

- **Introduction**

- Mechanical Systems Overview
- Mechanical Depth
- Structural Breadth
- Acoustical Breadth
- Conclusions
- Recommendations
- Questions

Twin Rivers Elementary/Intermediate of
McKeesport Area School District



1600 Cornell St., McKeesport, Pa

Tessa Bauman
Mechanical Option

Technical Consultant: Laura Miller

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Building Statistics

Occupancy: Education

Size: 127,000 ft²

Number of Stories: 2

Completion Date: February 2014

Project Cost: \$29 million

Project Team

Owner: McKeesport Area School District

Architect: J C Pierce

Construction Manager: PJ Dick

General Contractor: Gurtner Construction

Civil Engineers: Phillips & Associates, Inc.

Structural & MEP Engineers: Loftus Engineers

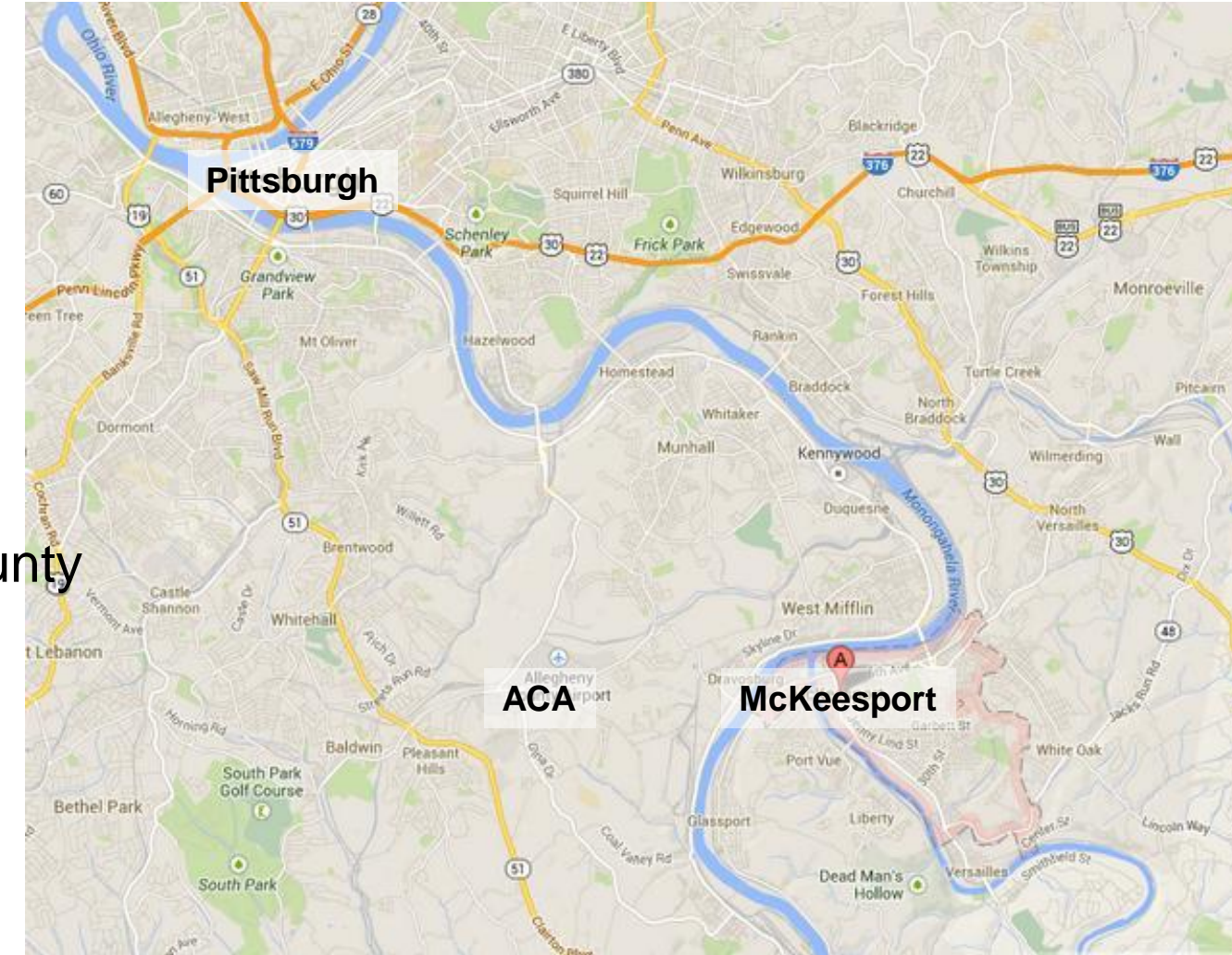
Environmental Engineers: American Geosciences, Inc.

