

500 Delaware Ave.

# APPENDICES

500 Delaware Ave.

## APPENDICES

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## APPENDIX A: LOAD CALCULATIONS

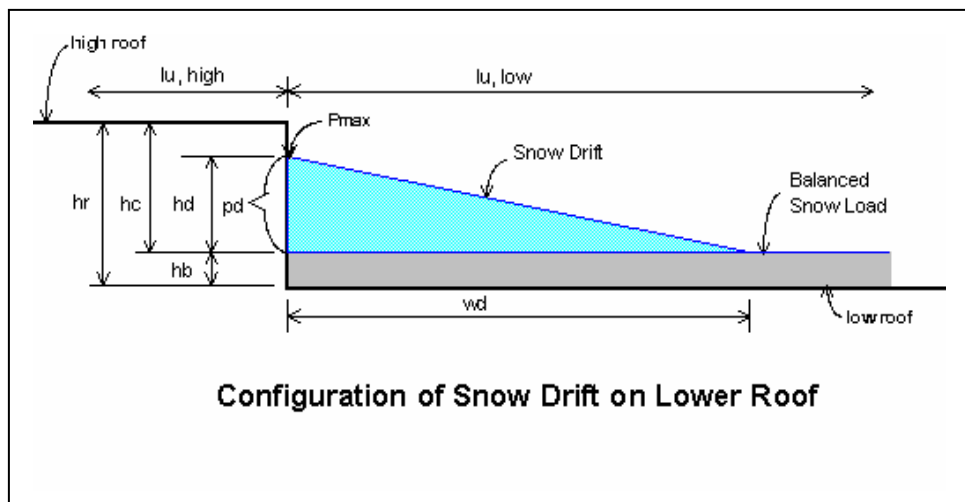
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**A.I Snow Loading**

<i>Design Parameters</i>		
$P_g$	25.00 psf	Ground Snow Load - Figure 1608.2
	Above Tree Line	Terrain Category - Section 1609.4
	Fully Exposed	Roof Exposure - Table 1608.3.1b
$C_e$	0.8	Exposure Factor - Table 1608.3.1
$C_t$	1.00	Thermal Factor - Section 1608.3.2
	I	Importance Category - Table 1604.5
$I$	1.0	Importance Factor - Table 1609.5
$P_f$	20.00 psf	Flat Roof Snow Load, $P_f = 0.7 * C_e * C_t * I_s * P_g$ - Section 1608.3
$D$	17 pcf	Snow density, $D = 0.13P_g + 14 \leq 30$ pcf - 1608.7
$h_b$	1'	Height of minimum roof snow load, (Default, $P_f/D$ ) - 1608.7
$h_r$	19'	Difference in height between upper and lower roofs
$h_c$	17'	Difference in height between upper roof and top of flat roof snow
$l_{u, high}$	36'	Horizontal dimension of upper roof normal to the line of change of roof level
$l_{u, low}$	48'	Horizontal dimension of lower roof normal to the line of change of roof level

<i>Drift Calculations</i>					
Drift location	Calc. $h_d$ (ft)	Corrected $h_d$ (ft)	$P_d$ (psf)	$P_{max}$ (psf)	$W_d$
Windward Drift	1.73	1.73	29.77	49.77	6.90
Leeward Drift	1.95	1.95	33.70	53.70	7.81
<b>Design Drift</b>	<b>1.95</b>	<b>1.95</b>	<b>33.7</b>	<b>53.7</b>	<b>7.8</b>

X	Y	A1 (psf)	A2 (psf)	Total (psf)
2.0	45	45	4	49
4.0	36	36	4	41
6.0	28	28	4	32
7.8	20	20	4	24



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**Design Parameters**

$P_g$	25.00 psf	Ground Snow Load - Figure 1608.2
	Above Tree Line	Terrain Category - Section 1609.4
	Fully Exposed	Roof Exposure - Table 1608.3.1b
$C_e$	0.7	Exposure Factor - Table 1608.3.1
$C_t$	1.00	Thermal Factor - Section 1608.3.2
	I	Importance Category - Table 1604.5
$I$	1.0	Importance Factor - Table 1609.5
$P_f$	20.00 psf	Flat Roof Snow Load, $P_f = 0.7 * C_e * C_t * I_s * P_g$ - Section 1608.3
$D$	17.25 pcf	Snow density, $D = 0.13P_g + 14 \leq 30$ pcf - 1608.7
$h_b$	1.16'	Height of minimum roof snow load, (Default, $P_f/D$ ) - 1608.7
$h_r$	18.5'	Difference in height between upper and lower roofs
$h_c$	17.3'	Difference in height between upper roof and top of flat roof snow
$l_{u, high}$	44'	Horizontal dimension of upper roof normal to the line of change of roof level
$l_{u, low}$	130'	Horizontal dimension of lower roof normal to the line of change of roof level

