# Final Report



North Pocono High School

**Covington Township, PA** 

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### NORTH POCONO HIGH SCHOOL

Covington Township, PA

Building Statistics
Building Occupant: North Pocono School District
Occupancy Type: Educational

29,000,000 Ground Break Completion Da



### **Project Team**

North Pocono School District Owner: Architects: Crabtree Rohrbaugh, and Associates Design Engineers: Greenman and Pederson Inc.

Construction Managers: Lobar Inc.







### rchitecture

The exterior of the school is a brick veneer that eats 900 people, as well as modern computer cience labs. The roof is flat with a slanted ped with sure-seal moisture protection. It also slanted overhand above the contract.



Mechanical Overview
2-7000 Btu oil based boilers provide hot water
16 DX-AHU with hot water heating coils provide air
and ventilation to serve VAV terminal reheat units
3-Condensing units provide the cooling capacity to





### Structural Overview

Cast in place reinforced concrete footings

8" CMU's or 12" cast in place concrete make up the exterior load bearing walls. Interior steel framing Slab on grade concrete floor systems.

The roof is 4" LW concrete on 0.5" steel decking with 3" insulation



### Electrical Overview

4-Dry type transformers step down the voltage from 480-3 phase to 120/208-3 phase 1-Dry type transforrer steps down the voltage from 480-3 phase to 277/480-3phase 1-350 KW emergency generator @ 480/277V The ligthing system consists of linear and compact flourescent lights

## Dan Hanley **Mechanical Option**







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# **Executive Summary**

North Pocono High School is a three level 230,000 ft <sup>2</sup> building located in Covington Township, Pennsylvania. It is designed for grades nine through twelve with a variety of classroom spaces. The current mechanical system meets the requirements of the design criteria established by the owner and design engineer. The existing design was limited by a strict budget and while the system adequately conditions the school, there is potential for improvement.

The goals of the HVAC redesign were to increase efficiency, decrease life cycle cost, educational purposes, and find savings in other building systems by modifying them to fit the mechanical system redesign. The 16 Direct Expansion (DX) rooftop air handling units were replaced by dedicated outdoor air systems (DOAS) with ground source heat pumps (GSHP) as a parallel system. The new system was not held to the same budget as the existing system. The new systems equipment cost was \$46 million more than the overall cost for the current design. An energy model generated by the Trane TRACE 700 program showed that the yearly energy use was reduced by 75% saving the North Pocono School District \$187.4 thousand a year in utility costs. This results in a 245 year payback period for the new system.

The two other systems directly affected by the HVAC redesign were the structural system and electrical system. Replacing the 16 rooftop air handlers and eliminating 6 condensing units with lighter DOAS units reduced the roof load by 55%. The reduction in load meant a lighter framing system which saved 17% for material and construction costs. Also, the 4 electrical panels that serve the major mechanical equipment were able to be reduced in frame size because the electrical load needed to run the DOAS units compared to the DX units was reduced by 55%. The savings from this system was included in the \$14.3 million yearly operational cost.

# General Building Information

North Pocono High School is a 230,000 square foot building located in Covington Township, Pennsylvania. The building consists of three levels of single use and mixed use spaces and will accommodate 3,000 students from grades nine through twelve. Construction began in the summer of 2007 and is scheduled to be completed in the fall of 2009.

The project team consisted of the owners, North Pocono School District, architects, Crabtree and Rohrbaugh Ass., design engineers, Greenman and Pedersen Inc., and the general contractor, Lobar Inc. The project was delivered as a design bid build with the winning bid being \$30 million dollars.

# **Building Systems Synopsis**

#### Architectural Overview

North Pocono High School is a three level building. The front of the building has a curved facade that extends the whole length on the building. The exterior façade is red brick veneer with a CMU wall. The entrance contains a vestibule attached to all of the administrative offices. Then you enter a lobby where you find your way throughout the rest of the building. The school contains a standard size gymnasium, a library, computer and science labs, and a food court.

#### Structural Overview

North Pocono's structural system consists of a steel frame that rests on load bearing masonry walls. There are 9 different types of reinforced wall footings that support the walls. They range from 3' to 7' in width. The most common type of rebar used in the wall footings is #5. The steel columns however rest on 4 different types of piers that then transfer the load to one of 14 different types of footings. The piers range in size from 22"x22" to 36"x28" with #6 and #8 bars for vertical reinforcing and #3 bars used as stirrups. The footings have a bearing pressure of 4,000 psf and range in size from 4'x4' to 11'x11'; they go from 12" deep to 29" deep. All the concrete is specified to having strength of 3,000 psi and the steel reinforcing has strength of 60,000psi. Typical floor construction consists of 4" slab-on-grade with normal weight and strength of 4,000 psi, with 6x6-W1.4x1.4 WWF reinforcing. The upper level floor construction is 2" normal weight concrete with 3,000 psi and reinforced with 6x6 W2.0x2.0 WWF on 1"-26 gage galvanized form deck. The total floor thickness is 3". North Pocono has two different exterior wall types. The first is 4" brick veneer that is supported by 8" CMU's that have a compressive strength of 2,800 psi on the net area of the block, the second is a 12" cast in place concrete wall that supports the 4" brick veneer, again with strength of 4,000 psi. The steel frame typically consists of 24K7 or 20K8 joists for the classrooms and 10K1 joists for the corridors. The gym uses 22K7 joists on the side while 56DLH15 joists span the middle section and they all transfer the load to 96G12N32K joist girders. The auditorium uses 56DHL17 joists that then transfer the load to the 12" concrete wall on either side of the auditorium. The roof deck is typically 1.5" 20 gauge galvanized steel decking with a

self weight of 7.0 psf, the gymnasium and auditorium however are have 3" concrete deck with 20 gauge galvanized decking.

#### Electrical Overview

North Pocono's electrical service is provided by the utility company PP&L. The utility serves a 4,000A - 480/277 3 Phase 4 Wire main switchboard. The switchboard then sends the service to the other panel boards and 5 Dry type transformers that step down the voltage from the 480V to 120/208V 3 phase power.

The emergency generator is 350 KW and supplies 480/277V power to the fire pumps and elevators along with the exit lights and most of the kitchen equipment. The generator also supplies the main electrical room along with the school's main telecommunications and data room.

### Lighting Overview

North Pocono's lighting system consists mostly of recessed linear fluorescent lights. The auditorium has dimming system over the seating as well as a theatrical lighting set on stage. The gymnasium features hi-bay linear fluorescent pendant fixtures.

#### Telecommunication Overview

North Pocono has a voice and data communications systems. They also have a closed-circuit television system that is available in all classrooms. It has a public announcement system in the gymnasium as well as in the auditorium.

# **Mechanical System Existing Conditions**

The mechanical design for North Pocono was based on initial cost saving. The goals of the designer were to create a system that met the school district's budget while providing a system that would meet the 2005 International Mechanical Code and provide a comfortable environment for the occupants.

### Design Conditions

The indoor design conditions were developed by the Greenman and Pedersen Inc. engineers. The designer determined the heating and cooling dry bulb temperatures, and the maximum relative humidity level for the school. They determined the most comfortable level for the school was to condition the spaces to 72 °F degree dry bulb temperature for heating and cooling with a maximum relative humidity at 50%. Next, the occupancy schedule for the building's design day was entered into the program. Chart 1 is an hourly breakdown of the occupancy schedule on the design day.

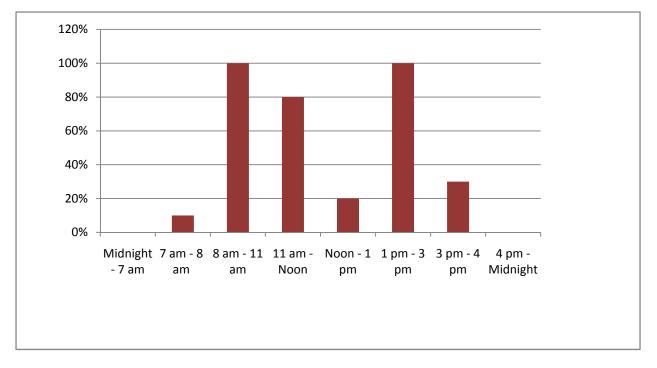


Chart 1 – Occupancy Schedule

The outdoor design conditions were taken from Wilkes-Barre, Pennsylvania since there is no weather data for Covington Township, PA. Table 1 summarizes the weather data that was used for design modeling.

Latitude	41.140
Longitude	75.52°
Elevation	550 ft.
Cooling Design DBT	87°
Heating Design DBT	5°

Table 1- Wilkes-Barre Design Conditions

#### System Description

The school is served by 16 direct expansion air handlers (DX), with duct mounted hot water heaters. Twelve of the AHUs serve approximately 100 variable air volume (VAV) terminal units with hydronic reheat coils. They serve the majority of the school. The other 4 are constant volume (CV) air handlers which are for economizer. One CV unit serves the locker room area, two supply a large multiuse space, and the last one serves the auditorium. The units mix return air with outside air then condition and supply it to the zones. Figure 1 is schematic of the VAV systems and Figure 2 is a schematic of the CV systems. Four condensing units serve the CV air handlers to provide additional

cooling capacity. The air handler that serves the gym also has two condensing units that provide cooling capacity.

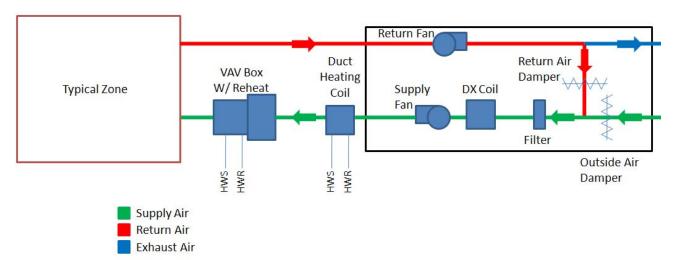
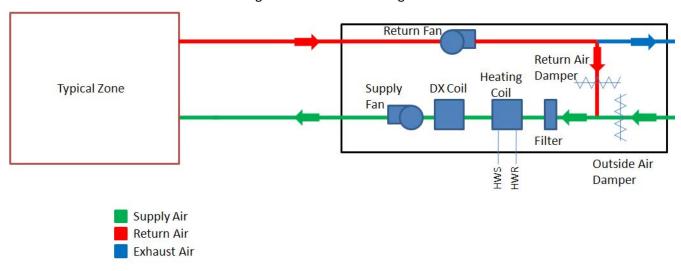


Figure 1 – VAV Air Flow diagram





The hydronic heating system for North Pocono is centralized in the mechanical room. It consists of two oil fired boilers, three centrifugal water pumps, the duct mounted heating coils, and the reheat coils contained in the VAV terminal units.

The water supplied to the boilers is heated to  $180^{\circ}$ F and then pumped through a two pipe system to the heating coils and terminal units. The boilers are programmed so that there is a lead boiler and when more heating is called for the second boiler is enabled. They alternate as the lead boiler every

week. The three pumps also trade off being the lead pump. The temperature of the water is monitored by the Direct Digital Control system. Figure 3 is a flow diagram representing the hydronic system.

