

TECHNICAL REPORT II

STRUCTURAL STUDY OF ALTERNATE FLOOR SYSTEMS



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EXECUTIVE SUMMARY

Technical Report II will investigate alternative solutions for the floor system of Layfield Tower. The report will give preliminary sizes of members, depths, and other pertinent information about each system. Figures from handbooks are present as well as hand calculations and tables.

The four systems analyzed were the current composite steel, non-composite steel, hollow core plank on steel members, and a two-way flat plate with drop panels. From analyzing and evaluating these it was found that the hollow core plank does not work well for this project and will no longer be considered. The non-composite and two-way flat plate systems were found to be feasible solutions and have warranted further consideration. The existing system appears to be the most suitable for this building.



INTRODUCTION

The Layfield Tower is part of an expansion and renovation project at Peninsula Regional Medical Center. It is located at 100 East Carroll Street in Salisbury, MD. It is a 200,000 square foot facility that will house a new emergency/trauma center, pediatric unit, intensive care unit, cardiac and thoracic and vascular unit and a neurosciences and stroke unit. The building also features a helipad on the lower roof with access to the third floor of the main tower. There is a connection to the existing hospital at the northeast corner. Construction on Layfield Tower was completed in 2008.

The structure is divided into two parts: the east side (Area A) with three stories and the west (Area B) with one story. An expansion joint connects the two sections of the building.

This report will evaluate and compare different structural floor systems for the building. First is an analysis and evaluation of the existing system: composite steel frame construction. Then alternate systems were evaluated: two-way flat-plate reinforced concrete, non-composite steel frame, and pre-stressed concrete hollow core plank on steel beams.

LOADS

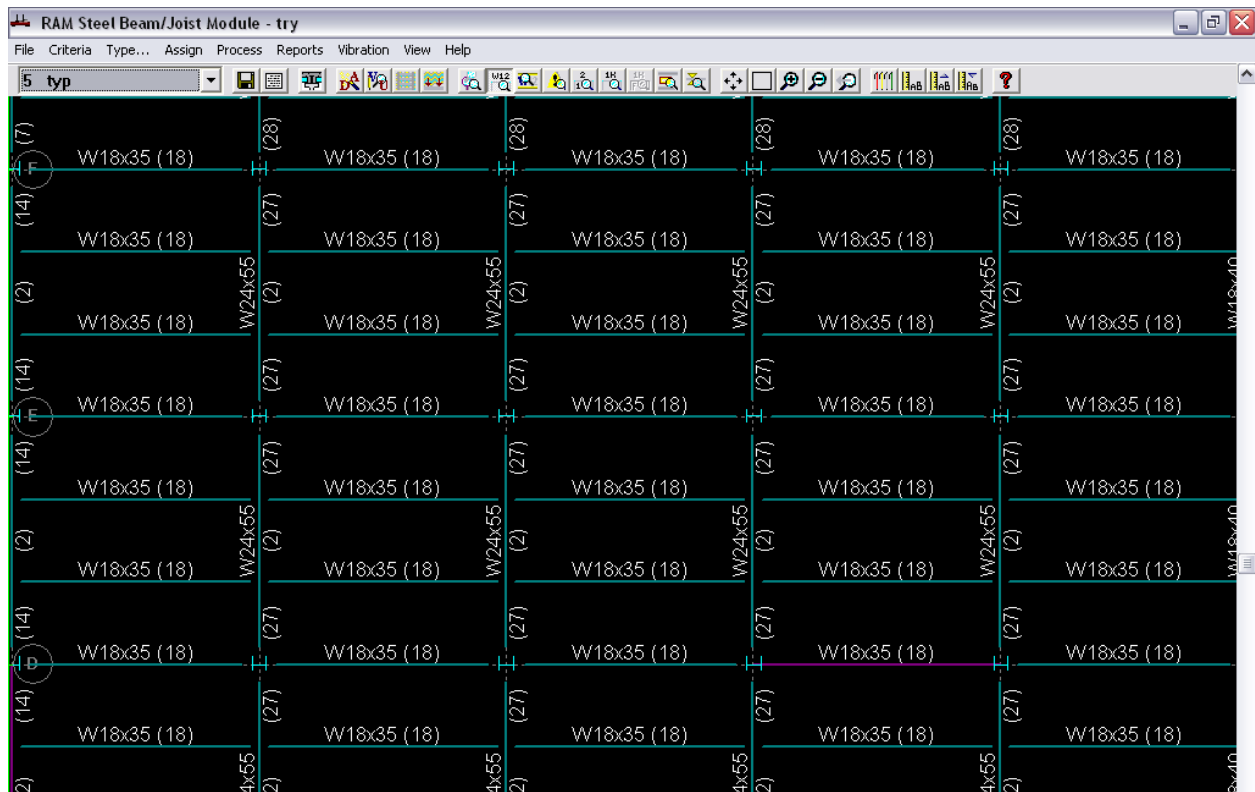
Floor Area	Dead Load (psf)
Partitions	20
Suspended Ceilings	3
Ductwork and Piping	5
Lights	2
Sprinklers	2
Fireproofing	2
Structural Steel Framing	8
6 1/4" Floor Slab (LW)	47
Hanging Load in Mechanical Rooms	65

Floor Area	Live Load (psf)
Elevator Penthouse	150
Mechanical Rooms	15
Office Areas	50
Toilets	60
Corridors	80
Minimum for Design	80

EXISTING STRUCTURAL SYSTEM

Description

The current structural system is made up of structural steel W-shape members. Most connections are shear connections. The typical beam size is W18x35 spaced at 10'-0" on center. Girders are typically W24X55. The typical bay size is 30'-0" x 30'-0". Shown below is a typical floor layout.



Floor slabs are 3-1/4" lightweight concrete on 3" deep 20 gage, galvanized composite metal deck for a total thickness of 6-1/4". They are reinforced with 6x6 W2.1xW2.1 welded wire fabric. All shear studs are 3/4" x 5 3/16".

Analysis

An analysis was run using Ram to design the typical members. Only gravity forces were used while wind and seismic were not considered. The analysis produced matching member sizes to the original plans.