**Drift Calculations**

Drift location	Calc. $h_d$ (ft)	Corrected $h_d$ (ft)	$P_d$ (psf)	$P_{max}$ (psf)	$W_d$
Windward Drift	2.85	2.85	49.14	69.14	11.39
Leeward Drift	2.19	2.19	37.82	57.82	8.77
<b>Design Drift</b>	<b>2.85</b>	<b>2.85</b>	<b>49.1</b>	<b>69.1</b>	<b>11.4</b>

X	Y	A1 (psf)	A2 (psf)	Total (psf)
2.0	61	61	4	65
4.0	52	52	4	56
6.0	43	43	4	48
8.0	35	35	4	39
10.0	26	26	4	30
11.4	20	20	3	23

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A.2 Lateral Loading

A.2.I Wind

**Input Information**

	L: Length of Building in X- Direction	B: Length of Building in Y - Direction	L/B	B/L	Story Heights (ft)	Building Story Height (ft)
						210.50 ft
R	270.00 ft	88.00 ft	3.07	0.33	14.50 ft	210.50 ft
15	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	196.00 ft
14	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	182.50 ft
13	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	169.00 ft
12	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	155.50 ft
11	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	142.00 ft
10	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	128.50 ft
9	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	115.00 ft
8	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	101.50 ft
7	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	88.00 ft
6	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	74.50 ft
5	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	61.00 ft
4	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	47.50 ft
3	270.00 ft	88.00 ft	3.07	0.33	13.50 ft	34.00 ft
2	270.00 ft	88.00 ft	3.07	0.33	10.25 ft	20.50 ft
Int.	270.00 ft	88.00 ft	3.07	0.33	10.25 ft	10.25 ft

210.50 ft

h	210.50 ft	Mean Roof Height of Building
H	210.50 ft	Total Height of Roof
Ct	0.030	Fundamental Period Coefficient, ASCE 7-02 Table 9.5.5.3.2
x	0.750	Fundamental Period Factor, ASCE 7-02 Table 9.5.5.3.2
Ta	0.60 Hz	Structure is flexible so G will be calculated per ASCE Section 6.5.8.2
⊙	0.0 deg	Angle of Roof Slope
V	90 mph	
I	1.00	
Exposure	B	
Roof Diaphragm	2	Is roof diaphragm considered rigid or flexible??

**Calculated Information**

Height	HIGH	"High" for Buildings >60', "Low" for Buildings < 60'
Cp-w	0.8	Windward Wall Pressure Coefficient, ASCE 7-02 Figure 6-6
Cp-S	-0.7	Side Wall Pressure Coefficient, ASCE 7-02 Figure 6-6
Kd	0.85	Wind Directionality Factor, ASCE 7-02 Table 6-4
Gcpi	0.18	Internal Pressure Coefficients for Enclosed Buildings, ASCE 7-02 Figure 6-5

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Criteria	Reference/Description		
h	210.5	height of building	
zmin	30	RIGID: From Table 6-2 of ASCE 7-02	
zbar	126.3	RIGID: $0.6 * h > zmin$ : ASCE 7-02 Section 6.5.8.1	
c	0.3	RIGID: From Table 6-2 of ASCE	
g <sub>a</sub>	3.4	per section 6.5.8.1 and 6.5.8.2 of ASCE 7-02	
g <sub>v</sub>	3.4	per section 6.5.8.1 and 6.5.8.2 of ASCE 7-02	
l	320	RIGID: Table 6-2 of ASCE 7-02	
e	0.33	RIGID: Table 6-2 of ASCE 7-02	
n <sub>1</sub> , Y-dir	0.561	Natural Period	
n <sub>1</sub> , X-dir	0.81	Natural Period	
b	0.05	Damping Factor	
V	90	Basic Wind Speed	
bbar	0.45	FLEXIBLE: Table 6-2 ASCE 7-02	
abar	0.25	FLEXIBLE: Table 6-2 ASCE 7-02	
L <sub>1</sub>	0.2398684	Equation 6-5 ASCE 7-02	
L <sub>2</sub>	500.52643	Equation 6-7 ASCE 7-02	
	Y - Direction	X - Direction	
g <sub>r</sub>	4.0493434	4.1389373	FLEXIBLE: Equation 6-9
V <sub>s</sub>	75.529414	75.529414	FLEXIBLE: Equation 6-14
h <sub>n</sub>	10.384339	10.384339	FLEXIBLE: Section 6.5.8.2
R <sub>n</sub>	0.0916621	0.0916621	FLEXIBLE: Section 6.5.8.2
N <sub>1</sub>	5.367795	5.367795	FLEXIBLE: Equation 6-12
R <sub>n</sub>	0.0485013	0.0485013	FLEXIBLE: Equation 6-11