Figure 3 – Flow Diagram

### **ASHRAE Standard 90.1**

### Building Envelope

The buildings fenestration percentage is less than 40% the total wall area; therefore it was acceptable to use the Prescriptive Method. North Pocono is located in climate zone 5 and is a nonresidential building; therefore had to comply with table 5.5-6. Table 2 shows the opaque elements of the building. Table 3 shows the window compliancy.

**Standard** Assembly Insulation **Assembly U-**Element Min. Compliant Max. U-Compliant **R-Value** Value **R-Value** Value Roof 10 20 No 0.681 0.48 No Wall Type 1 10 0.09 11.4 No 0.67 Yes Wall Type 2 10 11.4 No 0.093 0.09 No

NR

0.213

0.73

Yes

Table 2 – Opaque Envelope Compliance

Table 3 – Fenestration Compliance

NR

Fenestration	Assembly U- Value	Assembly Max. U-Value	Assembly SHGC	Max SHGC	Compliant
Metal Framing	0.5	0.45	0.55	0.4	No

### Building Equipment

Slab on Grade

NR

Since the building is larger than 25,000 ft<sup>2</sup> the Mandatory Provisions Method was followed in order to determine if the system was in compliance with 90.1 Section 6. The following tables are performance evaluations of the building's air handlers and boilers.

Table 4 – Boiler Efficiency

Boiler	Net MBH Output	Gross MBH Input	Efficiency	Standard Efficiency	Compliant
B-1	5,880	7,000	84%	78%	Yes
B-2	5,880	7,000	84%	78%	Yes

Air Flow Unit CFM\*0.0015 Complaint Fan HP (cfm) AHU-1 15,850 23.8 25 No AHU-2 16,415 24.6 25 No AHU-3 36,000 54.0 25 Yes AHU-4 3,700 5.6 5 Yes AHU-5 6,800 10.2 15 No AHU-6 19,500 29.3 20 Yes AHU-7 20.3 20 13,500 Yes 8-UHA 12,650 19.0 20 No AHU-9 14,195 21.3 25 No AHU-10 8,565 12.8 15 No 4.5 5 AHU-11 3,000 No AHU-12 3,800 5.7 NA NA AHU-13 18,200 27.3 30 No AHU-14 10,300 15.5 10 Yes AHU-15 15,300 23.0 25 No AHU-16 3,000 4.5 5 No

Table 5 – Air Handler Compliancy

Table 3 shows that only 5 of the 16 air handlers comply with Standard 90.1 2007 edition. However, they do comply with the 2004 Standard used during the design of the system.

### ASHRAE Standard 62.1

Section of Standard 62.1, Ventilation for Acceptable Indoor Air Quality, sets forth a procedure to determine the amount of ventilation air required in the building. Table 6 compares the amount of ventilation required to the amount of ventilation each air handler brings in. Appendix A lists each and air handler and the spaces they serve along with the designed ventilation value and the ASHRAE ventilation value.

Table 6 – Co	omputed Ventilation	vs. Designed Ventilation
I als al	ASHREA Standard	Designer Value

Label	ASHREA Standard	Designer Value
Label	(cfm)	(cfm)
AHU-1	4,195	4,355
AHU-2	5,025	7,360
AHU-3	4,810	10,270
AHU-5	2,750	3,860
AHU-6	2,865	19,500
AHU-7	4,525	4,800
AHU-8	3,895	4,315

Table 6 – cont.

AHU-9	5,370	6,225
AHU-10	1,670	3,685
AHU-11	465	3,000
AHU-12	2,400	2,255
AHU-13	5,105	10,725
AHU-14	1,985	2,470
AHU-15	3,950	5,890
AHU-16	470	3,000
Total	49,480	91,710
Difference	42,230	

Air handler 4 was excluded from this analysis because it is used as an economizer and only supplies 100% outdoor air to the space. This was done so that the exhaust fans that are in the zone were properly sized. In order to ensure optimal air quality, the engineer adequately ventilated North Pocono High School. However, this forces the system to condition more outdoor air than recommended and therefore increases the energy used by the system.

# **Existing Design Loads**

An energy model was used to determine the buildings cooling load. The Trace *TRACE 700* Program was used. The school was broken down into the 11 zones listed in Table 7.

Table 7 – Zone Description

Zone	Area (ft²)	Occupancy (People)
Lower Level Classrooms	35,685	425
Middle Level Classrooms	62,349	893
Upper Level Classrooms	51,375	945
Administrative Offices	10,000	121
Gymnasium	14,921	1500
Auditorium	10,720	890
Large Group Instruction	3,075	100
Cafeteria	15,362	480
Food Court	2,760	100
Faculty Dining	650	20
Kitchen	3,383	10
Lobby	2,245	0

After all the data was input into the program the results were generated. Tables 8 and 9 shows the results for North Pocono's cooling and heating load calculated by *TRACE 700*.

Table 8 – Computed Cooling Load

Zone	Computed Cooling Load (ft²/ton)
Lower Level Classrooms	388
Middle Level Classrooms	395
Upper Level Classrooms	357
Administrative Area	360
Gymnasium	244
Auditorium	324
Large Group Instruction	453
Cafeteria	374
Food Court	345
Faculty Dining	497
Kitchen	333
Lobby	509
Building Average	382
Total Tons	565

Table 9 – Computed Heating Load

Zone	Computed Heating Load (MBH)
Lower Level Classrooms	895
Middle Level Classrooms	1,041
Upper Level Classrooms	1,328
Administrative Area	343
Gymnasium	435
Auditorium	240
Large Group Instruction	59
Cafeteria	330
Food Court	63
Faculty Dining	12
Kitchen	318
Lobby	81
Building Average	429
Total Tons	5,145

# Lost Useable Space

North Pocono is not served by a central cooling plant and most of the equipment is on the roof. The amount of space lost to mechanical system is minimal. Table 10 is a comparison of the lost usable space due to the mechanical system.

 AREA (ft²)
 PERCENTAGE

 Mechanical Space
 2,357
 1%

 Remaining Spaces
 234,075
 99%

 Total
 236,432
 100%

Table 10 – Lost Useable Space

# Mechanical System Redesign

### Redesign Objectives

The objectives of the redesign were to lower the amount of energy the building needs to operate while meeting the computed design loads in tables 8 and 9, lower the emissions from the system, and gain knowledge in order to design a new system. The current system was restricted by the budget set by the school district; however, the new system will not be restrained by the budget.

### Ground Source Heat Pumps with Dedicated Outdoor Air Systems

The new design consisted of replacing the 16 DX AHU's with 15 Dedicated Outdoor Air Systems (DOAS) and using Ground Source Heat Pumps (GSHP) in the spaces. The reason for using 15 DOAS units is because two of the current AHUs, 11 and 16, serve one space therefore the ventilation air for that space will be brought in by one DOAS unit. The DOAS units were sized to bring in the amount of ventilation air set by ASHRAE Standard 62.1. Table 6 shows that approximately 42,000 less air is needed therefore less energy will be used on conditioning excess outdoor air.

The DOAS units were designed so that they can handle the latent load in the space during the cooling season. This is done by dehumidifying the air and driving the air temperature down to approximately 55 °F. By bringing the temperature down the DOAS unit will also eliminate approximately 20% of the sensible load; the remaining 80% will be handled by the GSHP. When heat is called for, the units are designed with small electric resistance heaters to provide some heating while the majority of the load is handled by the GSHP. Figure 4 is a picture of Carrier's 62D model, which was used as the basis of design.

Figure 4 – DOAS unit



### Sizing the Ground Loop

The GSHP system used a vertical closed loop system. This means bore holes are drilled to a depth between 100 – 400 ft, and the piping is not open to the thermal sink, such as a body of water or a well. The process of a ground loop is similar to that of a traditional water source heat pump. Instead of using mechanical equipment to provide the heat exchange the system takes advantage of the constant ground temperature to transfer heat to the water.

The ground loop was sized using a computer program developed at the University of Alabama, called *GCHPCalc*. The program is equipped to size ground loops based off the heat gains and losses the building under goes during the design day. Table 11 shows the heat gains and losses North Pocono under goes.

Table 11 - Building Heat Gains and Losses

Hours	Heat Losses (MBh)	Heat Gains (MBh)
8 a.m. – Noon	15186.2	11621.7
Noon – 4 p.m.	15779.0	11133.4
4 p.m. – 8 p.m.	851.0	623.2
8 p.m. – 8 a.m.	0	0

Next the program requested that all the ground data be entered into the program. Figures 5 and 6 shows the defaults the program uses, and since a thorough ground study was not done for the project the values provided by the program were used to size the ground loop. The ground temperature was however determined to be  $50\,^{\circ}$ F by the regional map provided in the program.

Figure 5 – Ground Properties

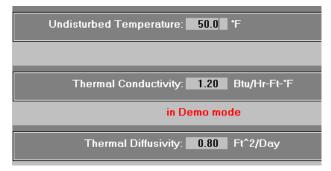
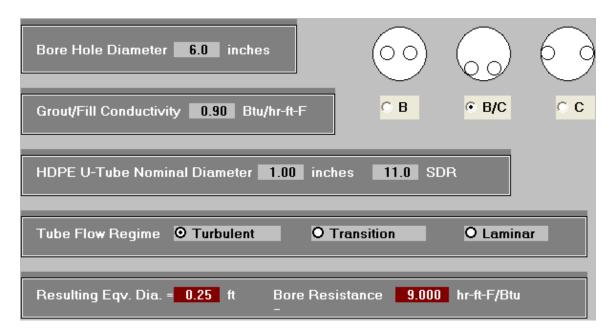
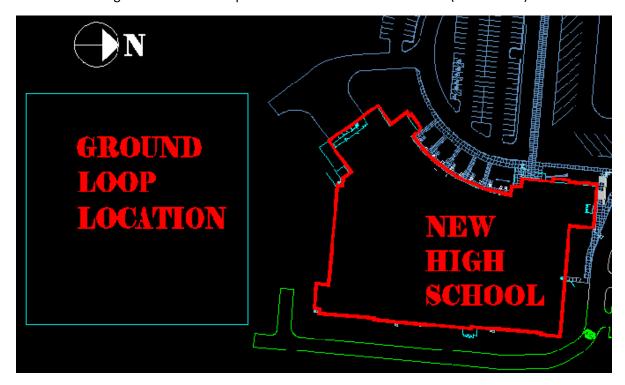


Figure 6 – Pipe Properties



Next the layout for the loop system was selected. The school is being built in a rural area with an abundance of land available. The configuration for the loop system is 35 rows by 30 rows with 8 bores per a parallel loop, and goes to depth of 390 ft. This turns out to be approximately 140,000 ft<sup>2</sup>. Figure 7 shows the location of the loop system.

Figure 7 – Ground Loop Location in Relation to the School (not to scale)



The same program offered a cost estimation program. The program determined that it would be approximately \$46.8 million dollars for materials and installation of the ground loop.