Evaluation

Pros

Durable
Speed of construction
Light Weight

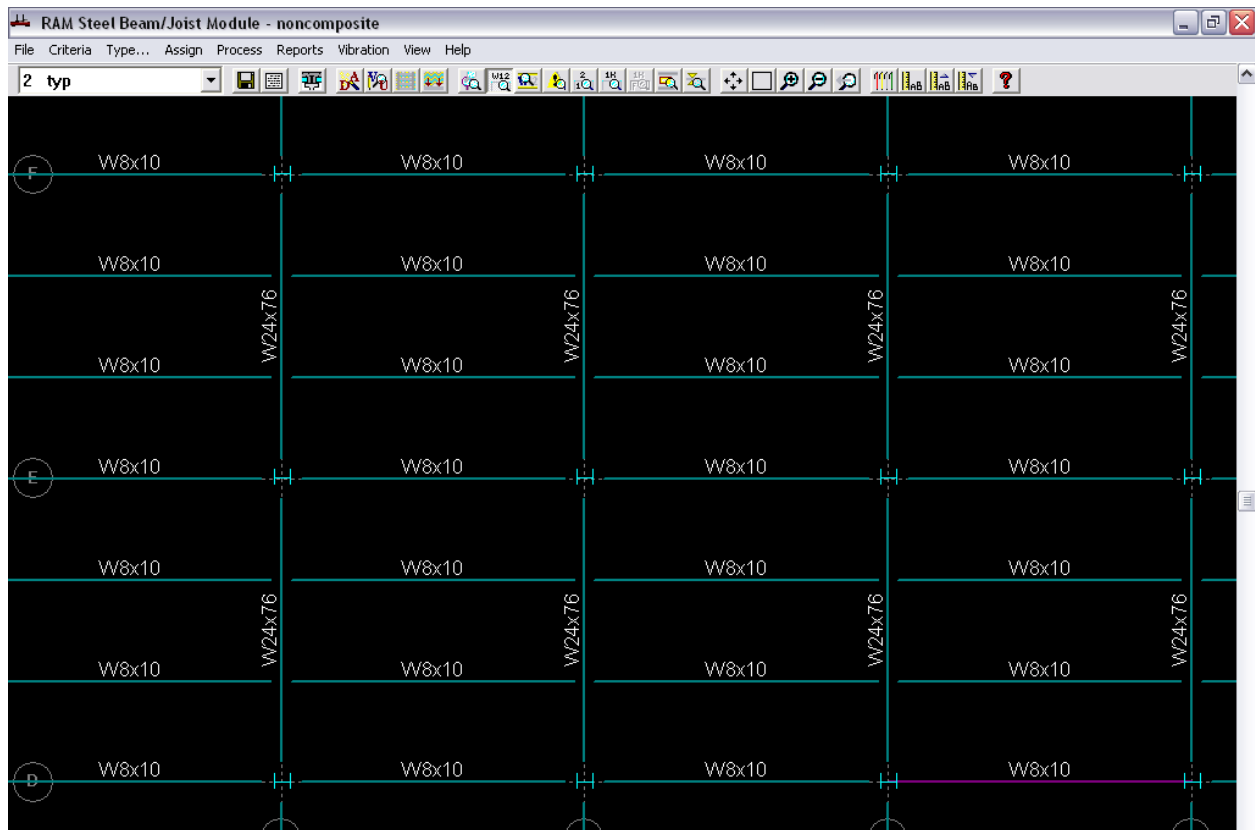
Cons

Spray-on Fireproofing required

ALTERNATE SYSTEM 1: Non-Composite Steel

Description

The non-composite structural steel system is made up of structural steel W-shape members. The typical beam size is W8x10 with spaced at 10'-0" on center. Girders are typically W24x76. The typical bay size is 30'-0" x 30'-0". Shown below is a typical floor layout.



Analysis

For this system Ram was again used to find member sizes. Beams were found to be similar to the original design but need camber and girders increased to W24x76. This system consists of a 3" lightweight concrete slab placed on 20 gage 2" high x 6-1/8" pitch x 24-1/2" wide Versa-Deck S.

Evaluation

Pros	Cons
Durable	Spray-on Fireproofing required
Speed of construction	Susceptible to vibration
Light Weight	Increase in floor depth

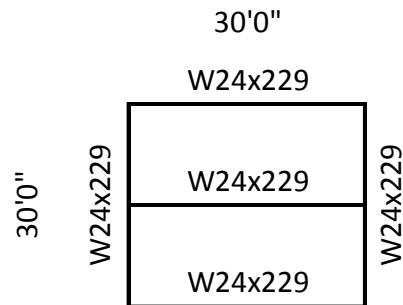
ALTERNATE SYSTEM 2: Hollow Core Plank

Description

Hollow core planking is a type of precast concrete system. The planks are cast in long lengths and cut to size to accommodate the project. The hollow cores can be filled with grout for added strength if need be. A topping slab may also be added for either structural purposes or strictly leveling. For this system, the precast will be supported by structural steel members. The system analyzed has a two-inch topping for both structural integrity and to ensure the floor is level. The Nitterhouse Concrete Products website provided free specifications and details for their typical planks.

Analysis

Based upon the factored loads and spans the hollow core plank chosen using the Nitterhouse specifications was 6" x 4'0" with 4 ½"φ 270K strands. This system was analyzed with beams spaced at 15'0" on center instead of 10'0". Beams and girders were found to be W24x229 to optimize floor depth.



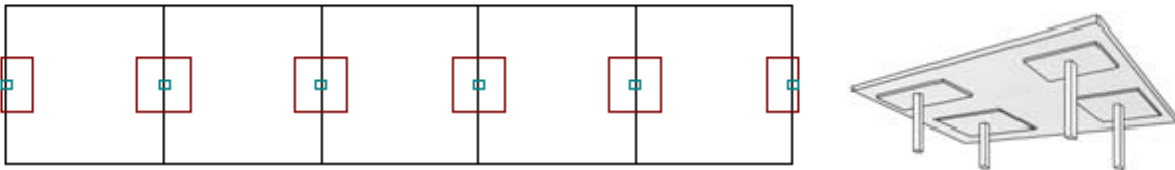
Evaluation

Pros	Cons
Durable	Spray-on Fireproofing required
Speed of construction	Susceptible to vibration
	Increase in floor depth
	High weight

ALTERNATE SYSTEM 3: Two-Way Flat Plate with Drop Panels

Description

This is a cast-in-place reinforced concrete two-way flat plate system with drop panels at column locations. It consists of a 10" slab and 8.5" drop panels. Although lateral forces were not considered for this system, shear walls would be required.



Analysis

From the CRSI Handbook it was found that for a 30'0" span drop panels were needed that are 10'0" square and 8.5" deep. Columns are to be 24" square. PCA Slab was run to evaluate this system and it was found to satisfy all conditions, including reinforcement and deflection.

Evaluation

Pros	Cons
Durable	Redesign of foundation
Smaller floor depth	Longer erection time
No extra fireproofing	Large columns

Overall Evaluation

	Existing	Non-Composite	Hollow Core Plank	Two-way Flat Slab
Floor Thickness	Moderate	Moderate	Large	Smallest
Fireproofing	Yes	Yes	Yes	No
Fast Erection	Yes	Yes	Yes	No
Lead Time	Long	Long	Long	Short
Further Evaluation	Yes	Yes	No	Yes

CONCLUSION

After analyzing these four systems it was found that the existing system is the most suitable. The hollow core plank is the worst system due to its weight and size of the supporting members. Non-composite steel and the two-way flat slab can be considered further. Both work well with the existing layout and have unique advantages. Although these two systems will be investigated further the existing structural system is probably the best for this project.

APPENDIX

Existing System Beam Design



RAM Steel v11.0
DataBase: try
Building Code: IBC

Gravity Beam Design

12/21/08 12:19:36
Steel Code: ASD 9th Ed.

Floor Type: typ **Beam Number = 95**

SPAN INFORMATION (ft): I-End (60.00,106.00) J-End (90.00,106.00)

Minimum Depth specified = 17.00 in

Beam Size (User Selected) = W18X35

Fy = 50.0 ksi

Total Beam Length (ft) = 30.00

COMPOSITE PROPERTIES (Not Shored):

		Left		Right
Concrete thickness (in)		3.25		3.25
Unit weight concrete (pcf)		115.00		115.00
f _c (ksi)		3.00		3.00
Decking Orientation		perpendicular		perpendicular
Decking type		ASC 3W		ASC 3W
b _{eff} (in)	= 90.00	Y bar(in)	=	18.09
Seff (in ³)	= 80.45	Str (in ³)	=	102.52
I _{eff} (in ⁴)	= 1172.43	Itr (in ⁴)	=	1812.41
Stud length (in)	= 5.19	Stud diam (in)	=	0.75
Stud Capacity (kips)	q = 7.4			
# of studs:	Full = 60	Partial = 18	Actual = 18	
Number of Stud Rows = 1	Percent of Full Composite Action = 25.87			

LINE LOADS (k/ft):

Load	Dist	DL	CDL	LL	Red%	Type	CLL
1	0.000	0.990	0.000	0.800	13.8%	Red	0.000
	30.000	0.990	0.000	0.800			0.000
2	0.000	0.035	0.035	0.000	---	NonR	0.000
	30.000	0.035	0.035	0.000			0.000

SHEAR: Max V (DL+LL) = 25.72 kips fv = 5.09 ksi Fv = 19.13 ksi

MOMENTS:

Span	Cond	Moment kip-ft	@ ft	Lb ft	Cb	Tension Flange fb	Fb	Compr Flange fb	Fb
Center	PreCmp+	3.9	15.0	0.0	1.00	0.82	33.00	0.82	33.00
	Max +	192.9	15.0	---	---				
	Mmax/Seff					28.78	33.00	---	---
	Mconst/Sx+Mpost/Seff					29.01	45.00	---	---
Controlling		192.9	15.0	---	---	28.78	33.00	---	---
	f _c (ksi) = 0.62	F _c = 1.35							

REACTIONS (kips):

	Left	Right
Initial reaction	0.53	0.53
DL reaction	15.38	15.38
Max +LL reaction	10.35	10.35
Max +total reaction	25.72	25.72

DEFLECTIONS:

Initial load (in) at 15.00 ft = -0.043 L/D = 8336

Existing System Girder Design



RAM Steel v11.0
DataBase: try
Building Code: IBC

Gravity Beam Design

12/21/08 12:19:36
Steel Code: ASD 9th Ed.