Stiff Building Calculations						Flexible Building Calculations					
Level	Height	B	L	Q	G stiff X-dir	nl	nb	Rl	Rb	R	G flex X-dir
Int.	10.25	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
3	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
4	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
5	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
6	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
7	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
8	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
9	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
10	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
11	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
12	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
13	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
14	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
15	13.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
R	14.5	88	270	0.829	0.833	44.592	4.341	0.0222	0.204	0.099	0.838
0	0	0	0	0.856	0.848	0.000	0.000	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

Stiff Building Calculations						Flexible Building Calculations					
Level	Height	B	L	G stiff Y-dir		nl	nb	Rl	Rb	R	G flex Y-dir
Int.	10.25	270	88	0.787	0.811	10.066	9.225	0.0944	0.103	0.072	0.813
3	13.5	270	88	0.787	0.811	10.066	9.225	0.0944	0.103	0.072	0.813
4	13.5	270	88	0.787	0.811	10.066	9.225	0.0944	0.103	0.072	0.813
5	13.5	270	88	0.787	0.811	10.066	9.225	0.0944	0.103	0.072	0.813
6	13.5	270	88	0.787	0.811	10.066	9.225	0.0944	0.103	0.072	0.813
7	13.5	270	88	0.787	0.811	10.066	9.225	0.0944	0.103	0.072	0.813
8	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
9	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
10	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
11	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
12	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
13	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
14	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
15	13.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
R	14.5	270	88	0.787	0.811	14.534	13.320	0.0664	0.072	0.060	0.812
0	0	0	0	0.856	0.848	0.000	0.000	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

**Summary**

h	G flex Y-dir		G flex X-dir		height	part to short	part to long
10	0	1	0.813	0.838	1	0	0.813 0.838
24	20	3	0.813	0.838	2	15	0.813 0.838
37.3	30	5	0.813	0.838	3	20	0.813 0.838
50.8	50	7	0.813	0.838	4	25	0.813 0.838
64	60	8	0.813	0.838	5	30	0.813 0.838
78	70	9	0.813	0.838	6	40	0.813 0.838
91	90	11	0.812	0.838	7	50	0.813 0.838
105	100	12	0.812	0.838	8	60	0.813 0.838
118	110	13	0.812	0.838	9	70	0.813 0.838
132	130	15	0.812	0.838	10	80	0.813 0.838
145	140	16	0.812	0.838	11	90	0.812 0.838
159	150	17	0.812	0.838	12	100	0.812 0.838
172	170	19	0.812	0.838	13	110	0.812 0.838
172	170	19	#DIV/0!	#DIV/0!	14	120	0.812 0.838



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**Design Wind Pressures on Main-Wind-Resisting-Systems**