At the given ground conditions the GSHP provided enough cooling capacity but additional heating was needed. The heating performance of the GSHP at that temperature provides 3,187.8 MBH of heating while the total building load is 5058.3 MBH. To provide the remaining load a 2,000 MBH boiler was placed in the loop. Figure 8 is the flow diagram for the GSHP loop system.

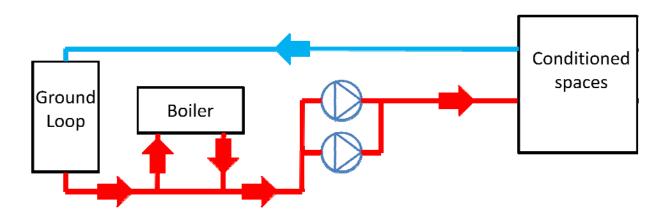


Figure 8 – GSHP Flow Diagram

#### Heat Pump Selection

The class room spaces will be served by a new console heat pump based on Carrier's 50PEC model. Figure 9 is picture of the unit.



Figure 9 – Carrier's 50PEC Console Heat Pump

The units were placed in the back of the classrooms and since they are only 12" deep they will take up minimal amount of space. This means that the outdoor air will be ducted directly into the space. This will ensure that each space gets the proper amount of ventilation. Figure 10 is a diagram of the air flow in a classroom.

Figure 10 – Typical Classroom Air Flow Diagram

The administrative offices and cafeteria area will use ceiling mounted heat pumps. The outdoor air will be ducted directly into these units so the space is properly ventilated. Figure 11 shows the units selected to condition these spaces. The unit is based off the Carrier 50YC, 50YD, and 50YE models.



Figure 11 – Ceiling Mounted Heat Pump

This model has a horizontal layout available which is the option that was selected for the school so that it can fit in the plenum space.

Due to the high loads and the absence of plenum space in the gym and auditorium rooftop water source heat pumps were selected to condition these areas. The gym will use 3 - 248 MBH cooling capacity units and the auditorium will use 2 - 175 MBH cooling capacity units. This equipment was based off Carrier's 50RTG unit pictured below.



Figure 12 – Rooftop Water Source Heat Pump

# Redesign – ASHRAE Standard 90.1

### **HVAC** Equipment

The new mechanical equipment performance values were reviewed to ensure that the system complied with ASHREA Standard 90.1-2007. Table 12 shows the 15 DOAS units compliance values. The fans horse power must be less than the airflow multiplied by 0.0015.

Unit	Air Flow (cfm)	CFM*0.0015	Fan HP	Compliant
DOAS-1	4,195	6.3	5	Yes
DOAS-2	4,815	7.2	5	Yes
DOAS-3	4,810	7.2	5	Yes
DOAS-5	2,750	4.1	3	Yes
DOAS-6	2,865	4.3	3	Yes
DOAS-7	4,525	6.8	5	Yes
DOAS-8	3,895	5.8	5	Yes
DOAS-9	4,910	7.4	5	Yes
DOAS-10	1,670	2.5	1.5	Yes
DOAS-11	935	1.4	1	Yes

Table 12 – DOAS Compliancy

Table 12 – cont.

DOAS-12	2,115	3.2	3	Yes
DOAS-13	5,105	7.7	5	Yes
DOAS-14	1,985	3	2	Yes
DOAS-15	3,950	5.9	5	Yes

Table 12 shows that each unit complies with Standard 90.1. The specifications of the other equipment selected for the redesign state they exceed the Standard requirements.

# System Comparison

After analyzing each system they both condition the school adequately. However, as stated before the current system was limited by the budget while the redesign had the luxury of not being constrained by the same budget. Table 13 compares the overall mechanical initial budget to the new systems equipment cost.

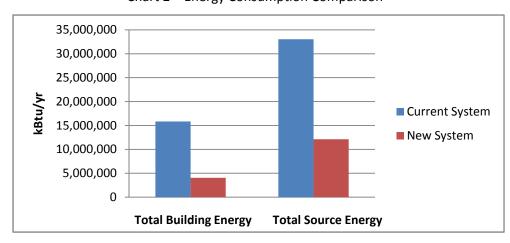
Table 13 –Initial Mechanical Cost vs. Redesigned Equipment Cost

	Cost (\$)
New Mechanical Cost	50,291,756
Mechanical Initial Cost	4,300,000
Difference	45,991,756

There is a significant difference in first cost between the two systems, however when the systems energy use was calculated it showed significant savings in the redesigned system.

Chart 2 compares the energy consumed by each system over one year. Appendix B has a monthly energy chart for each system.

Chart 2 – Energy Consumption Comparison



This difference led to savings in energy costs. Table 14 shows the utility rates for each system. The redesign did not include oil since the two oil fired boilers were eliminated from the design; however, the new boiler used to provide extra heating capacity in the ground loop system uses natural gas.

Utility Company Rate \$7.306 Electricity PP&L Charge per KW First 200 KWH \$12.11 Next 200 KWH \$9.162 \$0.03948/KWH Remaining KWH Consumption \$0.80/therm Oil **Natural Gas** UGI **Customer Fee** \$10.62 \$0.85/therm Consumption

Table 14 – Utility Rates

North Pocono is still looking for an oil provider therefore the rate that was used in the analysis was a sample that was in the TRACE 700 economic library. Chart 3 showed the yearly utility cost for North Pocono High School. Appendix C shows the monthly cost to operate each system.

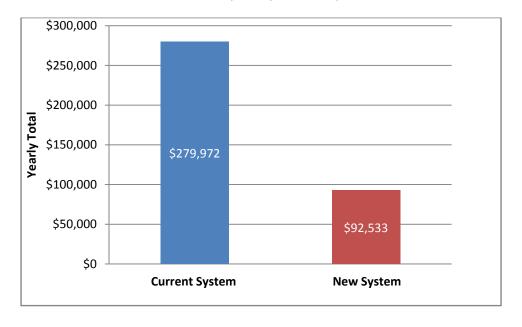


Chart 3 – Yearly Utility Cost Comparison

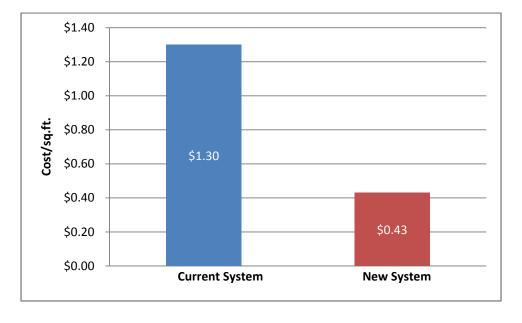


Chart 4 – Cost/ft<sup>2</sup>-yr Comparison

Table 12 showed that the new mechanical equipment cost is \$46 million more than the original system. The new system saved North Pocono \$187,439 a year in utility costs. This would result in a 245 year payback to change from the current system to the redesign.

The redesign also has an environmental advantage over the current system. Chart 5 and 6 compares the difference in emissions from each system.

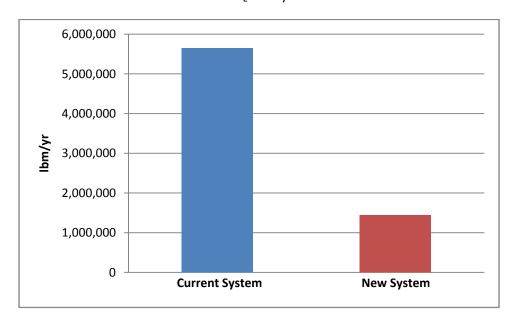
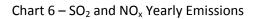
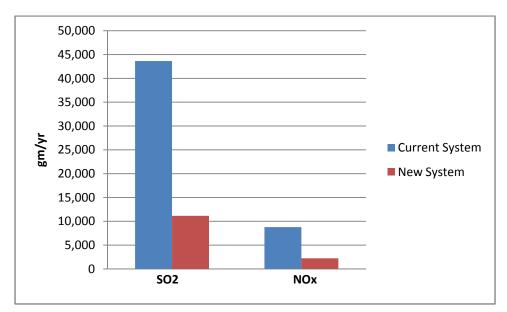


Chart 5 – CO<sub>2</sub> Yearly Emissions





## Structural Breadth

With the redesign of mechanical equipment that is placed on the roof, the structure was directly impacted by the new system. The roof is a non-composite 1.5" 20 gauge steel deck supported by steel joists that are bearing on 8" CMU walls. This breadth study kept the roof deck the same while analyzing the difference in the steel joists. The self weight of the deck is 7.0 psf with a controlling snow load of 39 psf. The equipment loads for the two systems are shown in Table 15.

Table 15 – Equipment Loads

CURRENT ROOF LOADS		REDES	IGNED ROC	F LOADS	
Unit	Weight (lbs)	Weight (lbs/ft²)	Unit	Weight (lbs)	Weight (lbs/ft²)
AHU-1	8,295	61.4	DOAS-1	4,975	43.7
AHU-2	9,360	32.8	DOAS-2	4,975	43.7
AHU-3	23,752	52.8	DOAS-3	5,575	49.0
AHU-4	2,816	33.4	AHU-4	2,816	33.4
AHU-5	4,903	45.5	DOAS-5	3,280	38.2
AHU-6	12,815	46.1	DOAS-6	3,260	38.0
AHU-7	6,602	43.2	DOAS-7	4,975	43.7
AHU-8	5,553	39.6	DOAS-8	3,260	38.0
AHU-9	8,364	41.2	DOAS-9	4,975	43.7
AHU-10	4,903	45.5	DOAS-10	3,160	36.8
AHU-11	4,891	55.7	DOAS-11	2,720	31.7
AHU-12	1,896	26.2	DOAS-12	2,855	33.3
AHU-13	9,965	32	DOAS-13	5,075	44.4
AHU-14	4,731	39.1	DOAS-14	3,160	36.8
AHU-15	8,364	41.2	DOAS-15	3,260	38.0
AHU-16	4,891	55.7	RTG-1 (3)	1,960	59.6
CU-2a	4,057	43.4	RTG-2 (2)	1,770	53.9
CU-2b	4,057	43.4	Х	Х	х
CU-3	3,998	29.4	Х	Х	х
CU-4	484	28.9	Х	Х	х
CU-5	484	28.9	Х	Х	х
CU-8	531	20.9	х	Х	х
Total	135,712	886.3	Totals	62,051	705.9

As shown above the new system reduced the total weight by 73,661 lbs which is a 55% decrease from the original roof loads. The DOAS units were placed in the same locations to ensure that the roof penetrations are not affected, and the architecture of the building is not impacted. Figure 13 shows the location of the 16 DX units while Figure 14 displays the location of the DOAS units.

