{ }^{\prime}=4000 \mathrm{psi}$
From United Steel Deck Catalog: w = $122.5 \mathrm{psf}>120 \mathrm{psf}$ live load.
Max. unshored span - 13.26,
The composite decking is ok. The drawings call for no shoring and the maximum span is $12^{\prime}-8^{1 / 4 \prime \prime}$, this is also allowable.