• Introduction

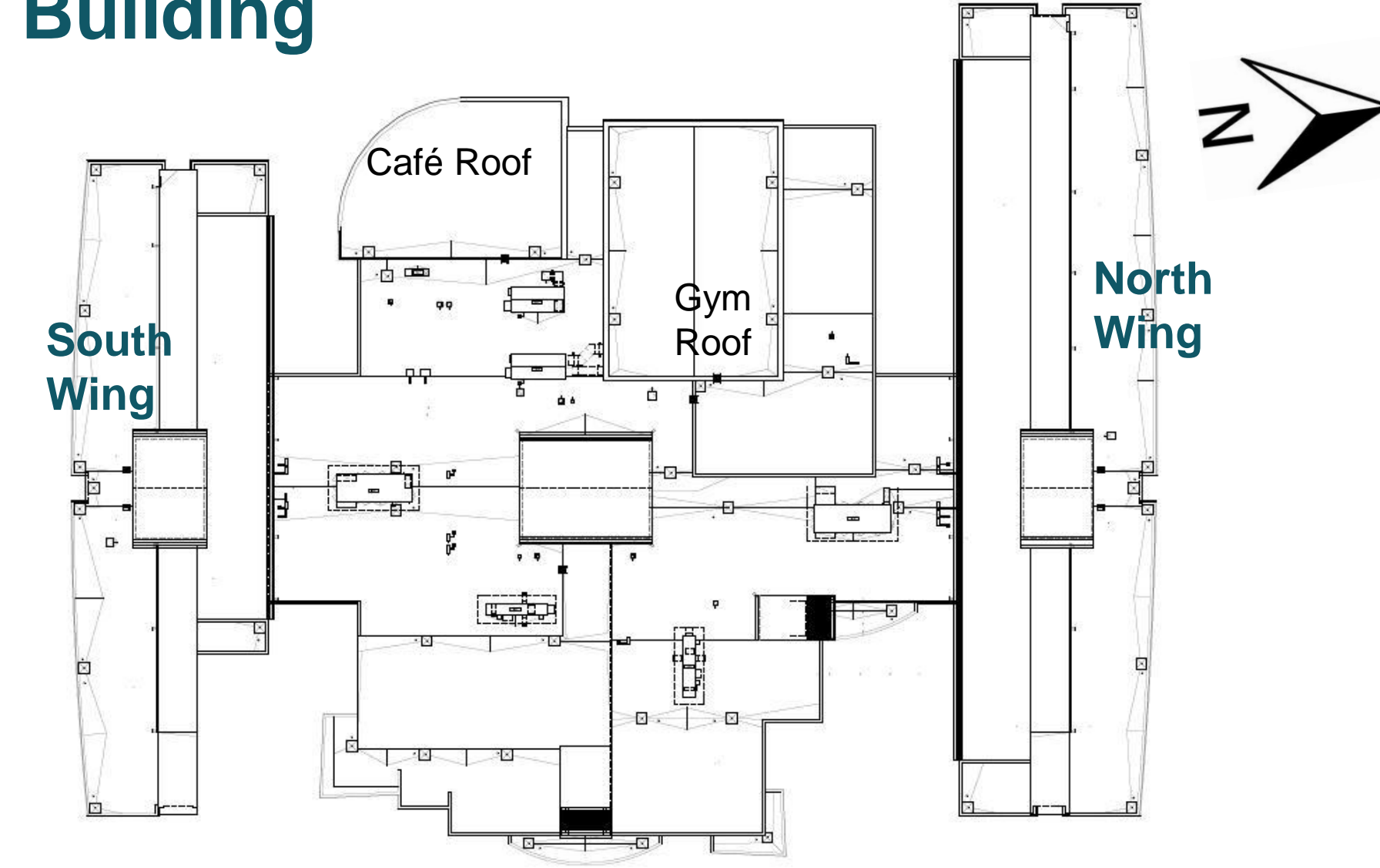
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Location

- 20 miles SE of Pittsburgh, Pa
- 5 miles east of Allegheny County Airport



Building



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Design Goals

- Tracking LEED Gold Accreditation
 - Mechanical designed with ASHRAE Advanced Energy Design Guide for K-12 School Buildings
- Education Aspects of Sustainable Design
 - LCD screens describing systems
 - Curtain wall system around Mechanical and Electrical Room

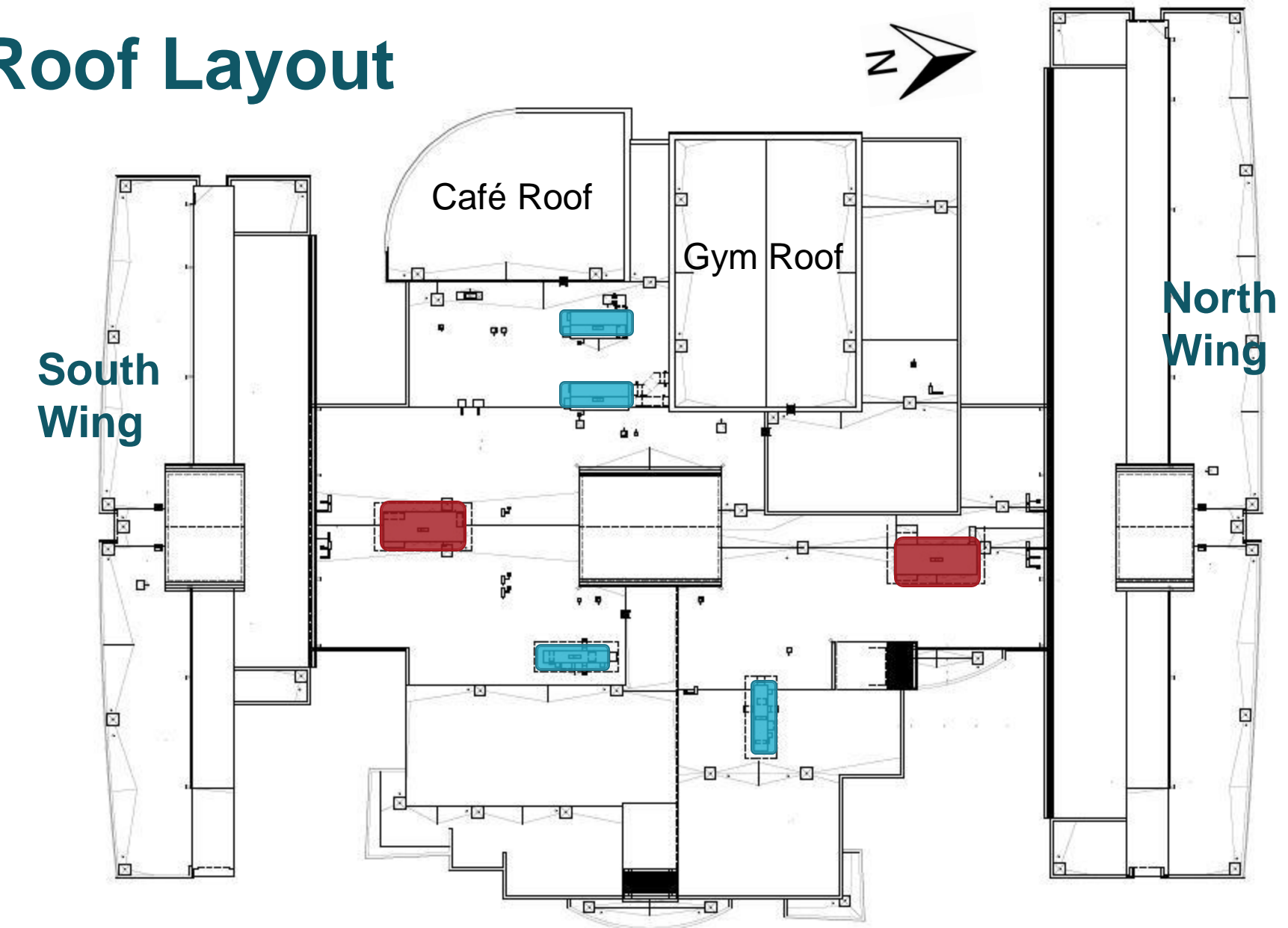


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Ventilation

- 2 DOAS
 - Heat Recovery Wheel
 - Desiccant Wheel
- 4 AHUs
 - Single Zone VAV
 - Multi Zone VAV with reheat
- Partial Occupancy