AHU-13 Section 1 AHŲ-11 €U-4 ■ AHU-10 AHU-16 Section 2 Section 5 AHU-7 AHU-12 AHU-5 AHU-3 AHU-14 AHU-4 AHU-2 8-UHA AHU-9 CU-2a,b Section 4 CU-3 Section 3 АНИ-6 AHU-15

Figure 13 – Current Equipment Location

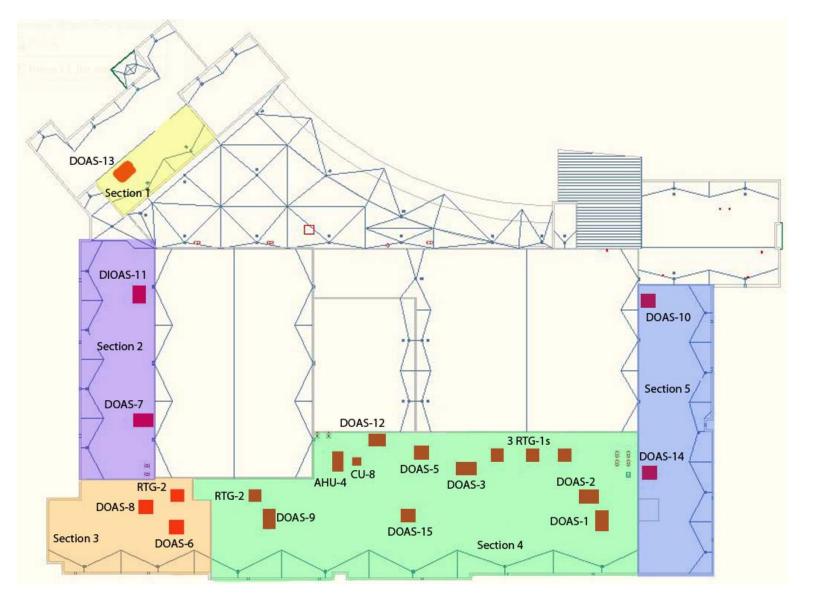


Figure 14 – New Equipment Locations

The information above was then entered into the RAM modeling program to determine the new sizes of the steel joists supporting the roof. Table 16 breaks down the 5 sections of the roof and the joists for each design scenario.

Table 16 – Roof Joist Comparison

Section	Joist Span	Joist Spacing	<b>Current Joist</b>	Redesigned Joist
Section 1	29'- 4"	5'-2"	22K9	16K2
Section 2	34'-8"	5'-8"	24K9	18K3
	13'-1"	5'-6"	16KCS3	10K1
Section3	13'-0"	5'-10 1/8"	12K3	10K1
	34'-8"	5'-7 1/2"	24k9	26k6
	13'-4"	5'-0"	16KCS3	10K1
Section 4	38'-0"	5'-7 1/2"	24K9	28k6
	13'-0"	5'-10 1/8"	12K3	10K1
	13'-0"	5'-4"	16KCS3	10K1
	11'-4"	4'-9"	16KCS3	10K1
	10'-0"	4-9"	12K5	10K1
	43'-8"	5'-6 1/2"	28K12	30K9
	10'-8"	6'-2"	12K3	10K1
	25'-8"	5'-7 1/2"	20K6	24K4
Section 5	13'-0"	5'-10 3/4"	12K3	10K1
	34'-4"	5'-9"	24K9	22K4

Table 17 is a breakdown of the roof girders that are located in those sections of the roof.

Table 17 – Girder Comparison

Section	Span	<b>Current Girder</b>	Redisgned Girder
Section1	27'-4"	W18x35	W16x26
	23'-8"	W18x35	W16x26
	29'-6"	W18x35	W16x31
	20'-4"	W16x31	W16x26
	26'-0"	W18x40	W18x35
	29'-4"	W14x22	W8x10
Section 2	23'-8"	W16x36	W8x10
Section 3	11'-4"	W12x19	W8x10
	34'-2"	W21x62	W21x19
	33'-6"	W14x22	W10x12
	12'-4"	W12x16	W8x10
	12'-0"	W12x16	W8x10
Section 4	33'-4"	W14x22	W12x14
	19'-0"	W12x19	W8x10

Table 17 – Cont.

	37'-0"	W16x31	W16x26
	20'-0"	W16x36	W14x22
	21'-4"	W16x36	W14X22
	10'-0"	W12x19	W8x10
	28'-0"	W16x26	W12x19
	15'-4"	W14x22	W8x10
	14'-8"	W14x22	W8x10
	30'-0"	W21x44	W14x22
	17'-3"	W16x36	W8x10
	29'-8"	W21x44	W21x44
	27'-8"	W21x44	W18x35
	39'-0"	W24x68	W21x44
Section 5	29'-3"	W21x44	W16x31
	28'-7"	W24x55	W24x55
	23'-3"	W18x35	W10x12
	34'-0"	W18x40	W14x22
	32'-6"	W18x40	W16x26
	13'-8"	W8x24	W8x10
_	33'-4"	W16x31	W8x10

The new system showed a reduction in the majority of the structural roof frame. The new system results in a cheaper material and construction cost. Chart 7 shows the overall savings in the reduced system while Appendix D has a breakdown of savings for the joists and girders.

\$250,000.00 \$200,000.00 \$150,000.00 \$100,000.00 \$0.00 \$0.00 Current System New System

# **Electrical Breadth**

Another building system affected by the mechanical system redesign is the electrical system. This breadth compared the electrical panels that serve the rooftop equipment as well as the major mechanical equipment in the mechanical room. There are 4- 480/277V panels that serve this equipment. Table 18 lists the current equipment that will be either changed out or eliminated because of the system redesign.

Table 18 – Current Equipment Electrical Data

Equipment	Amps	KVA
AHU-1	230.56	110.67
AHU-2	226.25	108.60
AHU-3	66.51	138.56
AHU-5	134.40	64.53
AHU-6	71.00	34.08
AHU-7	180.10	86.46
AHU-8	166.25	79.80
AHU-9	230.00	110.40
AHU-10	135.94	65.25
AHU-11	17.19	8.25
AHU-12	49.6	23.82
AHU-13	135.69	282.69
AHU-14	109.12	52.38
AHU-15	103.02	214.63
AHU-16	17.19	8.25
Pump-1	46.75	22.44
Pump-2	46.75	22.44
Pump-3	46.75	22.44
Boiler -1	6.33	13.19
Boiler -2	6.33	13.19
CU-2a	230	110.4
CU-2b	230	110.4
CU-3	75.81	157.93
CU-4	43.38	20.82
CU-5	43.38	20.82
Total	2648.3	1902.44

The redesign replaced all 16 air-handling units with 15 DOAS units. The condensing units, CU-Xs, were eliminated and one of the pumps was eliminated. The boilers were replaced by one smaller unit

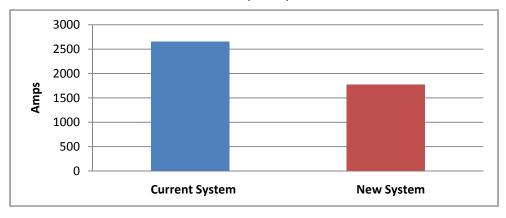
that will be served by a smaller sized panel board because it only requires 120V to run. Table 19 is list of the new equipment with their loads.

Table 19 – Redesigned Equipment Electrical Data

Equipment	Amps	KVA
DOAS-1	95.62	45.90
DOAS-2	105.63	50.70
DOAS-3	103.75	49.80
DOAS-5	67.50	32.40
DOAS-6	72.50	34.80
DOAS-7	88.12	42.30
DOAS-8	80.00	38.40
DOAS-9	175.00	84.00
DOAS-10	59.37	28.50
DOAS-11	49.37	23.70
DOAS-12	62.50	30.00
DOAS-13	292.50	140.40
DOAS-14	59.37	28.50
DOAS-15	80	38.4
Pump-1	46.75	22.44
Pump-2	46.75	22.44
RTG-1a	67.36	32.34
RTG-1b	67.36	32.34
RTG-1c	67.36	32.34
RTG-2a	40.31	19.35
RTG-2b	40.31	19.35
Total	1767.43	848.4

The new system showed a reduction in both KVA and amps. Charts 7 and 8 shows how the two systems electrical data compares to one another.

Chart 7 – Amp Comparison



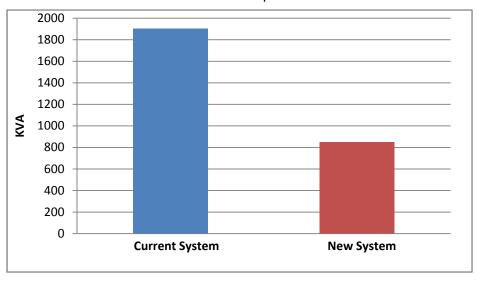


Chart 8 – KVA Comparison

When the numbers from the two systems were compared it is a 33% reduction in Amps and a 55% reduction in the KVA's needed to run the new system. Appendix E has the 4 panel boards and the current frame and feeder sizes. Appendix F has the replacement panel boards.

### Conclusions

The integrated redesign of North Pocono High School met all of the goals set prior to the start of the project. The redesign lowered the yearly energy consumption by 75%; the electrical consumption was cut by 55% a year. These reductions led to a saving of \$187.4 thousand a year in utility costs. However, the savings from the new system would not be seen until 245 years because the redesign was \$46 million more up front than the original design. The higher initial cost was due to the size of the ground loop. The ground loop could be reduced by adding a cooling tower and chiller to assist during the cooling season, and increasing the size of the boiler to provide more than auxiliary heating. The addition of this equipment would decrease the ground loop and thus decrease the cost of installing it. In an ever-growing environmentally conscious society it is important to see how building systems are affecting the environment. The new system emits 75% less pollutants a year than the current design. The smaller roof frame saved 17% of the initial cost. Overall, the redesign has numerous advantageous over the current system, however in today's world the financial benefits still drives the majority of the industry. From a financial standpoint it would be recommended that North Pocono keep the current system.

### References

ASHRAE, 2007, ANSI/ASHRAE, <u>Standard 62.1-2007</u>, <u>Ventilation for Acceptable Indoor Air Quality</u>. American Society of Heating, Refrigerating, and Air Conditioning Engineers, Inc. Atlanta, GA. 2007.

ASHRAE, 2007, ANSI/ASHRAE, <u>Standard 90.1-2007</u>, <u>Energy Standard for Buildings Except Low-Rise Residential Buildings</u>. American Society of Heating, Refrigerating, and Air Conditioning Engineers, Inc. Atlanta, GA. 2007.

Carrier Console Heat Pump Literature.

http://www.docs.hvacpartners.com/idc/groups/public/documents/techlit/50pec-2pd.pdf

Carrier Dedicated Outdoor Air System Literature.

http://www.docs.hvacpartners.com/idc/groups/public/documents/techlit/62d-1apd.pdf

Carrier Heat Pump Literature.

http://www.docs.hvacpartners.com/idc/groups/public/documents/techlit/ca161.pdf

Carrier Rooftop Water Source Heat Pump.

http://www.docs.hvacpartners.com/idc/groups/public/documents/techlit/50rtg-2pd.pdf

GPI Inc., 2007. Mechanical Specifications. GPI Inc., Scranton, PA. 2008.