Floor Type: typ **Beam Number = 13**

SPAN INFORMATION (ft): I-End (60.00,86.00) J-End (60.00,116.00)

Minimum Depth specified = 17.00 in
Beam Size (Optimum) = W24X55 $F_y = 50.0$ ksi
Total Beam Length (ft) = 30.00

COMPOSITE PROPERTIES (Not Shored):

		Left		Right
Concrete thickness (in)		3.25		3.25
Unit weight concrete (pcf)		115.00		115.00
f_c (ksi)		3.00		3.00
Decking Orientation		parallel		parallel
Decking type		ASC 3W		ASC 3W
b_{eff} (in) =	90.00	Y bar(in) =	22.14	
Se_{ff} (in ³) =	174.99	Str (in ³) =	187.86	
I_{eff} (in ⁴) =	3577.09	Itr (in ⁴) =	4052.40	
Stud length (in) =	5.19	Stud diam (in) =	0.75	
Stud Capacity (kips) $q = 9.9$				
# of studs per stud segment:		Full =	42,1,42	
		Partial =	27,2,27	
		Actual =	27,2,27	
Number of Stud Rows = 2		Percent of Full Composite Action =	65.63	

POINT LOADS (kips):

Dist	DL	CDL	RedLL	Red%	NonRLL	StorLL	Red%	RoofLL	Red%	CLL
10.000	15.38	0.53	12.00	31.7	0.00	0.00	0.0	0.00	Snow	0.00
10.000	15.38	0.53	12.00	31.7	0.00	0.00	0.0	0.00	Snow	0.00
20.000	15.38	0.53	12.00	31.7	0.00	0.00	0.0	0.00	Snow	0.00
20.000	15.38	0.53	12.00	31.7	0.00	0.00	0.0	0.00	Snow	0.00

LINE LOADS (k/ft):

Load	Dist	DL	CDL	LL	Red%	Type	CLL
1	0.000	0.055	0.055	0.000	---	NonR	0.000
	30.000	0.055	0.055	0.000			0.000

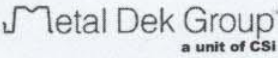
SHEAR: Max V (DL+LL) = 47.97 kips $f_v = 5.38$ ksi $F_v = 18.78$ ksi

MOMENTS:

Span	Cond	Moment	@	Lb	Cb	Tension Flange	Compr Flange
		kip-ft	ft	ft		fb Fb	fb Fb
Center	PreCmp+	16.8	15.0	10.0	1.00	1.75 30.00	1.75 25.01
	Max +	477.7	15.0	---	---		
	M_{max}/Se_{ff}					32.76 33.00	---
	$M_{const}/S_x + M_{post}/Se_{ff}$					33.35 45.00	---
Controlling		477.7	15.0	---	---	32.76 33.00	---
f_c (ksi) = 0.91	$F_c = 1.35$						

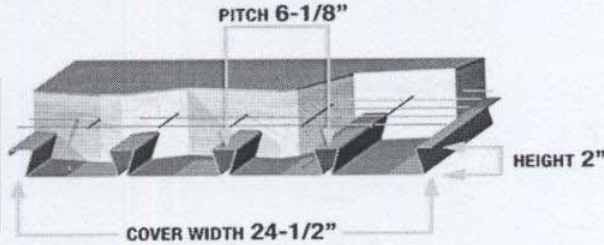
REACTIONS (kips):

Non-composite Deck Selection



Metal Dek Group
a unit of CSI

VERSA-DEK® S
 2" high x 6-1/8" pitch x 24-1/2" wide



PITCH 6-1/8"
 HEIGHT 2"
 COVER WIDTH 24-1/2"

SECTION PROPERTIES fy = 40 ksi

GAGE	t (in)	Ip (in^4)	In (in^4)	Sp (in^3)	Sn (in^3)
22	0.0295	0.4027	0.3266	0.2895	0.2692
20	0.0358	0.4918	0.4251	0.3620	0.3354
18	0.0474	0.6578	0.6166	0.4852	0.4616
16	0.0598	0.8372	0.8185	0.6192	0.6000

115 PCF LIGHTWEIGHT CONCRETE

h	4"				4.25"				4.5"				4.75"				5"				5.25"			
GAGE	22	20	18	16	22	20	18	16	22	20	18	16	22	20	18	16	22	20	18	16	22	20	18	16
Wc	35.2	35.2	35.2	35.2	37.6	37.6	37.6	37.6	40.0	40.0	40.0	40.0	42.4	42.4	42.4	42.4	44.8	44.8	44.8	44.8	47.2	47.2	47.2	47.2
Ac	39.7	39.7	39.7	39.7	42.1	42.1	42.1	42.1	44.4	44.4	44.4	44.4	46.8	46.8	46.8	46.8	49.2	49.2	49.2	49.2	51.5	51.5	51.5	51.5
Iav	4.6	5.0	5.6	6.2	5.5	5.9	6.6	7.3	6.4	6.9	7.7	8.5	7.4	8.0	8.9	9.8	8.5	9.2	10.2	11.3	9.7	10.5	11.7	12.9
Sb	1.48	1.75	2.24	2.75	1.61	1.91	2.44	2.99	1.74	2.07	2.65	3.25	1.87	2.23	2.86	3.50	2.01	2.39	3.07	3.77	2.15	2.56	3.29	4.03
St	30.5	32.5	36.4	38.0	34.0	36.1	39.3	42.1	37.6	40.0	43.5	46.5	41.4	44.0	47.9	51.2	45.4	48.2	52.5	56.1	49.5	52.6	57.3	61.2

L **MAXIMUM ALLOWABLE UNIFORM LIVE LOADS, (psf) - ASD/LRFD - NO STUDS ON BEAMS**

L	MAXIMUM ALLOWABLE UNIFORM LIVE LOADS, (psf) - ASD/LRFD - NO STUDS ON BEAMS																							
9'-0"	227	301	338	373	245	354	397	400	263	389	400	400	281	400	400	400	300	400	400	400	318	400	400	400
10'-0"	170	186	246	272	204	223	289	319	235	246	337	372	251	263	390	400	267	280	400	400	284	297	400	400
11'-0"	119	131	185	204	145	158	217	240	173	189	254	279	204	222	253	323	237	253	274	371	263	268	291	400
12'-0"	84	93	108	157	103	114	131	185	124	137	157	215	148	162	185	249	174	190	217	285	203	221	252	280
13'-0"	59	66	78	124	74	82	95	108	90	99	115	130	108	119	137	154	128	141	162	181	150	165	188	211
14'-0"	41	46	56	64	52	59	69	79	65	72	85	96	79	87	102	115	94	104	121	136	112	123	142	160
15'-0"				46		41	49	57	46	52	62	71	57	64	75	86	69	77	90	103	83	92	107	121
16'-0"				80		76	86	95	78	89	100	110	85	103	116	127	91	115	133	146	98	124	152	167
17'-0"							41				44	52	40	45	55	64	49	56	67	77	60	68	80	92
18'-0"							78				82	91	70	85	95	105	76	97	110	120	82	104	125	137
19'-0"																46		40	49	57	43	49	59	69
20'-0"																87		82	91	100	68	88	104	115
																				41		43	51	
																				85		88	97	