ASCE Section 6.5

Height above ground level, z	Kz	G X-Dir	G Y-Dir	L/B	B/L	Cp Leeward X-Dir	Cp Leeward Y-Dir	Velocity Pressure, qz	Velocity Pressure, qh	Design Windward Wall Pressure in X-Dir	Design Windward Wall Pressure in Y-Dir	Design Leeward Wall Pressure in X-Dir	Design Leeward Wall Pressure in Y-Dir	Total Pressure for MWFRS in X-Dir	Total Pressure for MWFRS in Y-Dir	Building Floor Elevation
0 ft	0.575	0.8378	0.8131	3.07	0.33	-0.248	-0.500	10.1 psf	21.2 psf	6.8 psf	6.6 psf	-4.4 psf	-8.6 psf	11.2 psf	15.2 psf	10.25 ft
15 ft	0.575	0.8378	0.8131	3.07	0.33	-0.248	-0.500	10.1 psf	21.2 psf	6.8 psf	6.6 psf	-4.4 psf	-8.6 psf	11.2 psf	15.2 psf	20.50 ft
20 ft	0.624	0.8378	0.8131	3.07	0.33	-0.248	-0.500	11.0 psf	21.2 psf	7.4 psf	7.2 psf	-4.4 psf	-8.6 psf	11.8 psf	15.8 psf	34.00 ft
25 ft	0.665	0.8378	0.8131	3.07	0.33	-0.248	-0.500	11.7 psf	21.2 psf	7.9 psf	7.6 psf	-4.4 psf	-8.6 psf	12.3 psf	16.3 psf	47.50 ft
30 ft	0.701	0.8378	0.8131	3.07	0.33	-0.248	-0.500	12.3 psf	21.2 psf	8.3 psf	8.0 psf	-4.4 psf	-8.6 psf	12.7 psf	16.7 psf	61.00 ft
40 ft	0.761	0.8378	0.8131	3.07	0.33	-0.248	-0.500	13.4 psf	21.2 psf	9.0 psf	8.7 psf	-4.4 psf	-8.6 psf	13.4 psf	17.4 psf	74.50 ft
50 ft	0.811	0.8378	0.8131	3.07	0.33	-0.248	-0.500	14.3 psf	21.2 psf	9.6 psf	9.3 psf	-4.4 psf	-8.6 psf	14.0 psf	17.9 psf	88.00 ft
60 ft	0.854	0.8378	0.8131	3.07	0.33	-0.248	-0.500	15.1 psf	21.2 psf	10.1 psf	9.8 psf	-4.4 psf	-8.6 psf	14.5 psf	18.4 psf	101.50 ft
70 ft	0.892	0.8378	0.8131	3.07	0.33	-0.248	-0.500	15.7 psf	21.2 psf	10.5 psf	10.2 psf	-4.4 psf	-8.6 psf	14.9 psf	18.9 psf	115.00 ft
80 ft	0.927	0.8378	0.8131	3.07	0.33	-0.248	-0.500	16.3 psf	21.2 psf	11.0 psf	10.6 psf	-4.4 psf	-8.6 psf	15.4 psf	19.3 psf	128.50 ft
90 ft	0.959	0.8378	0.8124	3.07	0.33	-0.248	-0.500	16.9 psf	21.2 psf	11.3 psf	11.0 psf	-4.4 psf	-8.6 psf	15.7 psf	19.6 psf	142.00 ft
100 ft	0.988	0.8378	0.8124	3.07	0.33	-0.248	-0.500	17.4 psf	21.2 psf	11.7 psf	11.3 psf	-4.4 psf	-8.6 psf	16.1 psf	19.9 psf	155.50 ft
120 ft	1.041	0.8378	0.8124	3.07	0.33	-0.248	-0.500	18.3 psf	21.2 psf	12.3 psf	11.9 psf	-4.4 psf	-8.6 psf	16.7 psf	20.6 psf	169.00 ft
140 ft	1.088	0.8378	0.8124	3.07	0.33	-0.248	-0.500	19.2 psf	21.2 psf	12.9 psf	12.5 psf	-4.4 psf	-8.6 psf	17.3 psf	21.1 psf	182.50 ft
160 ft	1.130	0.8378	0.8124	3.07	0.33	-0.248	-0.500	19.9 psf	21.2 psf	13.4 psf	12.9 psf	-4.4 psf	-8.6 psf	17.8 psf	21.6 psf	196.00 ft
180 ft	1.169	0.8378	0.8124	3.07	0.33	-0.248	-0.500	20.6 psf	21.2 psf	13.8 psf	13.4 psf	-4.4 psf	-8.6 psf	18.2 psf	22.0 psf	210.50 ft
200 ft	1.205	0.8378	0.8124	3.07	0.33	-0.248	-0.500	21.2 psf	21.2 psf	14.2 psf	13.8 psf	-4.4 psf	-8.6 psf	18.6 psf	22.4 psf	210.50 ft
250 ft	1.284	0.8378	0.8124	3.07	0.33	-0.248	-0.500	22.6 psf	21.2 psf	15.2 psf	14.7 psf	-4.4 psf	-8.6 psf	19.6 psf	23.3 psf	
300 ft	1.353	0.8378	0.8124													
350 ft	1.414	0.8378	0.8124													
400 ft	1.469	0.8378	0.8124													
450 ft	1.519	0.8378	0.8124													
500 ft	1.565	0.8378	0.8124													



500 Delaware Ave.

**Total Pressure for Frames Resisting Wind Forces Parallel to Y Direction**

Total, Windward, Leeward?