Geokiss. GCHPCalc. Northport, AL.

Mumma, Stanley, <u>Overview of Integrating Dedicated Outdoor Air Systems with Parallel Terminal Systems</u>. American Society of Heating, Refrigerating, and Air Conditioning Engineers, Inc. Atlanta, GA. 2003.

PP&L Electric Utilities Corporation, <u>Rates Schedule LP-4</u>. 2008. <u>http://www.pplelectric.com/NR/rdonlyres/C17294DC-59A1-4ADC-B566-29CA965528AA/0/rate lp4 r.pdf</u>

Trane, <u>Trace 700</u>. Trane Inc. Piscataway, New Jersey.

# Appendix A – Air Handler Ventilation

Air Handler 1	SA cfm = 15,850	Min OA c	fm = 4,335
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Corridor-D001	Corridor	55	210
FCS Lab-D014	Classroom	460	405
Storage-D016	Storage	50	40
Classroom-D017	Classroom	350	350
Classroom-D018	Classroom	350	350
Electrical-D025	Electrical	15	10
Business Room-D113	Classroom	350	345
Business Lab-D114	Computer Lab	480	345
Classroom-D117	Classroom	350	345
Corridor-D118	Corridor	85	90
Room-D120		170	135
Classroom-D121	Classroom	350	345
Classroom-D122	Classroom	350	345
Classroom-D123	Classroom	350	345
Electrical-D133	Electrical	15	10
Corridor-A101	Corridor	75	60
Training-A105	Classroom	70	90
Office-A106	Office	40	30
Classroom-A107	Classroom	390	345
Total		4,355	4,195

Air Handler 2	SA cfm = 16,415	Min OA c	fm = 7,675
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Faculty Room-D027	Office	375	310
Classroom-D010	Classroom	550	345
Classroom-D011	Classroom	570	360
Faculty Room-D135	Office	375	310
SGI-D136	Classroom	205	105
Classroom-D137	Classroom	560	350
Classroom-D138	Classroom	560	350
SGI-D139	Classroom	205	105
Aerobics-D140	Aerobics	810	670
Corridor-D001	Corridor	50	210
General Science-D106	Classroom	625	405
Storage-D107	Storage	20	15
Classroom-D109	Classroom	625	405
Classroom-D110	Classroom	550	345
Business Lab-D111	Computer Lab	550	345
Electrical Room-D250	Storage	180	50
Classroom-D206	Classroom	550	345
Total		7,360	5,025

Air Handler 3	SA cfm = 36,000	m = 10,270	
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Tickets-D226	Office	100	20
Gymnasium-D125	Gymnasium	9,005	4,475
Lobby - A202	Lobby	1,165	315
Total		10,270	4,810

Air Handler 4	SA cfm = 3,700	Min OA cfm = 3,700	
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Women's Team Room-D143	Conference	260	105
Coaches' Office-D144	Office	270	25
Women's Locker-D148	Conference	410	145
Instructor's Office-D149	Office	270	35
Men's Locker-D151	Conference	410	145
Instructor's Office-D152	Office	270	35
Men's Team Room-D156	Conference	260	105
Coaches' Office-D157	Office	270	25
Weight Room-D158	Weights	1,090	510
Corridor	Corridor	150	130
Corridor	Corridor	150	130
Total		3,810	1,390

Air Handler 5	SA cfm = 6,800	Min OA c	fm = 3,945
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Control Room-D232	Media Center	85	35
Studio-D233	Office	80	30
Corridor-D237	Corridor	80	95
Choral Room-D238	Music	1,225	1,100
Health-D240	Classroom	550	350
Music Classroom-D242	Music	375	255
Practice-D243	Music	100	60
Practice-D244	Music	100	60
Practice-D245	Music	100	60
Music Classroom-D246	Music	340	255
Music Office-D247	Office	275	65
Musice Lab-D248	Music	550	385
Total		3,860	2,750

Air Handler 6	SA cfm = 19,500	Min OA cf	m = 19,500
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Auditorium -C209	ıditorium Seati	17,760	2,645
Stage-C231	Stage	1,780	220
Total		19,540	2865

Air Handler 7	SA cfm = 13,500	Min OA cfm = 4,355	
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Corridor-C201	Corridor	175	135
Corridor-C202	Corridor	90	95
Corridor-C203	Corridor	90	70
Classroom-C210	Classroom	350	350
Classroom-C211	Classroom	350	345
Classroom-C212	Classroom	350	345
Classroom-C213	Classroom	350	345
Classroom-C214	Classroom	350	345
Classroom-C215	Classroom	350	345
Classroom-C216	Classroom	350	345
Classroom-C217	Classroom	390	345
Classroom-C218	Classroom	390	345
Classroom-C219	Classroom	390	345
Classroom-C220	Classroom	390	345
Classroom-C221	Classroom	390	345
Dressing Room-C225	Office	20	40
Dressing Room-C230	Office	25	40
Total		4,800	4,525

Air Handler 8	SA cfm = 13,500	Min OA cfm = 4,355	
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Corridor-C101	Corridor	70	85
Classroom-C103	Classroom	410	345
Classroom-C104	Classroom	410	345
Classroom-C105	Classroom	410	345
Classroom-C106	Classroom	410	345
Electrical-C115	Electrical	15	10
Classroom-C118	Classroom	370	350
Classroom-C119	Classroom	370	345
Classroom-C120	Classroom	370	345
Classroom-C121	Classroom	370	345
Classroom-C122	Classroom	370	345
Classroom-C123	Classroom	370	345
Classroom-C124	Classroom	370	345
Total		4,315	3,895

Air Handler 9	<b>SA cfm = 14,195</b>	Min OA cfm = 6,245	
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Chemistry-C222	Science Lab	500	710
Science Prep-C223	Classroom	135	65
Chemistry-C224	Science Lab	550	480
Earth Science-C107	Science Lab	500	710
Science Prep-C108	Science Lab	80	80
Earth Science-C109	Science Lab	605	480
Corridor-C001	Corridor	85	85
Classroom-C003	Clasroom	560	345
Classroom-C004	Clasroom	560	345
Art Classroom-C005	Art Class	840	595
Storage-C006	Storage	100	40
Art Classroom-C008	Art Class	750	600
Corridor-C011	Corridor	60	60
Corridor-C018	Corridor	30	30
Classroom-C020	Clasroom	435	350
Classroom-C021	Clasroom	435	345
Total		6,225	5,320

Air Handler 10	SA cfm = 8,565	Min OA cfm = 3,77		
		OA <sub>sup</sub>	ASHRAE	
Space	Use	(cfm)	Value	
Corridor - A203	Corridor	45	45	
Police - A205	Office	75	30	
Waiting - A206	Reception	220	70	
Adminstrative Area - A207	Reception	215	65	
Work/Break Room - A208	Break	210	55	
Storage - A209	Storage	75	15	
Corridor - A210	Corridor	240	25	
Adminstrative Area - A211	Reception	255	45	
Vice Priniciple -A214	Office	95	40	
Office - A215	Office	150	40	
Principal's Office- A216	Office	190	65	
Conference Room-A217	Conference	380	115	
Waiting - A218	Reception	65	65	
Nurses Office-A219	Office	165	65	
Cot-A220	Classroom	65	65	
Exam Room - A222	Office	95	25	
Storage - A224	Storage	20	20	
Hearing-A225	Office	100	45	
Cot-A226	Classroom	65	50	
Corridor-D211	Corridor	60	150	
Corridor-D216	Corridor	25	25	
Conference Room-D217	Conference	220	65	
Office-D218	Office	75	40	
Office-D219	Office	70	30	
Office-D220	Office	75	40	
Conference Room-D221	Conference	120	120	
File Room-D222	Storage	25	25	
Office-D223	Office	70	40	
Office-D224	Office	70	40	
Adminstrative Wating-D225	Reception	105	105	
Kitchenette-D271	Coffee Station	45	45	
Total		3,685	1,670	

Air Handler 11	SA cfm = 3,000	Min OA c	fm = 3,000
Space	Use OA <sub>sup</sub> (cfm)		ASHRAE Value
LGI-C208	Multi-Use	2,750	470

Air Handler 12	SA cfm = 3,800	Min OA cfm = 2,2		
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value	
Corridor-D249	Corridor	230	200	
Band Room-D254	Music	2,000	1,890	
Corridor-D274	Corridor	25	25	
Total	2,255	2400		

Air Handler 13	SA cfm = 18,200 Min OA cfm = 10,8				
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value		
Corridor-B202	Corridor	160	40		
Cafeteria-B203	Cafeteria	8,640	4,375		
Faculty Dining	Cafeteria	540	270		
Food Court-B208	Cafeteria	1,250	360		
Office-B214	Office	25	20		
School Store	Store	110	40		
Total	Total				

Air Handler 14	SA cfm = 10,300	Min OA c	fm = 2,575
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
Storage-D207	Storage	105	50
Computer Lab-D208	Computer Lab	720	440
Library-D209	Library	1,120	965
Office-D210	Office	130	55
Corridor-D211	Corridor	60	120
Classroom-D212	Classroom	285	345
Electrical Room-D235	Electrical	50	10
Total		2,470	1,985

Air Handler 15	SA cfm = 15,300	Min OA cfm = 6,12		
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value	
Physics-D203	Classroom	630	405	
Science Prep-D204	Classroom	145	65	
Physics-D205	Classroom	585	405	
Corridor-D101	Corridor	270	215	
Biology Classroom-D103	Classroom	630	405	
Science Prep-D104	Classroom	245	65	
Biology Classroom-D105	Classroom	585	405	
Electrical-C016	Electrical	90	10	
Corridor-D001	Corridor	80	210	
Communication Lab-D003	Computer	705	520	
Press Room-D004	Office	330	50	
Dark Room-D005	Classroom	75	75	
CADD Lab-D007	Computer	570	395	
Wood Shop-D008	Wood Shop	750	670	
Custodial BreakRoom	BreakRoom	200	55	
Total		5,890	3,950	

Air Handler 16	SA cfm = 3,000	Min OA c	fm = 3,000
Space	Use	OA <sub>sup</sub> (cfm)	ASHRAE Value
LGI-C208	Multi-Use	2,750,5	465

# Appendix B – Monthly Energy Consumption

Table B1 – Current System

Utility		Jan.	Feb.	Mar.	Apr.	May	June
Electricity	On-Pk Cons. (kWh)	305,564	281,327	307,909	132,569	185,980	244,396
	On-Pk Dem. (kW)	718	631	874	1,068	1,732	1,961
Oil	Cons. (therms)	15,666	18,995	9,814	4,268	1,153	618

Utility		July	Aug.	Sept.	Oct.	Nov.	Dec.
Electricity	On-Pk Cons. (kWh)	196,354	10,715	184,177	144,000	165,781	2,461,314
	On-Pk Dem. (kW)	2,191	326	1,932	1,228	1,086	2,191
Oil	Cons. (therms)	217	0	1,096	4,422	6,071	12,094