MAXIMUM UNSHORED CONSTRUCTION CLEAR SPANS

	6'-10"	7'-10"	9'-4"	10'-9"	6'-8"	7'-8"	9'-1"	10'-6"	6'-6"	7'-6"	8'-11"	10'-3"	6'-4"	7'-4"	8'-8"	10'-0"	6'-3"	7'-2"	8'-6"	9'-10"	6'-2"	7'-0"	8'-4"	9'-7"
1span	8'-7"	9'-7"	11'-2"	12'-7"	8'-5"	9'-4"	10'-11"	12'-4"	8'-3"	9'-2"	10'-9"	12'-2"	8'-1"	9'-0"	10'-6"	11'-11"	7'-11"	8'-10"	10'-4"	11'-9"	7'-10"	8'-8"	10'-2"	11'-6"
2span	8'-11"	9'-11"	11'-6"	13'-1"	8'-8"	9'-8"	11'-4"	12'-9"	8'-6"	9'-6"	11'-1"	12'-7"	8'-4"	9'-4"	10'-10"	12'-4"	8'-3"	9'-2"	10'-8"	12'-1"	8'-1"	9'-0"	10'-6"	11'-11"
3span	2'-8"	3'-2"	4'-0"	4'-10"	2'-7"	3'-1"	3'-11"	4'-9"	2'-7"	3'-1"	3'-11"	4'-8"	2'-7"	3'-0"	3'-10"	4'-7"	2'-6"	3'-0"	3'-9"	4'-6"	2'-6"	2'-11"	3'-9"	4'-6"
cy/100sf		1.13				1.21				1.29				1.37			1.44					1.52		


9'-0"	227	← maximum allowable live load (psf) based on ASD composite design
↑	230	← maximum allowable live load (psf) based on LRFD composite design
←		clear span

<p>t Design thickness of deck</p> <p>Ip Moment of inertia of deck for positive bending</p> <p>In Moment of inertia of deck for negative bending</p> <p>Sp Section modulus of deck for positive bending</p> <p>Sn Section modulus of deck for negative bending</p> <p>fy 40 ksi</p> <p>Fc 3000 psi</p>	<p>h Total height of concrete slab</p> <p>Wc Weight of concrete (neglecting deflection)</p> <p>Ac Effective area of concrete available to resist shear</p> <p>Iav Average moment of inertia of cracked & uncracked section</p> <p>Sb Cracked section modulus for positive bending</p> <p>St Cracked section modulus for negative bending</p> <p>L Span length; clear distance of deck between supports</p>
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Interior bearing of 5" in the above tables. If welded wire fabric is not supplied per ACI requirements (0.00075*Ac), reduce loads by 10%. The section property table is based on AISI's Cold-Formed Steel Design Manual, 2001 Edition. The live loads and unshored construction clear spans are based on the Steel Deck Institute's Composite Deck Design Handbook, March 1997 and Design Manual, Pub. No. 30, and ASCE's Standard for the Structural Design of Composite Slabs. Maximum Unshored Construction Clear Spans are based on ASD design. The loads in these tables are based on a Simple Span Design Analysis.

Rev: 01/27/05

115 PCF LIGHTWEIGHT CONCRETE TABLE



12

Non-composite Beam Design



RAM Steel v11.0
DataBase: noncomposite
Building Code: IBC

Gravity Beam Design

12/22/08 05:46:02
Steel Code: ASD 9th Ed.

Floor Type: typ **Beam Number = 105**

SPAN INFORMATION (ft): **I-End (90.00,106.00)** **J-End (120.00,106.00)**
 Beam Size (Optimum) = W8X10 $F_y = 50.0$ ksi
 Total Beam Length (ft) = 30.00

LINE LOADS (k/ft):

Load	Dist	DL	LL	Red%	Type
1	0.000	0.010	0.000	---	NonR
	30.000	0.010	0.000		

SHEAR: Max V (DL+LL) = 0.15 kips $f_v = 0.11$ ksi $F_v = 20.00$ ksi

MOMENTS:

Span	Cond	Moment kip-ft	@ ft	Lb ft	Cb	Tension Flange		Compr Flange	
						fb	Fb	fb	Fb
Center	Max +	1.1	15.0	30.0	1.00	1.74	30.00	1.74	3.41
Controlling		1.1	15.0	30.0	1.00	---	---	1.74	3.41

REACTIONS (kips):

	Left	Right
DL reaction	0.15	0.15
Max +total reaction	0.15	0.15

DEFLECTIONS:

Dead load (in)	at	15.00 ft =	-0.206	L/D =	1752
Live load (in)	at	15.00 ft =	0.000		
Net Total load (in)	at	15.00 ft =	-0.206	L/D =	1752

Non-composite Girder Design



RAM Steel v11.0
DataBase: noncomposite
Building Code: IBC

Gravity Beam Design

12/22/08 05:46:02
Steel Code: ASD 9th Ed.

Floor Type: typ **Beam Number = 23**

SPAN INFORMATION (ft): I-End (120.00,86.00) J-End (120.00,116.00)

Beam Size (Optimum) = W24X76 $F_y = 50.0$ ksi
Total Beam Length (ft) = 30.00

POINT LOADS (kips):

Dist	DL	RedLL	Red%	NonRLL	StorLL	Red%	RoofLL	Red%
10.000	0.15							
10.000	0.15							
20.000	0.15							
20.000	0.15							

LINE LOADS (k/ft):

Load	Dist	DL	LL	Red%	Type
1	0.000	2.670	2.400	39.6%	Red
	30.000	2.670	2.400		
2	0.000	0.076	0.000	---	NonR
	30.000	0.076	0.000		

SHEAR: Max V (DL+LL) = 63.22 kips $f_v = 6.01$ ksi $F_v = 20.00$ ksi

MOMENTS:

Span	Cond	Moment kip-ft	@ ft	Lb ft	Cb	Tension Flange fb	Fb	Compr Flange fb	Fb
Center	Max +	474.9	15.0	0.0	1.00	32.38	33.00	32.38	33.00
Controlling		474.9	15.0	0.0	1.00	32.38	33.00	---	---

REACTIONS (kips):

	Left	Right
DL reaction	41.49	41.49
Max +LL reaction	21.73	21.73
Max +total reaction	63.22	63.22

DEFLECTIONS:

Dead load (in)	at	15.00 ft =	-0.830	L/D =	434
Live load (in)	at	15.00 ft =	-0.433	L/D =	830
Net Total load (in)	at	15.00 ft =	-1.264	L/D =	285

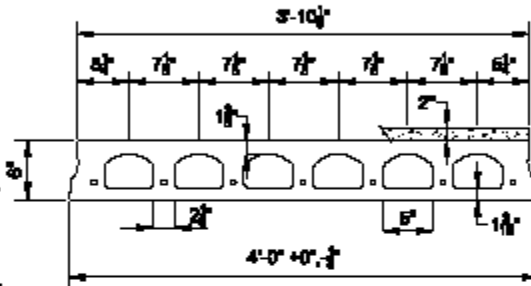
Hollow Core Plank Specifications

**Prestressed Concrete
6"x4'-0" Hollow Core Plank**
2 Hour Fire Resistance Rating With 2" Topping

PHYSICAL PROPERTIES Composite Section	
$A_c = 253 \text{ in.}^2$	Precast $b_w = 16.13 \text{ in.}$
$I_c = 1518 \text{ in.}^4$	Precast $S_{top} = 370 \text{ in.}^3$
$Y_{top} = 4.10 \text{ in.}$	Topping $S_{tot} = 561 \text{ in.}^3$
$Y_{cp} = 1.90 \text{ in.}$	Precast $S_{cp} = 799 \text{ in.}^3$
$Y_{ca} = 3.90 \text{ in.}$	Precast $W_L = 185 \text{ PLF}$
	Precast $W_L = 48.75 \text{ PSF}$

DESIGN DATA

1. Precast Strength @ 28 days = 6000 PSI
2. Precast Strength @ release = 3500 PSI
3. Precast Density = 150 PCF
4. Strand = 1/2"Ø 270K Lo-Relaxation.
5. Strand Height = 1.75 in.
6. Ultimate moment capacity (when fully developed)...
 4-1/2"Ø, 270K = 67.4 k-ft at 60% jacking force
 6-1/2"Ø, 270K = 82.6 k-ft at 60% jacking force
 7-1/2"Ø, 270K = 95.3 k-ft at 60% jacking force
7. Medium bottom tensile stress is $10\sqrt{f_c} = 775 \text{ PSI}$
8. All superimposed load is treated as live load in the strength analysis of flexure and shear.
9. Flexural strength capacity is based on stress/strain strand relationships.
10. Deflection limits were not considered when determining allowable loads in this table.
11. Topping Strength @ 28 days = 3000 PSI. Topping Weight = 25 PSF.
12. These tables are based upon the topping having a uniform 2" thickness over the entire span. A lesser thickness might occur if camber is not taken into account during design, thus reducing the load capacity.
13. Load values to the left of the solid line are controlled by ultimate shear strength.
14. Load values to the right are controlled by ultimate flexural strength or fire endurance limits.
15. Load values may be different for IBC 2000 & ACI 318-99. Load tables are available upon request.
16. Camber is inherent in all prestressed hollow core slabs and is a function of the amount of eccentric prestressing force needed to carry the superimposed design loads along with a number of other variables. Because prediction of camber is based on empirical formulas it is at best an estimate, with the actual camber usually higher than calculated values.