Roof Layout

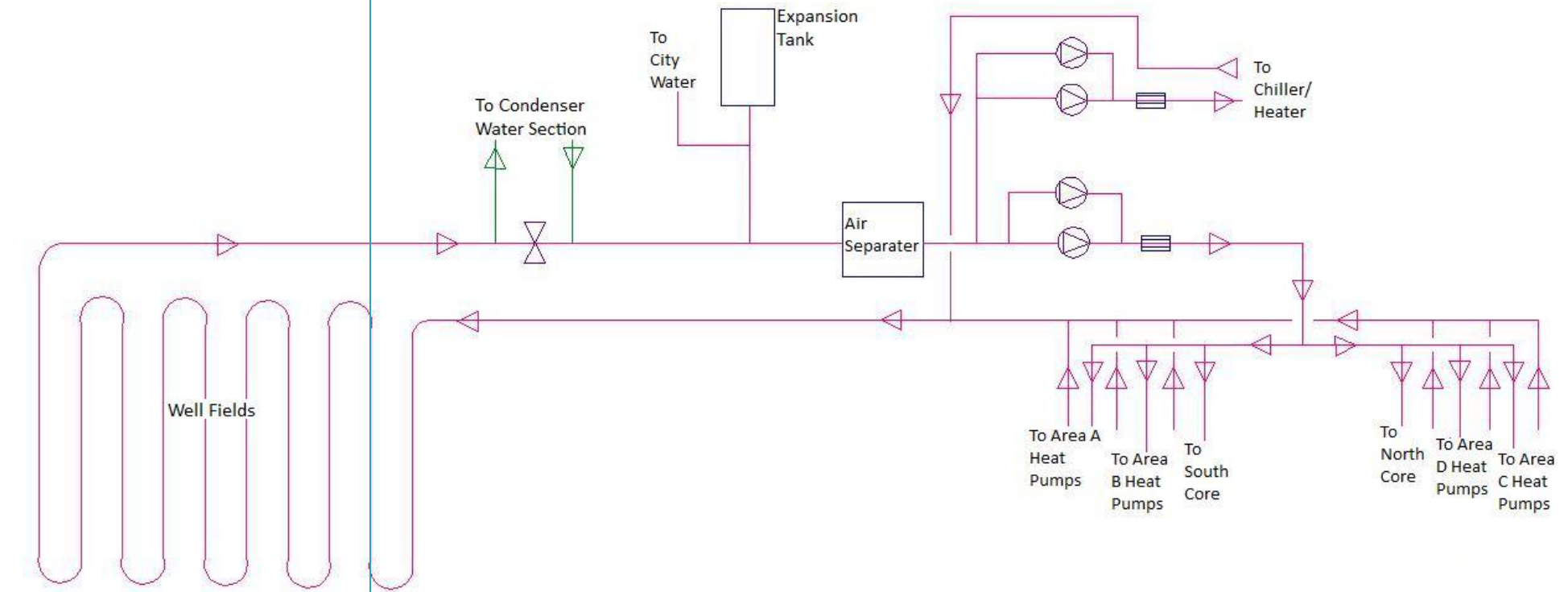


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Heating and Cooling

- Geothermal Heat Pumps
 - Closed looped earth coupled vertical water loop
 - 60°F water
 - Chiller supply
 - Water to Air HPs located in classroom cabinets
 - Auxiliary heating and cooling
- VAV Reheat to Library and Offices

Schematic



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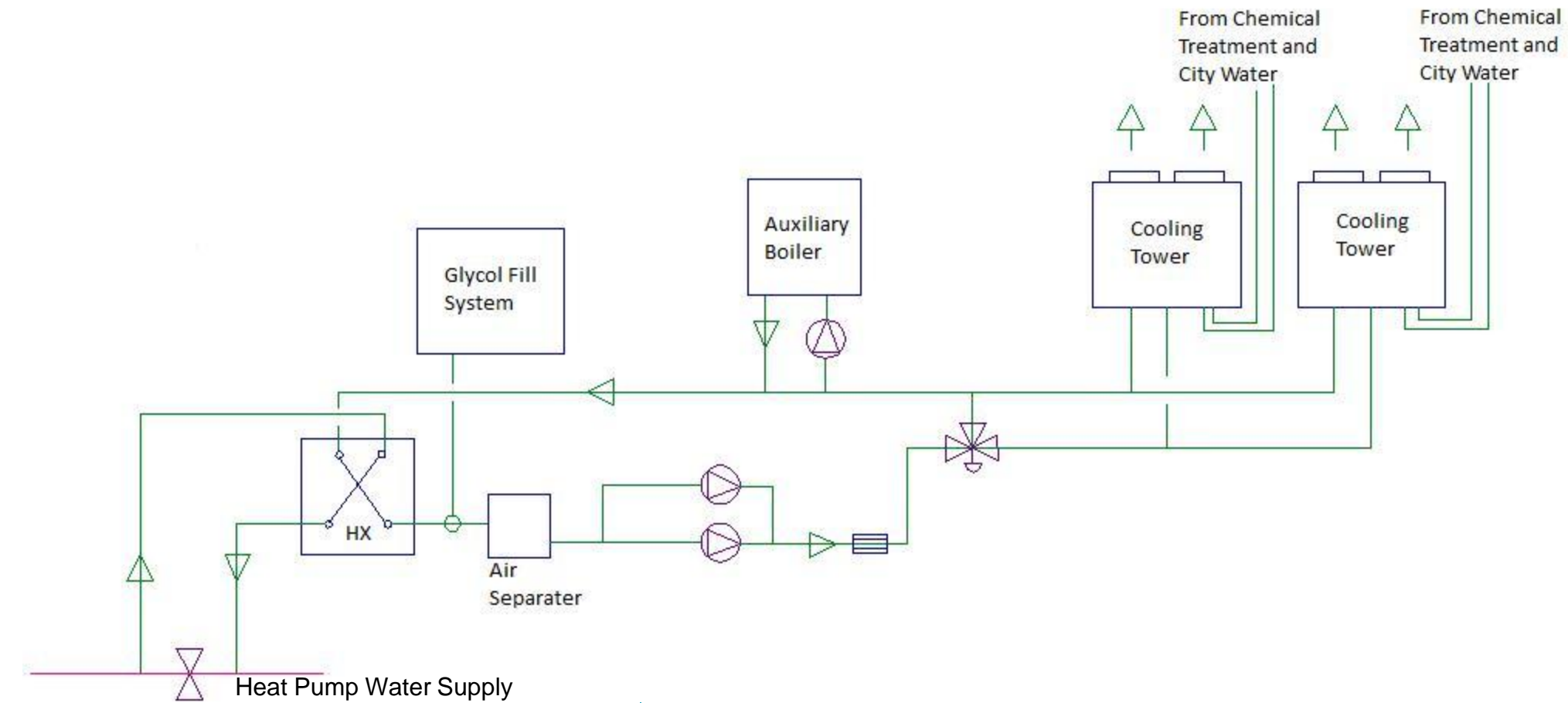
Condenser Water Loop