Table B2 – Redesigned System

Utility		Jan.	Feb.	Mar.	Apr.	May	June
Electricity	On-Pk Cons. (kWh)	111,134	109,432	88,717	71,274	93,038	117,034
	On-Pk Dem. (kW)	549	594	500	454	696	789
Gas	Cons. (therms)	16	15	14	8	9	0

Utility		July	Aug.	Sept.	Oct.	Nov.	Dec.
Electricity	On-Pk Cons. (kWh)	101,469	10,519	93,781	77,860	77,306	96,078
	On-Pk Dem. (kW)	832	325	758	501	463	504
Gas	Cons. (therms)	0	0	8	9	12	16

### Appendix C – Monthly Energy Cost

Table C1 - Current System

Utility		Jan.	Feb.	Mar.	Apr.	May	June
Electricity	Total (\$)	17,315	16,676	18,442	19,860	24,711	26,384
Oil	Cons. (\$)	6,266	7,598	3,926	1,707	247	87

Utility		July	Aug.	Sept.	Oct.	Nov.	Dec.	Total
Electricity	Total (\$)	28,064	14,438	26,172	21,028	19,991	17,500	250,581
Oil	Cons. (\$)	87	0	439	1,769	2,428	4,837	29,391

Table C2 - Redesigned System

Utility		Jan.	Feb.	Mar.	Apr.	May	June
Electricity	Total (\$)	8,404	8,665	7,161	6,136	8,764	10,390
Gas	Cons. (\$)	25	24	23	18	18	11

Utility		July	Aug.	Sept.	Oct.	Nov.	Dec.	Total
Electricity	Total (\$)	10,090	2,795	9,246	6,740	6,440	7,481	92,312
Gas	Cons. (\$)	11	11	18	18	20	24	221

### Appendix D – Structural Cost Analysis

Table D1 - Current Joist Estimate

Joist	<b>Total Liner Feet</b>	Cost/L.F.	Total Cost (\$)
12K3	1349.99	10.04	13,553.90
12K5	60	10.28	616.80
16KCS3	1247.25	9.67	12,060.91
20K6	102.666	10.68	1,096.47
22K9	439.995	13.18	5,799.13

28K12	1091.665 <b>Total</b>	17.26	18,842.14 <b>119,931.60</b>
24K9	4745.967	14.32	67,962.25

Table D2 – Redesigned Joist System

Joist	<b>Total Liner Feet</b>	Cost/L.F.	Total Cost (\$)
10K1	2706.239	10.78	29,173.26
16K2	439.995	9.67	4,254.75
18K3	1039.98	10.38	10,794.99
22K4	1132.989	11.18	12,666.82
24K4	102.666	11.52	1,182.71
26K6	623.999	12.27	7,656.47
28K6	1900	13.66	25,954.00
30K9	1091.665	14.06	15,348.81
	Total		107,031.81

Table D3 – Current Girder Estimate

Girder	Total ft <sup>2</sup>	Cost/ft <sup>2</sup>	Total Cost (\$)
W8x24	9.11	54.50	496.50
W12x16	24.333	36.00	875.99
W12x19	40.333	41.50	1,673.82
W14x22	108.304	53.00	5,740.11
W16x26	37.33	53.00	1,978.49
W16x31	120.888	63.50	7,676.39
W16x36	109.665	72.00	7,895.88
W18x35	155.623	72.00	11,204.86
W18x40	138.75	81.00	11,238.75
W21x44	151.519	87.50	13,257.91
W21x62	59.792	121.00	7,234.83
W24x55	57.167	107.00	6,116.87
W24x68	78	130.00	10,140.00
Total			85,530.39

Table D4 – Redesigned Girder Estimate

Girder	Total ft <sup>2</sup>	Cost/ft <sup>2</sup>	Total Cost (\$)
W8x10	141.054	28.50	4,020.04
W10x12	47.292	32.00	1,513.34
W12x14	33.333	35.00	1,166.66
W12x19	228	41.50	9,462.00
W14x22	122.889	53.00	6,513.12
W16x26	187.776	53.00	9,952.13
W16x31	78.333	63.50	4,974.15
W18x35	80.499	72.00	5,795.93
W21x19	59.792	41.50	2,481.37
W21x44	120.167	87.50	10,514.61
W24x55	57.167	107.00	6,116.87
Total			62,510.21

## Appendix E – Current Panel Boards

DESIGNATION:	VOLTA	GE:	480/27	77V-3PH-4	W			LOCATION: ELEC. RM.							
	MAINS	:	1200	A				FED BY:		MDP					
<b>M4U1</b>	TYPE:		MOT					FEEDER SIZE: 4 SETS OF 4#500,1#4/0G, IN 3"C (AL)							
W14U1	O.C. DI	VICE:	MLO	(1200A C	B IN MAIN	SWBD)		MINIMUM	I O.C. DEV	/ICE					
	MOUN	TING:	SURF	ACE				INTERRU	PTING RA	TING	: 65,000	)			
	O.C.			KVA		KVA		KVA			O.C.				
Description	CKT	AMP	P		4	]	В	•	<u> </u>	P	AMP	CKT	Description		
	1	ļ		25.27	36.80					ļ		2			
CONDSNER CU-3	3	150	3			25.27	36.80			3	200	4	AIR HAND AHU-9		
	5							25.27	36.80	ļ		6			
	7			21.51	34.34							8			
AIR HAND AHU-5	9	110	3			21.51	34.34			3	200	10	AIR HAND AHU-15		
	11							21.51	34.34			12			
	13			28.82	26.60							14			
AIR HAND AHU-7	15	150	3			28.82	26.60			3	125	16	AIR HAND AHU-8		
	17							28.82	26.60			18			
	19			23.17	11.36							20			
EX. FAN EF-2	21	125	3			23.17	11.36			3	70	22	AIR HAND AHU-6		
	23							23.17	11.36			24			
	25			0.83	0.83							26			
EXHAUST FAN EF-5	27	20	3			0.83	0.83			3	20	28	EXHAUST FAN EF-17		
	29							0.83	0.83			30			
	31			7.94	0.55					1	20	32	EXHAUST FAN EF-1		
AIR HAND AHU-12	33	40	3			7.94	0.83					34			
	35							7.94	0.83	3	20	36	EXHAUST FAN EF-17		
	37				0.83							38			
SPARE BREAKER	39	20	3							1	20	40	SPACE		
	41									1	20	42	SPACE		
	TOTAL	TOTAL KVA/PHASE			218.86 218.30			218.30 TOTAL KVA					655.47		
										-	TOTAL	AMP	788.41		

DESIGNATION:	VOLTA	GE:	480/27	77V-3 <b>PH</b> -4	W			LOCATION: ELEC. RM.						
	MAINS	:	1200	A				FED BY: MDP						
<b>M4U1</b>	TYPE:		MOTORS 1						SIZE:	4 SE	TS OF 4	#500,1#	4/0G, IN 3"C (AL)	
W14U1	O.C. DI	VICE:	MLO	(1200A C	B IN MAIN	SWBD)		MINIMUM	I O.C. DE	VICE				
	MOUN	TING:	SURF	ACE		INTERRU	PTING RA	ATING	: 65,000					
	_													
<b>.</b>	OT T	O.C.			VA ^		VA		VA.	١.,	O.C.	OTT		
Description	CKT AMI		P	,	A		В	<u> </u>	C	P	AMP		Description	
	43	<u> </u>		2.11	10.58					<b>_</b>	ļ	46		
AHU-4	45	30	3			2.11	10.58			3	30	48	CU-8	
	47							2.11	10.58			50		
	49										Ī	52		
SPACE	51	80	3							3	125	54	SPARE BREAKER	
	53		Ī								Ī	56		
	55											58		
SPACE	57	110	3							3	100	60	SPACE	
	59											62		
	TOTAL	KVA/P	HASE	12	.68	12	.68	12	.68		TOTAL	KVA	38.05	
					•			•		_	TOTAL	AMP	45.77	
										TOT	AL PAN	EL KVA	693.52	
										TOT	AL PANI	EL AMP	834.17	

7.7.4774	MAINS	:	1200. MOT					FED BY:	T.T.	MDP	TO OF 1	11500.111	AVOC DI SUCCATA	
<b>M4U2</b>	TYPE:	лист.			B IN MAIN	CMDD		FEEDER SIZE: 4 SETS OF 4#500,1#4/0G, IN 3"C (AL) MINIMUM O.C. DEVICE						
MITCE	MOUNT		SURF		B IIN MIAIIN	SWBD)		INTERRUPTING RATING: 65,000						
	MOUN	IIIVG:	SURF	ACE			INTERROFTING RATING: 05,000							
		O.C.		K	VA.	K	VA	K	V <b>A</b>		O.C.			
Description	CKT	AMP	P		4	]	В	(		P	AMP	CKT	Description	
	1			36.80	22.17							2		
CU-2A	3	225	3			36.80	22.17			3	100	4	AHU-3	
	5							36.80	22.17			6		
	7			36.20	36.89					Ī		8		
AHU-2	9	200	3			36.20	36.89			3	200	10	AHU-1	
	11							36.20	36.89			12		
	13			21.75	17.46							14		
AHU-10	15	110	3			21.75	17.46			3	90	16	AHU-14	
	17							21.75	17.46			18		
	19			5.83	2.11							20		
WOOD SHOP BUS	21	60	3			5.83	2.11			3	20	22	LIFT STATION	
	23							5.83	2.11			24		
	25			17.21	3.88							26		
PANEL M2L1	27	225	3			14.06	3.88			3	100	28	AC-1	
	29							13.13	3.88			30		
	31			7.20								32		
DC-1	33	50	3			7.20				3	80	34	SPARE BREAKER	
	35							7.20				36		
SPACE	37	20	1							1	20	38	SPACE	
SPACE	39	20	1							1	20	40	SPACE	
SPACE	41	20	1							1	20	42	SPACE	
	TOTAL	KVA/PI	ASE	207.52 204.36			203.44 TOTAL KVA				615.31			
										_	TOTAL	AMP	740.10	

DESIGNATION:	VOLTA	GE:	480/27	77V-3PH-4	W			LOCATIO	N: MID L	EVEL				
	MAINS	:	1200	A				FED BY: MDP						
TATIO	TYPE:		MOT					FEEDER SIZE: 4 SETS OF 4#500,1#4/0G, IN 3"C (AL)						
<b>M4U2</b>	O.C. DE	VICE:	MLO	O (1200A CB IN MAIN SWBD)				MINIMUM	O.C. DE	VICE				
	MOUNT	TING:	SURF	FACE				INTERRU	PTING RA	ATING	: 65,000	1		
•		O.C.		K	VA	K	VA.	KV	7A		O.C.			
Description	CKT	AMP	P	,	Ą	]	В	(		P	AMP	CKT	Description	
	1			36.80	22.05							2		
CU-2B	3	225	3			36.80	22.05			3	200	4	PANEL M2L1 XFMR	
	5							36.80	22.05			6		
	7											8		
SPARE BREAKER	9	225	3							3	100	10	SPARE BREAKER	
	11											12		
	13											14		
SPACE	15	100	3							3	100	16	SPACE	
	17											18		
	TOTAL	KVA/P	HASE	58	.85	58	.85	58.	.85		TOTAL	KVA	176.56	
											TOTAL	AMP	212.37	
										TOT	AL PAN	EL KVA	791.87	
										TOT	AL PAN	EL AMP	952.47	
										DIVE	RSITY		0.85	