SAFE SUPERIMPOSED SERVICE LOADS		IBC 2006 & ACI 318-05 (1.2 D + 1.6 L)																		
Strand Pattern	LOAD (PSF)	SPAN (FEET)																		
		12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
4 - 1/2"Ø	LOAD (PSF)	249	317	290	265	227	197	174	149	127	105	82	78	68	55	48 43 38 33				
6 - 1/2"Ø	LOAD (PSF)	324	478	437	377	334	292	269	237	215	188	165	142	122	104	88	73	61	49	38
7 - 1/2"Ø	LOAD (PSF)	541	482	461	415	364	321	293	274	242	214	190	167	144	124	107	91	77	64	53



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This table is for single spans and uniform loads. Design data for any of these span-load conditions is available on request. Individual designs may be furnished to satisfy unusual conditions of heavy loads, concentrated loads, cantilevers, bays or stem openings and narrow voids. The allowable loads shown in this table reflect a 2 Hour & 0 Minute fire resistance rating.

11/03/08

6F2.0T

Hollow Core Plank Calculations

$$W = 1.2(99 + 48.75 \text{ psf}) + 1.6 * 80 = 305.3 \text{ psf}$$

$$w = 305.3 \text{ psf} * 15 \text{ ft.} = 4.58 \text{ klf}$$

$$M_u = 4.58 * (30)^2 / 8 = 515 \text{ ft.-kips}$$

$$V_u = 4.58 * 30 / 2 = 68.7 \text{ kips}$$

$$I_{\text{required}} = 360 * 4.58 * (30 * 12)^2 / (384 * 29000) = 6907 \text{ in}^4$$

Try W24x229 to optimize floor thickness

$$w = 4.58 + 1.2 * .229 = 4.85$$

$$M_u = 4.85 * 30^2 / 8 = 546 \text{ ft-kips} < 1760 \text{ ft-kips}, \text{ OK}$$

$$V_u = 4.85 * 30 / 2 = 73 \text{ kips} < 674 \text{ kips}, \text{ OK}$$

CRSI Handbook

SPAN c.-c. (ft)		Factored Superim- posed Load (psf)	Square Drop Panel		(3) Square Column		REINFORCING BARS (E. W.)						MOMENTS			Factored Superim- posed Load (psf)	(3) Square Column Size (in.)	REINFORCING BARS (E. W.)						Concrete (cu. ft) (sq. ft)
			Depth (in.)	Width (ft)	Size (in.)	γ_f	Column Strip (1)		Middle Strip		Total Steel (psf)	Edge (-) (ft-k)	Bot. (+) (ft-k)	Int. (-) (ft-k)	Column Strip			Middle Strip		Total Steel (psf)				
h = 10 in. = TOTAL SLAB DEPTH BETWEEN DROP PANELS																								
25	100	5.50	8.33	12	0.776	12-#5 2	10-#6	14-#5	9-#5	9-#5	2.39	130.1	260.2	350.3	100	12	13-#5	9-#5	9-#5	9-#5	2.19	0.884		
25	200	5.50	8.33	15	0.809	12-#5 4	13-#6	13-#6	12-#5	10-#5	2.95	171.3	342.6	481.2	200	18	12-#6	12-#5	10-#5	9-#5	2.63	0.884		
25	300	7.00	8.33	19	0.664	12-#5 1	17-#6	15-#6	15-#5	9-#6	3.59	212.4	424.7	571.8	300	21	14-#6	15-#5	12-#5	10-#5	3.10	0.898		
25	400	8.50	8.33	19	0.632	12-#5 1	15-#7	12-#7	10-#7	15-#5	4.25	254.3	508.6	684.6	400	23	15-#6	18-#5	10-#6	12-#5	3.63	0.912		
25	500	8.50	10.00	21	0.744	13-#5 3	11-#9	26-#5	15-#6	10-#7	4.97	295.4	590.8	795.3	500	25	13-#7	15-#6	16-#5	10-#6	4.26	0.947		
26	100	5.50	8.67	12	0.810	12-#5 3	11-#6	16-#5	11-#5	10-#5	2.60	146.8	293.7	395.3	100	12	15-#5	11-#5	10-#5	10-#5	2.40	0.884		
26	200	7.00	8.67	15	0.704	12-#5 1	11-#7	14-#6	10-#6	12-#5	3.17	194.0	388.0	522.3	200	18	17-#5	14-#5	10-#5	10-#5	2.73	0.898		
26	300	8.50	8.67	18	0.633	12-#5 1	11-#8	15-#6	9-#7	15-#5	3.88	240.6	481.1	647.6	300	21	14-#6	9-#7	13-#5	11-#5	3.31	0.912		
26	400	8.50	8.67	19	0.745	13-#5 3	13-#8	18-#6	11-#7	9-#7	4.73	287.7	575.5	774.7	400	23	13-#7	11-#7	16-#5	10-#6	4.17	0.912		
26	500	8.50	10.40	24	0.745	15-#5 4	13-#9	12-#8	10-#8	14-#6	5.49	330.9	661.8	890.9	500	25	27-#5	10-#8	10-#7	16-#5	4.65	0.947		
27	100	7.00	9.00	12	0.748	12-#5 2	18-#5	16-#5	12-#5	10-#5	2.63	165.4	330.8	445.4	100	12	15-#5	12-#5	10-#5	10-#5	2.37	0.898		
27	200	7.00	9.00	15	0.804	12-#5 5	17-#6	15-#6	11-#6	13-#5	3.37	218.2	436.3	587.4	200	18	14-#6	11-#6	12-#5	10-#5	2.92	0.898		
27	300	8.50	9.00	18	0.674	12-#5 2	16-#7	13-#7	19-#5	16-#5	4.12	270.7	541.5	728.9	300	21	12-#7	19-#5	15-#5	9-#6	3.56	0.912		
27	400	8.50	10.80	22	0.756	14-#5 5	12-#9	12-#8	10-#8	19-#5	5.09	321.6	643.2	865.8	400	24	26-#5	10-#8	10-#7	15-#5	4.35	0.947		
27	500	8.50	10.80	27	0.682	16-#5 3	17-#8	13-#8	9-#9	9-#8	5.78	366.6	733.3	987.1	500	27	16-#7	11-#8	11-#7	18-#5	5.02	0.947		
28	100	7.00	9.33	12	0.784	13-#5 2	14-#6	18-#5	13-#5	11-#5	2.76	185.0	370.0	498.1	100	12	17-#5	13-#5	10-#5	10-#5	2.42	0.898		
28	200	8.50	9.33	16	0.714	13-#5 3	11-#8	15-#6	17-#5	15-#5	3.56	243.2	486.4	654.8	200	19	14-#6	17-#5	13-#5	12-#5	3.02	0.912		
28	300	8.50	9.33	19	0.757	13-#5 5	11-#9	14-#7	12-#7	10-#7	4.56	302.4	604.8	814.1	300	21	13-#7	22-#5	12-#6	10-#6	3.85	0.912		
28	400	8.50	11.20	25	0.692	16-#5 3	17-#8	13-#8	11-#8	12-#7	5.47	357.1	714.3	961.5	400	24	16-#7	11-#8	20-#5	12-#6	4.71	0.947		
29	100	8.50	9.67	12	0.737	13-#5 2	22-#5	18-#5	15-#5	12-#5	2.91	206.7	413.4	556.5	100	12	17-#5	15-#5	12-#5	11-#5	2.58	0.912		
29	200	8.50	9.67	16	0.758	13-#5 4	12-#8	13-#7	19-#5	16-#5	3.81	271.2	542.5	730.3	200	19	16-#6	19-#5	15-#5	13-#5	3.27	0.912		
29	300	8.50	9.67	22	0.718	15-#5 4	20-#7	16-#7	10-#8	20-#5	4.92	334.3	668.6	900.1	300	21	15-#7	10-#8	10-#7	16-#5	4.34	0.912		
29	400	8.50	11.60	28	0.639	17-#5 2	15-#9	14-#8	12-#8	10-#8	5.83	392.7	785.4	1057.3	400	26	13-#8	12-#8	12-#7	10-#7	5.06	0.947		
30	100	8.50	10.00	12	0.774	14-#5 2	10-#8	20-#5	16-#5	10-#6	3.16	229.4	458.8	617.6	100	12	14-#6	12-#6	13-#5	11-#5	2.77	0.912		
30	200	8.50	10.00	18	0.744	14-#5 4	11-#9	14-#7	21-#5	10-#7	4.16	299.6	599.1	808.5	200	19	18-#6	22-#5	12-#6	10-#6	3.57	0.912		
30	300	8.50	10.00	24	0.675	16-#5 3	17-#8	14-#8	11-#8	12-#7	5.24	369.5	739.1	994.9	300	21	16-#7	11-#8	11-#7	18-#5	4.56	0.912		