Total

Height above ground level, z	0.5	2	3	4	5	6	7	8	9	10	11	12	13	14	15	R
Floor To Floor Heights	10.25 ft	10.25 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	14.50 ft
Story Elevations	15.38 ft	27.25 ft	40.75 ft	54.25 ft	67.75 ft	81.25 ft	94.75 ft	108.25 ft	121.75 ft	135.25 ft	148.75 ft	162.25 ft	175.75 ft	189.25 ft	202.75 ft	210.50 ft
Mid-Story Elevations	0 ft															
15 ft	15.2 psf	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif	228.3 pif
20 ft	13.8 psf	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif	78.9 pif
25 ft	16.3 psf	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif	81.3 pif
30 ft	16.7 psf	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif	83.3 pif
40 ft	17.4 psf	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif	94.4 pif
50 ft	17.9 psf	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif	99.5 pif
60 ft	18.4 psf	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif	104.6 pif
70 ft	18.9 psf	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif	109.7 pif
80 ft	19.3 psf	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif	114.8 pif
90 ft	19.6 psf	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif	119.9 pif
100 ft	19.9 psf	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif	125.0 pif
120 ft	20.6 psf	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif	140.2 pif
140 ft	21.1 psf	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif	155.4 pif
160 ft	21.6 psf	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif	170.6 pif
180 ft	22.0 psf	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif	185.8 pif
200 ft	22.4 psf	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif	201.0 pif
250 ft	23.3 psf	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif	243.3 pif
300 ft																
350 ft																
400 ft																
450 ft																
500 ft																
Total Story Shear @ Floor	0 pif	87 pif	313 pif	552 pif	799 pif	1056 pif	1319 pif	1589 pif	1866 pif	2149 pif	2433 pif	2725 pif	3020 pif	3319 pif	3621 pif	3956 pif
Story Force per Floor	0.000 klf	0.087 klf	0.239 klf	0.256 klf	0.248 klf	0.256 klf	0.263 klf	0.270 klf	0.277 klf	0.282 klf	0.286 klf	0.291 klf	0.295 klf	0.298 klf	0.303 klf	0.335 klf

**Total Wind Force on MWFRS in Y Direction**

Floor Level	0.5	2	3	4	5	6	7	8	9	10	11	12	13	14	15	R
Length of Building	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft	270.0 ft
Frame Story Force per Floor	0.0 k	23.5 k	61.0 k	64.4 k	66.9 k	69.2 k	71.0 k	72.8 k	74.9 k	76.1 k	77.1 k	78.6 k	79.7 k	80.5 k	81.7 k	90.4 k
Frame Story Shear per Floor	10680.0 k	10680.0 k	10445.5 k	983.5 k	919.1 k	852.1 k	782.9 k	711.9 k	639.2 k	564.2 k	488.1 k	411.0 k	332.3 k	252.6 k	172.1 k	90.4 k

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**Total Pressure for Frames Resisting Wind Forces Parallel to X Direction**

Total, Windward, Leeward?

Height above ground level, z	Int.	2	3	4	5	6	7	8	9	10	11	12	13	14	15	R
<b>Floor To Floor Heights</b>	10.25 ft	10.25 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	13.50 ft	14.50 ft
Story Elevations	10.25 ft	20.50 ft	34.00 ft	47.50 ft	61.00 ft	74.50 ft	88.00 ft	101.50 ft	115.00 ft	128.50 ft	142.00 ft	155.50 ft	169.00 ft	182.50 ft	196.00 ft	210.50 ft
Mid - Story Elevations	15.38 ft	27.25 ft	40.75 ft	54.25 ft	67.75 ft	81.25 ft	94.75 ft	108.25 ft	121.75 ft	135.25 ft	148.75 ft	162.25 ft	175.75 ft	189.25 ft	202.75 ft	210.50 ft
0 ft																
20 ft	11.8 psf	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif	58.9 pif
25 ft	12.3 psf	61 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif	61.3 pif
30 ft	12.7 psf	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif	63.4 pif
40 ft	13.4 psf	53.6 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif	133.9 pif
50 ft	14.0 psf	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif	139.8 pif
60 ft	14.5 psf	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif	144.9 pif
70 ft	14.9 psf	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif	149.5 pif
80 ft	15.4 psf	69.1 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif	153.6 pif
90 ft	15.7 psf	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif	157.3 pif
100 ft	16.1 psf	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif	160.8 pif
120 ft	16.7 psf	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif	334.0 pif
140 ft	17.3 psf															
160 ft	17.8 psf															
180 ft	18.2 psf															
200 ft	18.6 psf															
250 ft	19.6 psf															
300 ft																
350 ft																
400 ft																
450 ft																
500 ft																
<b>Total Story Shear @ Floor</b>	0.0 pif	65.0 pif	237.1 pif	422.3 pif	617.1 pif	820.7 pif	1031.0 pif	1248.3 pif	1473.9 pif	1704.0 pif	1937.9 pif	2177.6 pif	2421.4 pif	2668.4 pif	2919.9 pif	3200.0 pif
<b>Story Force per Floor</b>	0.000 kif	0.065 kif	0.172 kif	0.185 kif	0.195 kif	0.204 kif	0.210 kif	0.217 kif	0.225 kif	0.230 kif	0.234 kif	0.240 kif	0.244 kif	0.247 kif	0.252 kif	0.260 kif