DESIGNATION:	VOLTA			7V-3PH-4	W			LOCATIO	ON: MAIN			OOM	
	MAINS	:	600A					FED BY:		MDP			
<b>M4U3</b>	TYPE:		MOTO					FEEDER S			TS OF	4#350,1	#1/0G, IN 3"C (AL)
W14U3					IN MAIN S	SWBD)			I O.C. DEV				
	MOUN	TING:	SURF.	ACE				INTERRU	PTING RA	TING	65,000	)	
		0.C.			VA		VA		VA		O.C.		
Description	CKT	AMP	P		A		В		C	P	AMP		Description
				7.48	7.48					ļ <u>.</u>		2	
PUMP P-2	3	50	3			7.48	7.48			3	50	4	PUMP P-3
				244	12.22			7.48	7.48	ļ		6	
	7	ļ <u> </u>		2.11	45.23			-		ļ <u>.</u>		8	
BOILER B-1	9	20	3			2.11	45.23	- 101	ļ	3	250	10	AIR HAND AHU-13
	11	ļ		2.22				2 🕸	45.23	}		12	
	13			3.88	6.94		4.0.1	_		ļ <u>.</u>		14	
KITCHEN AIR MAU-1	15	30	3			3.88	6.94			3	40	16	CONDENSER CU-4
	17							3.88	6.94	ļ		18	
	19			2.75	6.94		40.	-		ļ <u>.</u>		20	
AIR HAND AHU-11	21	40	3			2.75	6.94			3	40	22	CONDENSER CU-5
	23							2.75	6.94	ļ		24	
	25			2.75	1.33		4.00			ļ		26	
AIR HAND AHU-16	27	40	3			2.75	1.33	2.75	1.22	3	20	28	EX. FAN EF-21
	29			1.22	1.22			2.75	1.33	ļ		30	
EV EASIEE 20	31	20		1.33	1.33	1.22	1.22			3	20	32	EV FAMEE 31
EX. FAN EF-20	33	20	3			1.33	1.33	1.22	1.33		20	34 36	EX. FAN EF-21
SPACE	35 37	20						1.33	1.33	1	20	38	SPACE
SPACE	39	20	1							1	20	- 38 - 40	SPACE
SPACE	41	20	1							1	20	40	SPACE
STACE			l	9.0	.55	80	.55	80	.55	1			<b>—</b>
	TOTAL	KVA/PI	HASE	03	. 33	53	. 22	59	. 33	J	TOTAL		268.64 323.12

DESIGNATION:	VOLTA	GE:	480/27	7V-3PH-4	W			LOCATIO	N: MAIN	ELEC:	TRIC R	ООМ	
	MAINS	:	600A					FED BY:		MDP			
<b>M4U3</b>	TYPE:		MOTO	ORS				FEEDER S	IZE:	2 SI	TS OF	4#350,1	#1/0G, IN 3"C (AL)
W14U3	O.C. DI	VICE:	MLO	(500A CB	IN MAIN	SWBD)		MINIMUM	I O.C. DE	VICE			
	MOUN	TING:	SURF.	ACE				INTERRU	PTING R	ATING	: 65,000	)	
		O.C.			VA	K	VA	K	VA		O.C.		
Description	CKT	AMP	P	i	Δ	]	В	(	<u> </u>	P	AMP	CKT	Description
	43			3.33	0.83					1	20	44	EX. FAN EF-12
CONDSER CU-6	45	20	3			3.33	0.28					46	
	47							3.33	0.28	3	20	48	EX. FAN EF-27
	49			2.13	0.28							50	
PANEL M2U1	51	60	3			2.14	1.18					52	
	53							1.89		3	20	54	AIR COMPRESSOR
	55							"				56	
SPARE BREAKER	57	20	3							1	20	58	
	59									1	20	60	SPACE
	TOTAL	KVA/P	HASE	6.	57	6.	92	5.	49		TOTAL	. KVA	18.97
			•								TOTAL	AMP	22.82
										TOT	AL PAN	EL KVA	287.61
													0.83
										TOT	AL PAN	EL AMP	345.94
										DIVE	RSITY		0.85

Panel EQ4U1

DESIGNATION:	VOLTA MAINS		225A	7V-3PH-4V	N .			LOCATIO FED BY:	IN: IVIAIIN	MDP			
TO ITIA		•		GENCY				FEEDER S	175.			1 IN 2 5	"C (AL)
EO4U1		VICE.			DDEARTI	R IN ED4U	1)	MINIMUM	·		00,1#20	7, II 1 2.3	C (AL)
LVICI	MOUNT		SURF		DIVEARE	X IIV ED4U.	1)	INTERRU			65 000		
	MOUNT	IIIO.	30ICI	ACE				INTERRO	TINGK	IIIII	. 03,000		
		O.C.		KV	VA.	K	VA	KV	VA.		O.C.		
Description	CKT	AMP	P	1	4	]	В	(	C	P	AMP	CKT	Description
	1			5.82	7.48							2	
WELL PUMP	3	40	3			5.82	7.48			3	50	4	PUMP P-1
	5							5.82	7.48			6	
	7			0.28	3.33							8	
FUEL PUMP FOP-1	9	20	3			0.28	3.33			3	20	10	CU-7
	11							0.28	3.33			12	
	13			2.11	0.44							14	
3-2	15	20	3			2.11	0.44			3	20	16	BC-2
	17							2.11	0.44			18	
	19			11.70	9.37							20	
3P-1	21	60	3			11.70	10.28			3	80	22	PANEL EQ2U3
	23							11.70	10.77			24	
	25									1	20	26	SPACE
SPARE BREAKER	27	20	3							1	20	28	SPACE
	29									1	20	30	SPACE
	TOTAL	KVA/PI	HASE	40.	.52	41	.43	41.	.92		TOTAL	L KVA	123.88
					·					_	TOTAL	L AMP	149.00

### Main Switch Board

MAIN		MAIN SWITE	CHBOARD	OMSB41S0	CHEDULE				(NORMAL)	)	
ELECTRIC	RM										
VOLTAGE:	277/480	3	PHASE		4 VIRE				65,000		AIC
MAIN BUS:	SIZE: 4000A	l l	JEUTRAL:		FULL		GROUND	BUS:	FULL		
MAIN DEVI	CE: "4000A M	ICB I	иоитіng:		SURFACE						
CIRCUIT			OVERO	CURRENT	DEVICE						
NUMBER	LOADITE	М	FRAME	TRIP	POLE	F	EEDER SI	ZE		REMARKS	3
1	FIRE PUMP 1	ΓAΡ			3	SEEF	RISER DIA	GRAM			
2	M4U1		1200	1200	3	SEEP	ANEL SCH	HEDULE			
3	M4U2		1200	1200	3	SEEP	ANEL SCH	HEDULE			
4	M4U3		600	500	3	SEEP	ANEL SCH	HEDULE			
5	ED4U1		600	600	3	SEEP	ANEL SCH	HEDULE			
6	K4U1		600	600	3	SEEP	ANEL SCH	HEDULE			
7	L4U1/L4M1/I	.4L1	600	600	3	SEEP	ANEL SCH	HEDULE			
8	L4U2/L4M2/I	L4L2	600	400	3	SEEP	ANEL SCH	HEDULE			
9	L4U3		100	100	3	SEEP	ANEL SCH	HEDULE			
10	L4U4		100	100	3	SEEP	ANEL SCH	HEDULE			
11	EQ4U1		225	225	3	SEEP	ANEL SCH	HEDULE			
12	E4U1		225	125	3	SEEP	ANEL SCH	HEDULE			
13	R2U4 XFM	ER	100	60	3	SEEF	RISER DIA	GRAM			
14	SPARE		400	400	3						
15	SPACE		600	600	3						
16	SPACE		400	400	3						

# Appendix F – New Panels

DESIGNATION:	VOLTA	GE:	480/27	77V-3PH-4V	W			LOCATIO	N: ELEC.	RM.			
	MAINS	:	800A					FED BY:		MDP	•		
<b>M4U1</b>	TYPE:		MOT					FEEDER S	IZE:	4 SET	rs of 4#	<sup>‡</sup> 2/0, 1#0	G, IN 2.5" C (CU)
W14 U 1					IN MAIN S	SWBD)		MINIMUM					
	MOUN	TING:	SURF	ACE				INTERRU	PTING RA	TING	: 65,000	)	
		O.C.		K	VA.	K	VA.	K	VA.		O.C.		1
Description	CKT	AMP	P		Ą	1	3	(		P	AMP	CKT	Description
	1			10.00	28.00							2	
DOAS-12	3	70	3			10.00	28.00			3	200	4	DOAS-9
	5							10.00	28.00			6	
	7			10.80	12.80							8	
DOAS-5	9	70	3			10.80	12.70			3	200	10	DOAS-15
	11							10.80	12.80			12	
	13			14.10	12.80							14	
DOAS-7	15	90	3			14.10	12.80			3	80	16	DOAS-8
	17							14.10	12.80			18	
	19			23.17	11.60							20	
EX. FAN EF-2	21	125	3			23.17	11.60			3	80	22	DOAS-6
	23							23.17	11.60			24	
	25			0.83	0.83							26	
EXHAUST FAN EF-5	27	20	3			0.83	0.83			3	20	28	EXHAUST FAN EF-17
	29							0.83	0.83			30	
	31				0.55					1	20	32	EXHAUST FAN EF-1
SPARE BREAKER	33	40	3				0.83					34	
	35								0.83	3	20	36	EXHAUST FAN EF-17
	37				0.83							38	
SPARE BREAKER	39	20	3							1	20	40	SPACE
	41									1	20	42	SPACE
	TOTAL	KVA/PI	IASE	128	5.32	125	.66	125	.76		TOTAL	L KVA	377.74
										-	TOTAL	L AMP	454.35