CONCRETE REINFORCING STEEL INSTITUTE

PCA Slab Design

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A Computer Program Analysis, Design, and Investigation of
Reinforced Concrete Slab and Continuous Beam Systems
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[1] INPUT ECHO

General Information:

```

File name: C:\Documents and Settings\USER\My Documents\FlatPlate.slb
Project: Flat Plate
Frame:
Code: ACI 318-02      Mode: Design      Engineer:
Number of supports = 6      Reinforcement Database: ASTM A615
Floor System: Two-Way

Live load pattern ratio = 75%
Minimum free edge for punching shear = 10 times slab thickness
Deflections are based on cracked section properties.
In negative moment regions, Ig and Mcr DO NOT include flange/slab contribution (if available)
Compression reinforcement calculations NOT selected.
  
```

Material Properties:

```

=====
              Slabs|Beams      Columns
-----
wc =          150      150 lb/ft3
f'c =          4      4 ksi
Ec =       3834.3      3834.3 ksi
fr =       0.47434      0.47434 ksi

fy =          60 ksi, Bars are not epoxy-coated
fyv =         60 ksi
Es =       29000 ksi
  
```

Reinforcement Database:

```

Units: Db (in), Ab (in^2), Wb (lb/ft)
Size  Db  Ab  Wb  Size  Db  Ab  Wb
-----
#3    0.38  0.11  0.38  #4    0.50  0.20  0.67
#5    0.63  0.31  1.04  #6    0.75  0.44  1.50
#7    0.88  0.60  2.04  #8    1.00  0.79  2.67
#9    1.13  1.00  3.40  #10   1.27  1.27  4.30
  
```


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#11	1.41	1.56	5.31	#14	1.69	2.25	7.65
#18	2.26	4.00	13.60				

Span Data:

```

=====
Slabs: L1, wL, wR (ft); t, Hmin (in)
Span Loc  L1      t      wL      wR      Hmin
-----
1 Int     30.000  10.00  15.000  15.000  10.18  *b
2 Int     30.000  10.00  15.000  15.000   9.33
3 Int     30.000  10.00  15.000  15.000   9.33
4 Int     30.000  10.00  15.000  15.000   9.33
5 Int     30.000  10.00  15.000  15.000  10.18  *b
  
```

NOTES:
*b- Slab thickness is less than minimum.

Support Data:

```

=====
Columns: c1a, c2a, c1b, c2b (in); Ha, Hb (ft)
Supp     c1a     c2a     Ha     c1b     c2b     Hb     Red%
-----
1      24.00   24.00  16.000  24.00  24.00  19.000  100 *
2      24.00   24.00  16.000  24.00  24.00  19.000  100
3      24.00   24.00  16.000  24.00  24.00  19.000  100
4      24.00   24.00  16.000  24.00  24.00  19.000  100
5      24.00   24.00  16.000  24.00  24.00  19.000  100
6      24.00   24.00  16.000  24.00  24.00  19.000  100 *
  
```

* Do not check punching shear around this column.

Drop Panels: h (in); L1, L2, W1, W2 (ft)

```

Supp     h      L1      L2      W1      W2
-----
1      8.50   1.000  5.000  5.000  5.000 *a b d
2      8.50   5.000  5.000  5.000  5.000 *b
3      8.50   5.000  5.000  5.000  5.000 *b
4      8.50   5.000  5.000  5.000  5.000 *b
5      8.50   5.000  5.000  5.000  5.000 *b
6      8.50   5.000  1.000  5.000  5.000 *a b d
  
```

*a- Do not check punching shear around this drop panel.
*b- Standard drop.
*d- Excessive drop thickness will not be used for flexural design.

Boundary Conditions: Kz (kip/in); Kry (kip-in/rad)

```

Supp     Spring Kz   Spring Kry   Far End A   Far End B
-----
1         0         0         Fixed       Fixed
2         0         0         Fixed       Fixed
3         0         0         Fixed       Fixed
4         0         0         Fixed       Fixed
5         0         0         Fixed       Fixed
6         0         0         Fixed       Fixed
  
```

Load Data:

```

=====
Load Cases and Combinations:
Case  SELF   Dead   Live
Type  DEAD   DEAD   LIVE
U1    1.200  1.200  1.600
  
```

Span Loads:

Span Case Wa

Area Loads - Wa (lb/ft2):

1 Dead	99
2 Dead	99
3 Dead	99
4 Dead	99
5 Dead	99
1 Live	80
2 Live	80
3 Live	80
4 Live	80
5 Live	80

Support Loads: --- NONE ---

Support Displacements: --- NONE ---

Reinforcement Criteria:

```

=====
                Top bars      Bottom bars      Stirrups
                Min      Max      Min      Max      Min      Max
-----
Slabs and Ribs:
Bar Size      #5      #8      #5      #8
Bar spacing   1.00   18.00   1.00   18.00 in
  
```

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Reinf ratio 0.14 5.00 0.14 5.00 %
Cover 1.50 1.50 in

Beams:
Bar Size #5 #8 #5 #8 #3 #5
Bar spacing 1.00 18.00 1.00 18.00 6.00 18.00 in
Reinf ratio 0.14 5.00 0.14 5.00 %
Cover 1.50 1.50 in

=====

[2] DESIGN RESULTS

=====

Top Reinforcement:

=====

Units: Width (ft), Mmax (k-ft), Xmax (ft), As (in^2), Sp (in)

Span	Strip	Zone	Width	Mmax	Xmax	AsMin	AsMax	SpReq	AsReq	Bars
1	Column	Left	15.00	240.57	1.000	5.076	36.170	10.588	3.250	17-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	895.31	29.000	5.076	36.170	4.390	12.625	41-#5
	Middle	Left	15.00	-0.00	1.000	3.240	26.620	16.364	0.000	11-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	298.45	29.000	3.240	26.620	6.429	8.537	28-#5
2	Column	Left	15.00	767.05	1.000	5.076	36.170	4.390	10.721	41-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	620.88	29.000	5.076	36.170	6.000	8.593	30-#5
	Middle	Left	15.00	255.68	1.000	3.240	26.620	6.429	7.255	28-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	206.96	29.000	3.240	26.620	9.000	5.820	20-#5
3	Column	Left	15.00	653.76	1.000	5.076	36.170	6.000	9.068	30-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	653.76	29.000	5.076	36.170	6.000	9.068	30-#5
	Middle	Left	15.00	217.92	1.000	3.240	26.620	9.000	6.140	20-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	217.92	29.000	3.240	26.620	9.000	6.140	20-#5
4	Column	Left	15.00	620.88	1.000	5.076	36.170	6.000	8.593	30-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	767.05	29.000	5.076	36.170	4.390	10.721	41-#5
	Middle	Left	15.00	206.96	1.000	3.240	26.620	9.000	5.820	20-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	255.68	29.000	3.240	26.620	6.429	7.255	28-#5
5	Column	Left	15.00	895.31	1.000	5.076	36.170	4.390	12.625	41-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	240.57	29.000	5.076	36.170	10.588	3.250	17-#5
	Middle	Left	15.00	298.45	1.000	3.240	26.620	6.429	8.537	28-#5
		Middle	15.00	0.00	15.000	0.000	26.620	0.000	0.000	---
		Right	15.00	-0.00	29.000	3.240	26.620	16.364	0.000	11-#5