**Total Wind Force on MWFRS in X Direction**

Floor Level	Int.	2	3	4	5	6	7	8	9	10	11	12	13	14	15	R
<b>Length of Building</b>	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft	88.0 ft
<b>Frame Story Force per Floor</b>	0.0 k	5.7 k	15.1 k	16.3 k	17.1 k	17.9 k	18.5 k	19.1 k	19.8 k	20.3 k	20.6 k	21.1 k	21.5 k	21.7 k	22.1 k	24.6 k
<b>Frame Story Shear per Floor</b>	281.6 k	281.6 k	275.9 k	260.7 k	244.4 k	227.3 k	209.4 k	190.9 k	171.7 k	151.9 k	131.6 k	111.1 k	90.0 k	68.5 k	46.8 k	24.6 k

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A.2.2 Seismic

**Input Information**

D	Site Class - Section 1615.1.1
II	Seismic Use Group - Section 1616.2
B	Seismic Design Category - Section 1616.3
.300g	$S_s$ , Spectral Accelerations for Short Periods - Section 1615.1
.075g	$S_1$ , Spectral Accelerations for 1 Second Period - Section 1615.1
1.56	$F_a$ , Site Coefficient - Table 1615.1.2(1)
2.4	$F_v$ , Site Coefficient - Table 1615.1.2(2)
0.468	$S_{MS}$ , Maximum Spectral Accelerations for Short Periods - Section 1615.1.2
0.18	$S_{M1}$ , Maximum Spectral Accelerations for 1 Second Period - Section 1615.1.2
0.312	$S_{DS}$ , Design Spectral Accelerations for Short Periods - Section 1615.1.3
0.12	$S_{D1}$ , Design Spectral Accelerations for 1 Second Period - Section 1615.1.3
0.03	$C_T$ , Building Period Coefficient - Section 1617.4.2.1
0.75	X
210.5 ft	$h_n$ , Building Height - Section 1617.4.2.1
1.66	$T_a = C_T * h_n^{3/4}$ - Approximate Fundamental Period - Section 1617.4.2.1
0.077	$T_O = 0.2 * (S_{D1}/S_{DS})$ - Section 1615.1.4
0.385	$T_S = S_{D1}/S_{DS}$ - Section 1615.1.4
0.072	$S_a$ , Spectral Response Acceleration - Section 1615.1.4
1.25	$I_e$ , Seismic Occupancy Importance Factor - Table 1604.5
5	R, Response Modification Factor - Table 1617.6
0.0780	$C_S$ , Seismic Response Coefficient - Section 1617.4.1.1
0.0172	$C_S$ (min) - Section 1617.4.1.1
0.0181	$C_S$ (Max) - Section 1617.4.1.1
0.0181	$C_S$ (Actual) - Section 1617.4.1.1
39,207 k	W, Effective Seismic Weight of Structure - Section 1617.4.1
709.4	$V = C_S * W$ - Seismic Base Shear - Section 1617.4.1
1.579	k, Distribution Exponent - Section 1617.4.3



2-5 Floor Plan  
Area = 23,011 ft<sup>2</sup>  
Perimeter = 773'



Typical Floor Plan  
Area = 21,900 ft<sup>2</sup>  
Perimeter = 718'