DESIGNATION:	VOLTA	GE:	480/27	77V-3PH-4	W			LOCATIO	ON: ELEC.	RM.			
	MAINS	:	800A					FED BY:		MDP	)		
<b>M4U1</b>	TYPE:		MOT	ORS				FEEDER S	SIZE:	4 SET	rs of 4#	‡2/0, 1#	tOG, IN 2.5" C (CU)
W14 U 1	O.C. DE	VICE:	MLO	(800A CE	IN MAIN S	SWBD)		MINIMUM	I O.C. DE	VICE			
	MOUNT	TING:	SURF	ACE				INTERRU	PTING R	ATING	: 65,000	)	
		O.C.		K	VA	K	VA	K	VA	Т	O.C.		Τ
Description	CKT	AMP	P		A		В		С	P	AMP	CKT	Description
	43			2.11	10.58							46	
AHU-4	45	30	3			2.11	10.58			3	30	48	CU-8
	47							2.11	10.58			50	
	49							Ï			<u> </u>	52	
SPACE	51	80	3							3	125	54	SPARE BREAKER
	53										<u> </u>	56	
	55							Î				58	
SPACE	57	110	3							3	100	60	SPACE
	59											62	
	TOTAL	KVA/P	HASE	12	.68	12	.68	12	.68		TOTAL	KVA	38.05
											TOTAL	AMP	45.77
										TOT	AL PAN	EL KVA	415.79
										TOT	AL PAN	EL AMP	500.12
										DIVE	RSITY		0.85

DESIGNATION:	VOLTA			77V <b>-3PH-4</b>	W			LOCATIO	N: MID LE				
	MAINS	_	800A					FED BY:		MDP			
<b>M4U2</b>	TYPE:		MOT					FEEDER SI			S 4#500	,1#0G, I	N 3" C (AL)
111402					IN MAIN S	SWBD)		MINIMUM					
	MOUN	TING:	SURF	ACE				INTERRUF	TING RAT	ING:	65,000		
	1	O.C.		K	VA	K	VA	KV	7 <b>A</b>		O.C.		
Description	CKT	AMP	P		A	]	В	(		P	AMP	CKT	Description
	1			6.45	16.60							2	
RTG-2	3	50	3			6.45	16.60			3	125	4	DOAS-3
	5							6.45	16.60			6	
	7			16.90	15.30							8	
DOAS-2	9	125	3			16.90	15.30			3	100	10	DOAS-1
	11	Ī						16.90	15.30			12	
	13			9.50	9.50							14	
DOAS-10	15	60	3			9.50	9.50			3	60	16	DOAS-14
	17							9.50	9.50			18	
	19			5.83	2.11							20	
WOOD SHOP BUS	21	60	3			5.83	2.11			3	20	22	LIFT STATION
	23							5.83	2.11			24	
	25			17.21	3.88			İ				26	
PANEL M2L1	27	225	3			14.06	3.88			3	100	28	AC-1
	29							13.13	3.88			30	
	31			7.20	6.45							32	
DC-1	33	50	3			7.20	6.45			3	50	34	RTG-2
	35							7.20	6.45			36	
SPACE	37	20	1							1	20	38	SPACE
SPACE	39	20	1							1	20	40	SPACE
SPACE	41	20	1							1	20	42	SPACE
	TOTAL	KVA/PI	IASE	111	6.93	113	3.78	112	.85		TOTAL	KVA	343.57
										-	TOTAL	AMP	413.25

DESIGNATION:	VOLTA	GE:	480/27	7V-3PH-4	W			LOCATI	ON: MID L	EVEL			
	MAINS	:	800A					FED BY:		MDP	•		
<b>M4U2</b>	TYPE:		MOTO	ORS				FEEDER	SIZE:	2 SET	ΓS 4#500	,1#0G, I	N 3" C (AL)
W14UZ	O.C. DI	EVICE:	MLO	(800A CI	B IN MAIN S	WBD)		MINIMU	M O.C. DE	VICE			
	MOUN	TING:	SURF.	ACE				INTERRU	UPTING RA	ATING	: 65,000	)	
	1	O.C.		K	VA	K	VA.	K	VA	Τ	O.C.		
Description	CKT	AMP	P		A	]	3		C	P	AMP	CKT	Description
	1				22.05							2	
SPARE BREAKER	3	225	3				22.05			3	200	4	PANEL M2L1 XFMR
	5								22.05			6	
	7											8	
SPARE BREAKER	9	225	3						1	3	100	10	SPARE BREAKER
	11	1	1									12	
	13											14	
SPACE	15	100	3							3	100	16	SPACE
	17											18	
	TOTAL	KVA/P	HASE	22	2.05	22	.05	22	2.05		TOTAL	KVA	66.15
			•							_	TOTAL	AMP	79.57
										TOT	AL PANI	EL KVA	409.72
										TOT	AL PANI	EL AMP	492.81
										DIVE	RSITY		0.85

DESIGNATION:	VOLTA	GE:	480/27	77V-3PH-47	W			LOCATIO	N: MAIN I	ELECT	RIC RO	ООМ	
	MAINS	:	600A					FED BY:		MDP	ı		
<b>N/I/III2</b>	TYPE:		MOT	ORS				FEEDER S	IZE:	2 SE	rs of 4	#300,1#	1G, IN 2.5" C (CU)
<b>M4U3</b>	O.C. DI	EVICE:	MLO	(600A CB	IN MAIN S	SWBD)		MINIMUM	O.C. DEV	ICE			
	MOUN	TING:	SURF	ACE				INTERRU	PTING RA	TING:	65,000		
		O.C.		1/3	VA	1/3	7 <b>A</b>	1/3	VA.	_	O.C.		<u> </u>
Description	CKT	AMP	P		VA. A		у <b>д</b> . З		va. C	P	AMP	CKT	Description
•				7.48	7.48							2	
PUMP P-1	3	50	3			7.48	7.48			3	50	4	PUMP P-2
								7.48	7.48			6	
	7				46.80							8	
	9	20	3				46.80			3	300	10	DOAS-13
	11								46.80			12	
	13			3.88	10.78							14	
KITCHEN AIR MAU-1	15	30	3			3.88	10.78			3	70	16	RTG-1
	17							3.88	10.78			18	
	19			7.90	10.78							20	
DOAS-11	21	40	3			7.90	10.78			3	70	22	RTG-1
	23							7.90	10.78			24	
	25			10.78	1.33			Ĭ				26	
RTG-1	27	70	3			10.78	1.33			3	20	28	EX. FAN EF-21
	29							10.78	1.33			30	
	31			1.33	1.33							32	
EX. FAN EF-20	33	20	3			1.33	1.33			3	20	34	EX. FAN EF-21
	35							1.33	1.33			36	
SPACE	37	20	1							1	20	38	SPACE
SPACE	39	20	1							1	20	40	SPACE
SPACE	41	20	1							1	20	42	SPACE
	TOTAL	KVA/PI	HASE	109	9.88	109	.88	109	9.88		TOTAL	KVA	329.63
										_	TOTAL	AMP	396.48

DESIGNATION:	VOLTA	GE:	480/27	77V-3PH-4	W			LOCATIO	ON: MAIN	ELEC	TRIC R	OOM	
	MAINS	:	600A					FED BY:		MDP			
T/I/II2	TYPE:		MOT	ORS				FEEDER S	SIZE:	2 SE	TS OF 4	#300,1#	1G, IN 2.5" C (CU)
M4U3	O.C. DI	VICE:	MLO	(600A CB	IN MAIN S	SWBD)		MINIMUM	I O.C. DE	VICE			
	MOUN	TING:	SURF	ACE				INTERRU	PTING R	ATING	: 65,000	)	
		O.C.	1 1	K	VA	K	VA	K	VA		O.C.		
Description	CKT	AMP	P		Ą	I	В		С	P	AMP	CKT	Description
	43				0.83					1	20	44	EX. FAN EF-12
	45	20	3				0.28					46	
	47								0.28	3	20	48	EX. FAN EF-27
	49			2.13	0.28							50	
PANEL M2U1	51	60	3			2.14	1.18					52	
	53							1.89		3	20	54	AIR COMPRESSOR
	55											56	
SPARE BREAKER	57	20	3							1	20	58	
	59									1	20	60	SPACE
	TOTAL	KVA/P	HASE	3.	24	3.	59	2.	16		TOTAL	KVA	9.00
											TOTAL	AMP	10.82
										TOT	AL PAN	EL KVA	338.62
													0.83
										TOT	AL PAN	EL AMP	407.30
										DIVE	RSITY		0.85

### Panel EQ4U1

DESIGNATION:	VOLTA	GE:	480/27	7V-3PH-4	W			LOCATIO	ON: MAIN	ELEC.	ROOM		
	MAINS	:	225A					FED BY:		MDP	•		
<b>EO4U1</b>	TYPE:			GENCY				FEEDER S	SIZE:	4#3	00,1#20	, IN 2.5	"C (AL)
LQ4U1			MLO	(225 AMP	BREAKE	R IN ED4U	1)		I O.C. DE				
	MOUN	TING:	SURF.	ACE				INTERRU	PTING RA	ATING	: 65,000	)	
		O.C.		K	VA	K	VA	K	VA	П	O.C.		1
Description	CKT	AMP	P	,	Ą		В		C	P	AMP	CKT	Description
	1			5.82								2	
WELL PUMP	3	40	3			5.82				3		4	
	5							5.82				6	
	7			0.28	3.33							8	
FUEL PUMP FOP-1	9	20	3			0.28	3.33			3	20	10	CU-7
	11							0.28	3.33			12	
	13				0.44							14	
	15		3				0.44			3	20	16	BC-2
	17								0.44			18	
	19			11.70	9.37							20	
BP-1	21	60	3			11.70	10.28			3	80	22	PANEL EQ2U3
	23							11.70	10.77			24	
	25									1	20	26	SPACE
SPARE BREAKER	27	20	3							1	20	28	SPACE
	29									1	20	30	SPACE
	TOTAL	KVA/PI	IASE	30	.94	31	.84	32	.33		TOTAL	KVA	95.11
										_	TOTAL	AMP	114.40
											DIVER	SITY	0.

### Main Switchboard

MAIN BUS	SIZE: 4000A	NEUTRAL		FULL	GROUND BUS:	FULL
MAIN DEV	ICE: "4000A MCB	MOUTING	:	SURFACE		
CIRCUIT		OVER	CURRENT	DEVICE		
NUMBER	LOADITEM	FRAME	TRIP	POLE	FEEDER SIZE	REMARKS
1	FIRE PUMP TAP			3	SEE RISER DIAGRAM	
2	M4U1	800	800	3	SEE PANEL SCHEDULE	
3	M4U2	800	800	3	SEE PANEL SCHEDULE	
4	M4U3	600	600	3	SEE PANEL SCHEDULE	
5	ED4U1	600	600	3	SEE PANEL SCHEDULE	
6	K4U1	600	600	3	SEE PANEL SCHEDULE	
7	L4U1/L4M1/L4L1	600	600	3	SEE PANEL SCHEDULE	
8	L4U2/L4M2/L4L2	600	400	3	SEE PANEL SCHEDULE	
9	L4U3	100	100	3	SEE PANEL SCHEDULE	
10	L4U4	100	100	3	SEE PANEL SCHEDULE	
11	EQ4U1	225	225	3	SEE PANEL SCHEDULE	
12	E4U1	225	125	3	SEE PANEL SCHEDULE	
13	R2U4 XFMER	100	60	3	SEE RISER DIAGRAM	
14	SPARE	400	400	3		
15	SPACE	600	600	3		
16	SPACE	400	400	3		