Top Bar Details:

=====

Units: Length (ft)

Span	Strip	Left				Continuous		Right			
		Bars	Length	Bars	Length	Bars	Length	Bars	Length	Bars	Length
1	Column	17-#5	10.24	---	---	---	---	21-#5	11.25	20-#5	7.46
	Middle	11-#5	7.16	---	---	---	---	28-#5	11.25	---	---
2	Column	21-#5	12.25	20-#5	6.88	---	---	17-#5	10.75	13-#5	6.60
	Middle	28-#5	12.25	---	---	---	---	20-#5	10.75	---	---
3	Column	17-#5	10.50	13-#5	6.62	---	---	17-#5	10.50	13-#5	6.62
	Middle	20-#5	10.50	---	---	---	---	20-#5	10.50	---	---
4	Column	17-#5	10.75	13-#5	6.60	---	---	21-#5	12.25	20-#5	6.88
	Middle	20-#5	10.75	---	---	---	---	28-#5	12.25	---	---
5	Column	21-#5	11.25	20-#5	7.46	---	---	17-#5	10.24	---	---
	Middle	28-#5	11.25	---	---	---	---	11-#5	7.16	---	---

Bottom Reinforcement:

=====

Units: Width (ft), Mmax (k-ft), Xmax (ft), As (in^2), Sp (in)

Span	Strip	Width	Mmax	Xmax	AsMin	AsMax	SpReq	AsReq	Bars
1	Column	15.00	305.60	12.250	3.240	26.620	6.207	8.753	29-#5

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	Middle	15.00	203.73	12.250	3.240	26.620	9.474	5.726	19-#5
2	Column	15.00	171.50	15.500	3.240	26.620	11.250	4.792	16-#5
	Middle	15.00	114.33	15.500	3.240	26.620	16.364	3.163	11-#5
3	Column	15.00	196.27	15.000	3.240	26.620	10.000	5.509	18-#5
	Middle	15.00	130.85	15.000	3.240	26.620	15.000	3.630	12-#5
4	Column	15.00	171.50	14.500	3.240	26.620	11.250	4.792	16-#5
	Middle	15.00	114.33	14.500	3.240	26.620	16.364	3.163	11-#5
5	Column	15.00	305.60	17.750	3.240	26.620	6.207	8.753	29-#5
	Middle	15.00	203.73	17.750	3.240	26.620	9.474	5.726	19-#5

Bottom Bar Details:

=====

Units: Start (ft), Length (ft)

Span Strip		Long Bars		Short Bars			
		Bars	Start	Length	Bars	Start	Length
1	Column	29-#5	0.00	30.00	---		
	Middle	11-#5	0.00	30.00	8-#5	4.50	21.00
2	Column	16-#5	0.00	30.00	---		
	Middle	11-#5	0.00	30.00	---		
3	Column	18-#5	0.00	30.00	---		
	Middle	11-#5	0.00	30.00	1-#5	4.50	21.00
4	Column	16-#5	0.00	30.00	---		
	Middle	11-#5	0.00	30.00	---		
5	Column	29-#5	0.00	30.00	---		
	Middle	11-#5	0.00	30.00	8-#5	4.50	21.00

Flexural Capacity:

=====

Units: From, To (ft), As (in²), PhiMn (k-ft)

Span Strip		From		To		AsTop	AsBot	PhiMn-	PhiMn+
		From	To	AsTop	AsBot				
1	Column	0.000	1.000	5.27	8.99			-386.55	313.40
		1.000	5.000	5.27	8.99			-386.55	313.40
		5.000	9.240	5.27	8.99			-188.04	313.40
		9.240	10.240	0.00	8.99			0.00	313.40
		10.240	10.800	0.00	8.99			0.00	313.40
		10.800	15.000	0.00	8.99			0.00	313.40
		15.000	18.750	0.00	8.99			0.00	313.40
		18.750	19.200	0.00	8.99			0.00	313.40
		19.200	19.928	0.00	8.99			0.00	313.40
		19.928	22.540	6.51	8.99			-230.50	313.40
	22.540	23.718	6.51	8.99			-230.50	313.40	
	23.718	25.000	12.71	8.99			-432.65	313.40	
	25.000	29.000	12.71	8.99			-900.99	313.40	
	29.000	30.000	12.71	8.99			-900.99	313.40	
	Middle	0.000	1.000	3.41	3.41			-123.07	123.07
		1.000	4.500	3.41	3.41			-123.07	123.07
		4.500	5.653	3.41	3.41			-123.07	123.07
		5.653	6.161	3.41	5.89			-123.07	209.36
		6.161	7.161	0.00	5.89			0.00	209.36
		7.161	10.800	0.00	5.89			0.00	209.36
10.800		15.000	0.00	5.89			0.00	209.36	
15.000		18.750	0.00	5.89			0.00	209.36	
18.750		19.200	0.00	5.89			0.00	209.36	
19.200		19.916	0.00	5.89			0.00	209.36	
19.916	24.347	8.68	5.89			-303.18	209.36		
24.347	25.500	8.68	3.41			-303.18	123.07		
25.500	29.000	8.68	3.41			-303.18	123.07		
29.000	30.000	8.68	3.41			-303.18	123.07		
2	Column	0.000	1.000	12.71	4.96			-900.99	177.32
		1.000	5.000	12.71	4.96			-900.99	177.32
		5.000	5.878	12.71	4.96			-432.65	177.32
		5.878	6.878	6.51	4.96			-230.50	177.32
		6.878	10.800	6.51	4.96			-230.50	177.32
		10.800	11.250	6.51	4.96			-230.50	177.32
		11.250	12.250	0.00	4.96			0.00	177.32
		12.250	15.000	0.00	4.96			0.00	177.32
		15.000	19.200	0.00	4.96			0.00	177.32
		19.200	19.250	0.00	4.96			0.00	177.32
		19.250	20.346	0.00	4.96			0.00	177.32
		20.346	23.399	5.27	4.96			-188.04	177.32
		23.399	24.495	5.27	4.96			-188.04	177.32
		24.495	25.000	9.30	4.96			-323.57	177.32
		25.000	29.000	9.30	4.96			-669.75	177.32
29.000	30.000	9.30	4.96			-669.75	177.32		
Middle	0.000	1.000	8.68	3.41			-303.18	123.07	