500 Delaware Ave.

Floor	Mass Calculations						Force Calculations					
	Floor-Floor Height (ft)	Area (ft <sup>2</sup> )	Floor Load (psf)	Perimeter	Wall Loading (psf)	Weight	Height from Ground	$w_x h_x^k$	$C_{vx}$ , (Eq. 9.5.4.2)	Story Force (k)	Story Shear (k)	
R		21,900	65.0 psf	718 ft	15.0 psf	1424 k	210.5 ft	0	0	0.0 k	0.0 k	
15	14.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2597 k	210.5 ft	6632316	0.0889	63.1 k	63.1 k	
14	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2669 k	196 ft	10,808,579	0.145	102.8 k	165.9 k	
13	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	182.5 ft	9,927,131	0.133	94.4 k	260.3 k	
12	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	169 ft	8,775,004	0.118	83.5 k	343.8 k	
11	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	155.5 ft	7,694,106	0.103	73.2 k	416.9 k	
10	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	142 ft	6,666,241	0.089	63.4 k	480.3 k	
9	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	128.5 ft	5,693,479	0.076	54.2 k	534.5 k	
8	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	115 ft	4,778,194	0.064	45.4 k	579.9 k	
7	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	101.5 ft	3,923,145	0.053	37.3 k	617.3 k	
6	13.5 ft	21,900	115.0 psf	718 ft	15.0 psf	2664 k	88 ft	3,131,594	0.042	29.8 k	647.0 k	
5	13.5 ft	23,000	115.0 psf	773 ft	15.0 psf	2802 k	74.5 ft	2,407,495	0.032	22.9 k	669.9 k	
4	13.5 ft	23,000	115.0 psf	773 ft	15.0 psf	2802 k	61 ft	1,846,499	0.025	17.6 k	687.5 k	
3	13.5 ft	23,000	115.0 psf	773 ft	15.0 psf	2802 k	47.5 ft	1,243,992	0.017	11.8 k	699.3 k	
2	13.5 ft	23,000	115.0 psf	773 ft	15.0 psf	2802 k	34 ft	733,720	0.010	7.0 k	706.3 k	
Gnd	20.5 ft	23,000	115.0 psf	773 ft	15.0 psf	2802 k	20.5 ft	330,061	0.004	3.1 k	709.4 k	
<b>TOTAL</b>	<b>210.5 ft</b>	<b>355,900</b>				<b>39,207 k</b>	<b>TOTAL</b>	<b>74,591,555</b>	<b>1.000</b>	<b>709.45</b>		

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## APPENDIX B: PRELIMINARY MEMBER DESIGN

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## B.I Post-tensioned Slab

Given: Live Load = 80 psf

Dead Load = 100 psf (assuming 8" thick slab)

Total Load = 180 psf

Preliminary Design:

- Balance Load:
- Net Load:  $\omega_n = TL - \omega_{pre}$   
 $\omega_n = 180 \text{ psf} - 90 \text{ psf} = 90 \text{ psf}$
- Design limits
  - Cover:  $\frac{3}{4}$ " from top and bottom
  - Allowable Stresses: Class U
    - At time of jacking
      - $f'_c = 6,000 \text{ psi}$
      - Compression (18.4.2a) =  $0.60 f'_c = 0.6(6,000 \text{ psi}) = 3,600 \text{ psi}$
      - Tension (18.4.2b) =  $3\sqrt{f'_c} = 3\sqrt{6000 \text{ psi}} = 232 \text{ psi}$
    - At service
      - $f'_c = 6,000 \text{ psi}$
      - Compression =  $0.45 f'_c = 0.45(6,000 \text{ psi}) = 2,700 \text{ psi}$
      - Tension =  $6\sqrt{f'_c} = 6\sqrt{6000 \text{ psi}} = 465 \text{ psi}$
  - Average pre-compression limits = 125 psi (min)  
 = 300 psi (max)
  - Target Load Balances: 60%-80% of selfweight for slabs. Use 75%
    - $\omega_{pre} = 0.75 \text{ slab}$
    - $\omega_{pre} = 0.75(100 \text{ psf}) = 75 \text{ psf}$
- Tendon profile
  - $a_A = 4.0"$
  - $a_B = \frac{(4.0" + 7.0")}{2} - 1.75" = 3.75"$
- Prestress Force Required to Balance 70% of selfweight



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$$\circ w_b = 0.70(100 \text{ psf})(52.5') = 3675 \text{ plf} = 3.68 \text{ klf}$$

- Force needed in tendons to counteract the load in bay A-B.

$$\circ P = \frac{w_b l^2}{8a_A} = \frac{3.68 \text{ klf}(30')^2}{8(3.75"/12)} = 1323 \text{ k}$$