- 30% polyethylene glycol solution
- Heat Exchanger
- Cooling Towers
- Auxiliary Boiler

Domestic Hot Water

- Two 125 Gallon Water Heaters
- Supply at 140°F

Schematic

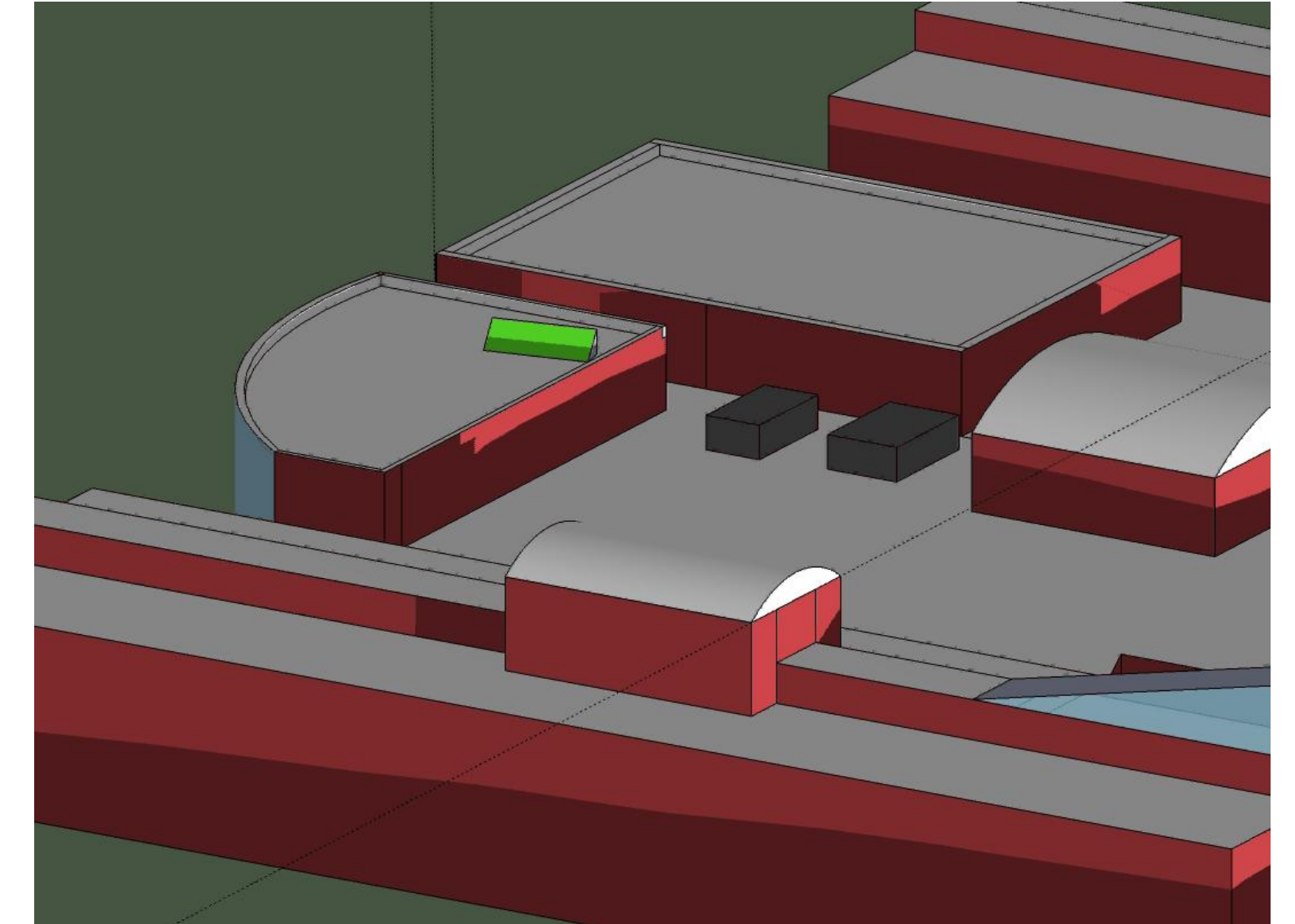


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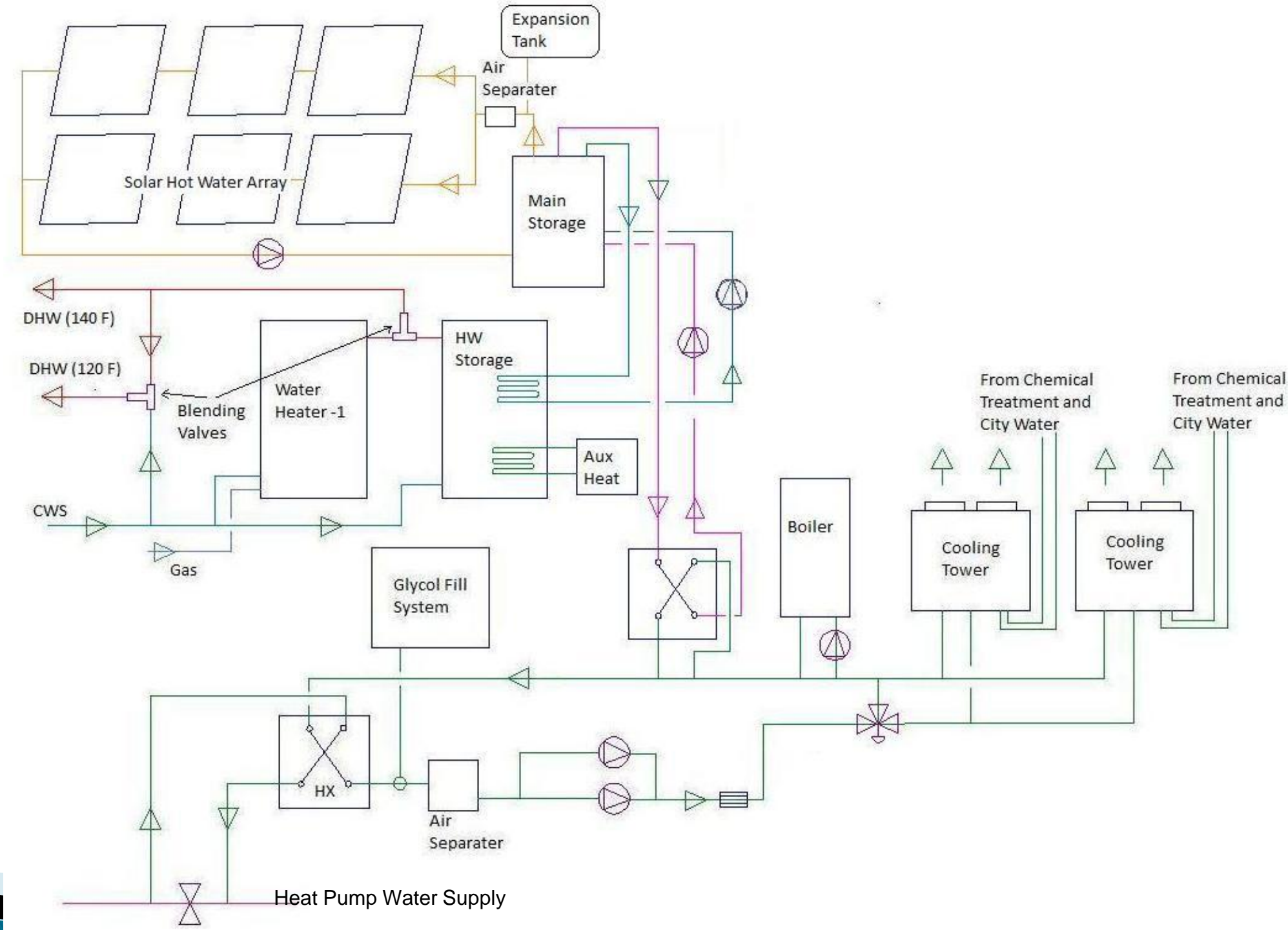
Solar Thermal Auxiliary

- Goals:
 - Reduce dependency on natural gas
 - Increase sustainability
 - “If cost is no issue” possibility
- Boiler and Water Heater Reduced Loads
- Solar Thermal Array

Shading Analysis



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Solar Thermal Auxiliary

Main Components

- FPC Array
- Main Storage Tank
- Solar Hot Water Tank
- GA Heat Exchanger

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Hourly Solar Calculations

$$\delta = 23.45^\circ \sin \left(\frac{360}{365} (284 + n) \right)$$

$$\cos \theta = \sin(\phi - \beta) \sin \delta + \cos(\phi - \beta) \cos \delta \cos \omega$$

$$G_T = DNI \cos \theta + DHI \left(\frac{1 + \cos \beta}{2} \right) + \rho_g GHI \left(\frac{1 - \cos \beta}{2} \right)$$

Array Calculations

$$Q_u = A_c (F_r \tau \alpha G_T - F_r U_L (T_i - T_a))$$

$$T_o = \frac{Q_u}{m_{\text{dot}} c_p} + T_i$$

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System Calculations

$$T'_s = T_s + \left(\frac{1}{c_p V_{tank}} \right) (Q_u - L_{tank} - L_{DHW} - L_{GA})$$