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	1.000	10.800	8.68	3.41	-303.18	123.07
	10.800	11.250	8.68	3.41	-303.18	123.07
	11.250	12.250	0.00	3.41	0.00	123.07
	12.250	15.000	0.00	3.41	0.00	123.07
	15.000	19.200	0.00	3.41	0.00	123.07
	19.200	19.250	0.00	3.41	0.00	123.07
	19.250	20.363	0.00	3.41	0.00	123.07
	20.363	29.000	6.20	3.41	-219.95	123.07
	29.000	30.000	6.20	3.41	-219.95	123.07
3 Column	0.000	1.000	9.30	5.58	-669.75	198.72
	1.000	5.000	9.30	5.58	-669.75	198.72
	5.000	5.461	9.30	5.58	-323.57	198.72
	5.461	6.618	5.27	5.58	-188.04	198.72
	6.618	9.344	5.27	5.58	-188.04	198.72
	9.344	10.500	0.00	5.58	0.00	198.72
	10.500	10.800	0.00	5.58	0.00	198.72
	10.800	15.000	0.00	5.58	0.00	198.72
	15.000	19.200	0.00	5.58	0.00	198.72
	19.200	19.500	0.00	5.58	0.00	198.72
	19.500	20.656	0.00	5.58	0.00	198.72
	20.656	23.382	5.27	5.58	-188.04	198.72
	23.382	24.539	5.27	5.58	-188.04	198.72
	24.539	25.000	9.30	5.58	-323.57	198.72
	25.000	29.000	9.30	5.58	-669.75	198.72
	29.000	30.000	9.30	5.58	-669.75	198.72
Middle	0.000	1.000	6.20	3.41	-219.95	123.07
	1.000	4.500	6.20	3.41	-219.95	123.07
	4.500	5.657	6.20	3.41	-219.95	123.07
	5.657	9.325	6.20	3.72	-219.95	134.01
	9.325	10.500	0.00	3.72	0.00	134.01
	10.500	10.800	0.00	3.72	0.00	134.01
	10.800	15.000	0.00	3.72	0.00	134.01
	15.000	19.200	0.00	3.72	0.00	134.01
	19.200	19.500	0.00	3.72	0.00	134.01
	19.500	20.675	0.00	3.72	0.00	134.01
	20.675	24.343	6.20	3.72	-219.95	134.01
	24.343	25.500	6.20	3.41	-219.95	123.07
	25.500	29.000	6.20	3.41	-219.95	123.07
	29.000	30.000	6.20	3.41	-219.95	123.07
4 Column	0.000	1.000	9.30	4.96	-669.75	177.32
	1.000	5.000	9.30	4.96	-669.75	177.32
	5.000	5.505	9.30	4.96	-323.57	177.32
	5.505	6.601	5.27	4.96	-188.04	177.32
	6.601	9.654	5.27	4.96	-188.04	177.32
	9.654	10.750	0.00	4.96	0.00	177.32
	10.750	10.800	0.00	4.96	0.00	177.32
	10.800	15.000	0.00	4.96	0.00	177.32
	15.000	17.750	0.00	4.96	0.00	177.32
	17.750	18.750	0.00	4.96	0.00	177.32
	18.750	19.200	6.51	4.96	-230.50	177.32
	19.200	23.122	6.51	4.96	-230.50	177.32
	23.122	24.122	6.51	4.96	-230.50	177.32
	24.122	25.000	12.71	4.96	-432.65	177.32
	25.000	29.000	12.71	4.96	-900.99	177.32
	29.000	30.000	12.71	4.96	-900.99	177.32
Middle	0.000	1.000	6.20	3.41	-219.95	123.07
	1.000	9.637	6.20	3.41	-219.95	123.07
	9.637	10.750	0.00	3.41	0.00	123.07
	10.750	10.800	0.00	3.41	0.00	123.07
	10.800	15.000	0.00	3.41	0.00	123.07
	15.000	17.750	0.00	3.41	0.00	123.07
	17.750	18.750	0.00	3.41	0.00	123.07
	18.750	19.200	8.68	3.41	-303.18	123.07
	19.200	29.000	8.68	3.41	-303.18	123.07
	29.000	30.000	8.68	3.41	-303.18	123.07
5 Column	0.000	1.000	12.71	8.99	-900.99	313.40
	1.000	5.000	12.71	8.99	-900.99	313.40
	5.000	6.282	12.71	8.99	-432.65	313.40
	6.282	7.460	6.51	8.99	-230.50	313.40
	7.460	10.072	6.51	8.99	-230.50	313.40
	10.072	10.800	0.00	8.99	0.00	313.40
	10.800	11.250	0.00	8.99	0.00	313.40
	11.250	15.000	0.00	8.99	0.00	313.40
	15.000	19.200	0.00	8.99	0.00	313.40
	19.200	19.760	0.00	8.99	0.00	313.40
	19.760	20.760	0.00	8.99	0.00	313.40
	20.760	25.000	5.27	8.99	-188.04	313.40
	25.000	29.000	5.27	8.99	-386.55	313.40
	29.000	30.000	5.27	8.99	-386.55	313.40
Middle	0.000	1.000	8.68	3.41	-303.18	123.07
	1.000	4.500	8.68	3.41	-303.18	123.07
	4.500	5.653	8.68	3.41	-303.18	123.07
	5.653	10.084	8.68	5.89	-303.18	209.36

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10.084	10.800	0.00	5.89	0.00	209.36
10.800	11.250	0.00	5.89	0.00	209.36
11.250	15.000	0.00	5.89	0.00	209.36
15.000	19.200	0.00	5.89	0.00	209.36
19.200	22.839	0.00	5.89	0.00	209.36
22.839	23.839	0.00	5.89	0.00	209.36
23.839	24.347	3.41	5.89	-123.07	209.36
24.347	25.500	3.41	3.41	-123.07	123.07
25.500	29.000	3.41	3.41	-123.07	123.07
29.000	30.000	3.41	3.41	-123.07	123.07

Slab Shear Capacity:

Units: b, d (in), Xu (ft), PhiVc, Vu(kip)

Span	b	d	Vratio	PhiVc	Vu	Xu
1	360.00	8.19	1.000	279.62	196.87	28.32
2	360.00	8.19	1.000	279.62	169.72	1.68
3	360.00	8.19	1.000	279.62	162.76	1.68
4	360.00	8.19	1.000	279.62	169.72	28.32
5	360.00	8.19	1.000	279.62	196.87	1.68

Flexural Transfer of Negative Unbalanced Moment at Supports:

Units: Width (in), Munb (k-ft), As (in^2)

Supp	Width	GammaF*Munb	Comb Pat	AsReq	AsProv	Additional Bars
1	---	Not checked	---	---	---	---
2	79.50	191.35	U1	Odd	2.593	5.614
3	79.50	119.41	U1	Odd	1.607	4.107
4	79.50	119.41	U1	Odd	1.607	4.107
5	79.50	191.35	U1	Odd	2.593	5.614
6	---	Not checked	---	---	---	---

Punching Shear Around Columns:

Units: Vu (kip), Munb (k-ft), vu (psi), Phi*vc (psi)

Supp	Vu	vu	Munb	Comb Pat	GammaV	vu	Phi*vc
1	---	Not checked	---	---	---	---	---
2	406.33	152.0	-198.16	U1	All	0.400	177.3
3	358.30	134.0	50.81	U1	All	0.400	140.5
4	358.30	134.0	-50.81	U1	All	0.400	140.5
5	406.33	152.0	198.16	U1	All	0.400	177.3
6	---	Not checked	---	---	---	---	---

Punching Shear Around Drops:

Units: Vu (kip), vu (psi), Phi*vc (psi)

Supp	Vu	Comb Pat	vu	Phi*vc
1	---	Not checked	---	---
2	365.70	U1	All	89.3
3	317.67	U1	All	77.6
4	317.67	U1	All	77.6
5	365.70	U1	All	89.3
6	---	Not checked	---	---

Maximum Deflections:

Units: Dz (in)

Span	Frame			Column Strip			Middle Strip		
	Dz(DEAD)	Dz(LIVE)	Dz(TOTAL)	Dz(DEAD)	Dz(LIVE)	Dz(TOTAL)	Dz(DEAD)	Dz(LIVE)	Dz(TOTAL)
1	-0.223	-0.124	-0.347	-0.329	-0.183	-0.512	-0.117	-0.065	-0.182
2	-0.077	-0.076	-0.153	-0.105	-0.102	-0.207	-0.050	-0.049	-0.100
3	-0.095	-0.091	-0.186	-0.128	-0.123	-0.252	-0.062	-0.059	-0.121
4	-0.077	-0.076	-0.153	-0.105	-0.102	-0.207	-0.050	-0.049	-0.100
5	-0.223	-0.124	-0.347	-0.329	-0.183	-0.512	-0.117	-0.065	-0.182

Material Takeoff:

Reinforcement in the Direction of Analysis

Top Bars:	5526.2 lb	<=>	36.84 lb/ft	<=>	1.228 lb/ft^2
Bottom Bars:	5472.6 lb	<=>	36.48 lb/ft	<=>	1.216 lb/ft^2
Stirrups:	0.0 lb	<=>	0.00 lb/ft	<=>	0.000 lb/ft^2
Total Steel:	10998.8 lb	<=>	73.33 lb/ft	<=>	2.444 lb/ft^2
Concrete:	4104.2 ft^3	<=>	27.36 ft^3/ft	<=>	0.912 ft^3/ft^2