$$L_{tank} = UA(T_s - T_{a,mech})$$

$$L_{DHW} = \epsilon_{HX} m_{DHW} c_p (T_s - T_{r,DHW})$$

$$L_{GA} = \epsilon_{HX} m_{GA} c_p (T_s - T_{r,GA})$$

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System Calculations

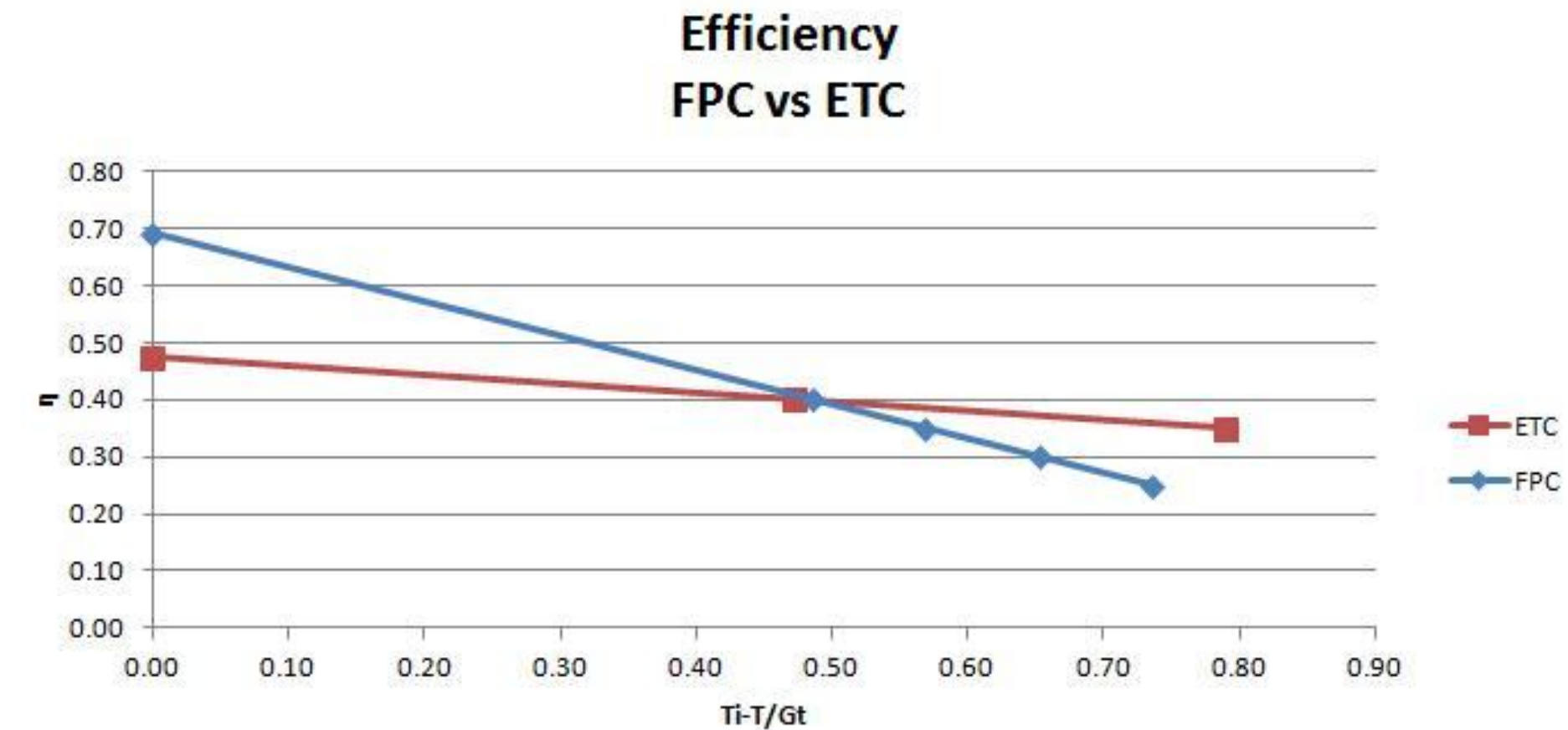
6/21		m,dhw (gph) 2100		m, ga (gph) 2100								
Start Time	End Time	Qu,array (MBH)	tank Loss (MBH)	DHW load (MBH)	GA load (MBH)	Ts (F)	Tr,dhw (F)	Tr,ga (F)	Tr (F)	Aux needed, DHW (MBH)	Aux needed, GA (MBH)	Solar Fraction
5:00 AM	6:00 AM	0	0.48195161	0	0	149.9374	119.9374	79.93741	114.93741	252.57232	427.5856925	0
6:00 AM	7:00 AM	0	0.48157453	0	0	149.8749	119.8749	79.87486	114.87486	252.57232	427.5856925	0
7:00 AM	8:00 AM	287.8563	0.48119774	335.4336	782.67841	41.98442	22.48442	-3.51558	9.4844189	-82.86128361	-355.092716	1.643900375
8:00 AM	9:00 AM	481.5536	-0.1687769	218.0318	508.74097	10.15893	-2.51607	-19.4161	-10.96607	34.54047765	-81.155273	1.068535244
9:00 AM	10:00 AM	601.894	-0.3605062	141.7207	330.68163	27.02325	18.7845	7.799501	13.292001	110.8516225	96.90406495	0.694547909
10:00 AM	11:00 AM	612	-0.2589089	92.11845	214.94306	66.6602	61.30501	54.16476	57.73489	160.4538666	212.6426346	0.451456141
11:00 AM	12:00 PM	581.6336	-0.0201203	59.87699	139.71299	116.28	112.7992	108.158	110.47859	192.6953253	287.8727049	0.293446491
12:00 PM	1:00 PM	487.2437	0.27880925	38.92005	90.813442	162.6748	160.4122	157.3955	158.90387	213.6522734	336.7722505	0.190740219
1:00 PM	2:00 PM	387.1472	0.5583097	25.29803	59.028737	201.9306	200.4599	198.499	199.47944	227.2742897	368.5569552	0.123981143
2:00 PM	3:00 PM	323.4228	0.79480181	16.44372	38.368679	236.7126	194.0441	192.7695	193.40678	236.1286003	389.2170133	0.080587743
3:00 PM	4:00 PM	272.1585	1.00434274	477.0823	491.33354	146.157	118.4225	117.594	118.00823	-224.5099953	-63.7478465	1.423810109
4:00 PM	5:00 PM	226.956	0.45880006	310.1035	319.3668	93.82163	75.79416	75.25565	75.524906	-57.53118493	108.2188922	0.925476571
5:00 PM	6:00 PM	154.6463	0.1435109	201.5673	207.58842	60.74904	49.03119	48.68116	48.856175	51.0050418	219.9972723	0.601559771
6:00 PM	7:00 PM	109.2878	-0.0557314	131.0187	134.93247	40.40991	32.79331	32.56579	32.679547	121.5535892	292.6532194	0.391013851
7:00 PM	8:00 PM	73.21783	-0.1782624	85.16218	0	38.88181	33.93102	-6.06898	33.931021	167.410145	427.5856925	0.125209398
Average:										110.3871605	206.3730833	0.534284331

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ETC VS FPC

ETC				
Date	Total $Q_{u,avg}$ (MBH)	Axillary For DHW (MBH)	Axillary for GA (MBH)	Solar Fraction
12/21	35.27	218.83	427.59	5%
3/20	237.68	185.04	296.14	29%
6/21	225.06	203.56	328.31	22%
9/23	257.93	190.69	308.40	27%
11/30	45.52	204.45	402.34	11%
1/12	141.05	194.71	278.87	30%
Hourly Average:	157.09	199.55	340.28	21%

FPC				
Date	Total $Q_{u,avg}$ (MBH)	Axillary For DHW (MBH)	Axillary for GA (MBH)	Solar Fraction
12/21	2.13	252.57	427.59	0%
3/20	418.05	197.34	221.40	38%
6/21	353.77	110.39	206.37	53%
9/23	453.75	171.00	240.63	39%
11/30	93.65	208.30	394.04	11%
1/12	419.23	182.59	252.63	36%
Hourly Average:	290.10	187.03	290.44	30%



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Cost Analysis

Cost of System: \$371,450

Fuel Savings at Solar Fraction of 0.3: \$3,386

Life Cycle Cost Analysis

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Cost Analysis

Year	Extra mortgage payment (\$) : fixed	Fuel savings (\$) : projected to increase by 1.03 each year	Extra insurance, maintenance, and parasitic cost (\$) : projected to increase by 1.01 each year	Annual Solar savings (\$)	PW of annual solar savings (\$) : must use PW for each year	Cumulative Solar Savings (\$)	Yearly Interest Payment (\$) : need to multiply balance by 1.0575	Principle Payment	Principle Balance (total system cost, less 20% Down Payment)	Periodic Payment Present Worth Factor (15, 0, 0.0575)	Present Worth for Savings (n, 0, d) : must use $1/(1+d)^n$
0		\$3,686.60		-\$74,290.00	-\$74,290.00	\$0.00		\$297,160.00	\$297,160.00	9.87288553	1.0000
1	-\$30,098.60	\$3,797.19	-\$3,714.50	-\$30,015.90	-\$28,316.89	-\$102,606.89	\$0.00	-\$30,098.60	\$267,061.40		0.9434
2	-\$30,098.60	\$3,911.11	-\$3,751.65	-\$29,939.13	-\$26,645.72	-\$129,252.61	\$15,356.03	-\$14,742.57	\$252,318.84		0.8900
3	-\$30,098.60	\$4,028.44	-\$3,789.16	-\$29,859.31	-\$25,070.46	-\$154,323.07	\$14,508.33	-\$15,590.26	\$236,728.57		0.8396
4	-\$30,098.60	\$4,149.30	-\$3,827.05	-\$29,776.35	-\$23,585.66	-\$177,908.73	\$13,611.89	-\$16,486.70	\$220,241.87		0.7921
5	-\$30,098.60	\$4,273.78	-\$3,865.32	-\$29,690.14	-\$22,186.20	-\$200,094.93	\$12,663.91	-\$17,434.69	\$202,807.18		0.7473
6	-\$30,098.60	\$4,401.99	-\$3,903.98	-\$29,600.58	-\$20,867.24	-\$220,962.17	\$11,661.41	-\$18,437.18	\$184,370.00		0.7050
7	-\$30,098.60	\$4,534.05	-\$3,943.02	-\$29,507.56	-\$19,624.22	-\$240,586.39	\$10,601.27	-\$19,497.32	\$164,872.68		0.6651
8	-\$30,098.60	\$4,670.07	-\$3,982.45	-\$29,410.97	-\$18,452.81	-\$259,039.20	\$9,480.18	-\$20,618.42	\$144,254.26		0.6274
9	-\$30,098.60	\$4,810.17	-\$4,022.27	-\$29,310.70	-\$17,348.96	-\$276,388.15	\$8,294.62	-\$21,803.98	\$122,450.28		0.5919
10	-\$30,098.60	\$4,954.48	-\$4,062.49	-\$29,206.61	-\$16,308.82	-\$292,696.97	\$7,040.89	-\$23,057.71	\$99,392.57		0.5584
11	-\$30,098.60	\$5,103.11	-\$4,103.12	-\$29,098.60	-\$15,328.78	-\$308,025.75	\$5,715.07	-\$24,383.52	\$75,009.05		0.5268
12	-\$30,098.60	\$5,256.21	-\$4,144.15	-\$28,986.54	-\$14,405.42	-\$322,431.18	\$4,313.02	-\$25,785.58	\$49,223.47		0.4970
13	-\$30,098.60	\$5,413.89	-\$4,185.59	-\$28,870.30	-\$13,535.52	-\$335,966.70	\$2,830.35	-\$27,268.25	\$21,955.23		0.4688
14	-\$30,098.60	\$5,576.31	-\$4,227.45	-\$28,749.74	-\$12,716.04	-\$348,682.73	\$1,262.43	-\$28,836.17	-\$6,880.94		0.4423
15	-\$30,098.60	\$5,743.60	-\$4,269.72	-\$28,624.72	-\$11,944.10	-\$360,626.83	-\$395.65	-\$30,494.25	-\$37,375.19		0.4173
15				Totals:	\$2,002.87	-\$358,623.96	-\$2,149.0737				

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Array Effect on Structural Roof



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Array Effect on Structural Roof

$$w_{LL} = (1.2D + 1.6S + L_r)(joist\ spacing) + 1.2(joist\ weight)$$

$$w_{TL} = 1.2(D + S(or\ L_r))(joist\ spacing) + (joist\ weight)$$

where

- D = Dead Load
- S = Snow Load
- L_r = Roof Live Load

LRFD

STANDARD LOAD TABLE FOR LONGSPAN STEEL JOISTS, LH-SERIES
Based on a 50 ksi Maximum Yield Strength - Loads Shown In Pounds Per Linear Foot (plf)

Joist Designation	Approx. Wt in Lbs. Per Linear Ft. (Joists only)	Depth in inches	Max Load (plf)	SAFELOAD* in Lbs. Between		SPAN IN FEET																		
				< 39	39-46	47-49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64			
				32LH06	14	32	647	25230	25230	507	489	472	456	441	426	412	399	385	373	363	351	340	330	321
32LH07	16	32	728	28380	28380	568	549	529	511	493	477	462	447	432	418	406	393	381	370	360				
32LH08	17	32	790	30810	30810	616	595	574	553	535	517	499	483	468	453	439	426	412	400	388				
32LH09	21	32	992	38670	38670	774	747	720	694	670	648	627	606	586	568	550	534	517	502	487				
32LH10	21	32	1096	42750	42750	856	825	796	768	742	717	693	667	645	624	603	583	564	546	529				
32LH11	24	32	1201	46830	46830	937	903	870	840	811	783	757	732	709	687	664	643	624	604	585				
32LH12	27	32	1409	54960	54960	1101	1068	1032	996	961	928	897	867	838	811	786	762	738	715	694				
32LH13	30	32	1572	61320	61320	1225	1201	1177	1156	1133	1072	1035	999	964	931	900	871	843	816	790				
32LH14	33	32	1618	63120	63120	1264	1239	1215	1192	1170	1149	1107	1069	1032	997	964	933	903	874	846				
32LH15	35	32	1673	65250	65250	1305	1279	1255	1231	1207	1186	1164	1144	1125	1087	1051	1017	984	952	924				
				< 43	43-46	47-56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72		
36LH07	16	36	590	25350	25350	438	424	411	399	387	376	366	355	345	336	327	318	310	301	294				
36LH08	18	36	649	27900	27900	481	466	453	439	426	414	402	390	379	369	358	349	340	331	322				
36LH09	21	36	832	35760	35760	616	597	579	561	544	528	513	499	484	471	459	445	433	423	412				
36LH10	21	36	916	39390	39390	681	660	639	619	601	583	567	550	535	520	507	492	480	466	454				
36LH11	23	36	1000	42990	42990	742	720	697	676	657	637	618	601	583	567	552	537	522	508	495				
36LH12	25	36	1197	51450	51450	889	862	835	810	784	762	739	717	696	675	655	636	618	600	583				

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Redesign of Mechanical Room Walls



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Redesign of Mechanical Room Walls

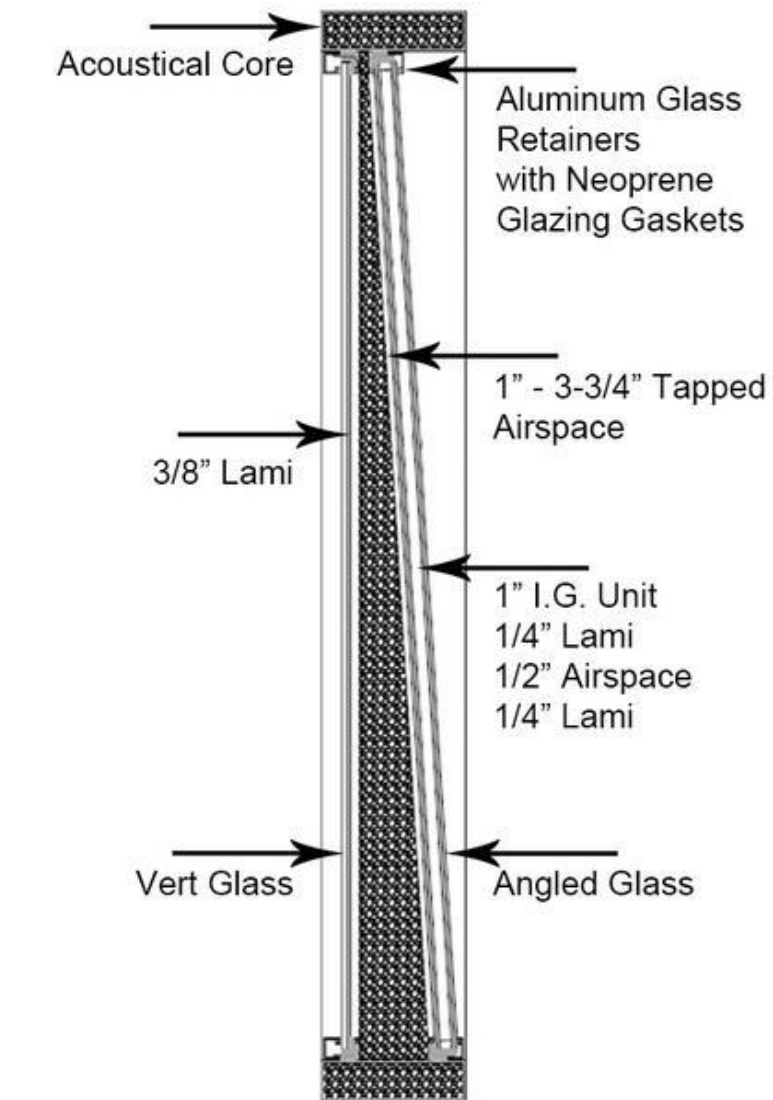
Table B.1 — Minimum STC ratings recommended between an ancillary space and an adjacent space

Receiving ancillary learning space	Adjacent space			
	Corridor or staircase ^{a)} , common-use, and public-use toilet and bathing room ^{b)}	Music room	Office or conference room ^{a)}	Mechanical equipment room ^{f)} , cafeteria, gymnasium, or indoor swimming pool
Corridor used as ancillary learning space	45	60 ^{c)}	45 ^{d)}	55 ^{c)}
Music room	45	60	60 ^{e)}	60
Office or conference room	45 ^{d)}	60 ^{g)}	45 ^{d)}	60

c) When the corridor will not be used as an ancillary learning space, the minimum STC rating may be reduced to not less than 45. Use of corridors as ancillary learning spaces should be avoided when they are located next to the noisy spaces indicated in the table by the high STC ratings.

Current STC of Glass Window: STC-30

Proposed Redesign



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Conclusions

- As Solar hot Water System is possible and economical
- Costly ramifications for structure
- Acoustical Treatment is necessary for the mechanical display windows

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Recommendations

- Generate More Accurate Model
- Do not proceed with solar hot water system

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Questions?

Special Thanks To:
David Nitchkey
Harry Bauman
David Winklebleck