- Check Precompression

$$\circ \# \text{ tendons} = \frac{(1323 \text{ k})}{26.6 \text{ k / tendon}} = 49 \text{ tendons}$$

$$\circ \text{ Actual force for banded tendons: } P_{\text{actual}} = (49 \text{ tendons})(26.6 \text{ k}) = 1303 \text{ k}$$

$$\circ \text{ Actual precompression stress: } \frac{P_{\text{actual}}}{A} = \frac{1303 \text{ k}}{630 \text{ in}^2 \times 8"} = 259 \text{ psi}$$

$$\square 125 \text{ psi} < 259 \text{ psi} < 300 \text{ psi}$$

- Check Interior Span Force

$$\square P = \frac{(3.68 \text{ klf})(30')^2}{8(6")} = 827 \text{ k} < 1303 \text{ k} \text{ Less force is required in the center bay.}$$

- Check balance load for interior

$$\bullet w_b = \frac{(1303 \text{ k})(8)(6"/12)}{(30')^2} = 5.7 \text{ klf}$$

$$\bullet \frac{w_b}{w_{DL}} = \frac{5.7 \text{ klf}}{5.25 \text{ klf}} = 100\%$$

- **Effective prestress force,  $P_{\text{eff}} = 1303 \text{ k}$**

For further analysis, this layout was entered into RAM Concept and checked further.

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**B.2 Columns**

Typical Columns Along Column Line 1

k	2	trib. W	30'
A <sub>t</sub>	790 sf	f <sub>c</sub>	6 ksi
span l <sub>ab</sub>	52.5'	beam	800 plf
span l <sub>bc</sub>	36'		

	w <sub>LL</sub>	A <sub>t</sub> (ft <sup>2</sup> )	A <sub>i</sub> (ft <sup>2</sup> ) = A <sub>t</sub> x k	Reduction = 0.25+ <sup>15</sup> / <sub>√A<sub>i</sub></sub>	LL (k)	w <sub>DL</sub> (psf)	DL (k)	Pu (k)	w <sub>uTL</sub> (psf)	FEM <sub>ab</sub>
R	60	790	1,580	0.63	30	65	72	134 k	3.24	447'k
15	80	1,580	3,160	0.52	65	115	224	373 k	7.98	1100'k
14	80	2,370	4,740	0.47	89	115	336	545 k	7.98	1100'k
13	80	3,160	6,320	0.44	111	115	447	714 k	7.98	1100'k
12	80	3,950	7,900	0.42	132	115	559	883 k	7.98	1100'k
11	80	4,740	9,480	0.40	153	115	671	1050 k	7.98	1100'k
10	80	5,530	11,060	0.40	177	115	783	1223 k	7.98	1100'k
9	80	6,320	12,640	0.40	202	115	895	1397 k	7.98	1100'k
8	80	7,110	14,220	0.40	228	115	1007	1572 k	7.98	1100'k
7	80	7,900	15,800	0.40	253	115	1119	1747 k	7.98	1100'k
6	80	8,690	17,380	0.40	278	115	1230	1921 k	7.98	1100'k
5	80	9,480	18,960	0.40	303	115	1342	2096 k	7.98	1100'k
4	80	10,270	20,540	0.40	329	115	1454	2271 k	7.98	1100'k
3	80	11,060	22,120	0.40	354	115	1566	2445 k	7.98	1100'k
2	80	11,850	23,700	0.40	379	115	1678	2620 k	7.98	1100'k

	b	h	γ	Rn	Kn	ρ	A <sub>s</sub>		
R	20 in	20 in	0.80	0.1717	0.0862	0.031	12.4	(8)	#11
15	20 in	26 in	0.85	0.2503	0.1839	0.042	21.84	(14)	#11
14	20 in	26 in	0.85	0.2503	0.2685	0.048	24.96	(16)	#11
13	20 in	26 in	0.85	0.2503	0.3522	0.048	24.96	(16)	#11
12	20 in	26 in	0.85	0.2503	0.4353	0.048	24.96	(16)	#11
11	20 in	26 in	0.85	0.2503	0.5180	0.048	24.96	(16)	#11
10	20 in	26 in	0.85	0.2503	0.6029	0.048	24.96	(16)	#11
9	20 in	30 in	0.87	0.1880	0.5972	0.047	28.2	(18)	#11
8	20 in	30 in	0.87	0.1880	0.6718	0.047	28.2	(18)	#11
7	20 in	30 in	0.87	0.1880	0.7464	0.047	28.2	(18)	#11
6	20 in	30 in	0.87	0.1880	0.8211	0.047	28.2	(18)	#11
5	20 in	30 in	0.87	0.1880	0.8957	0.075	45	(20)	#14
4	20 in	30 in	0.87	0.1880	0.9704	0.075	45	(20)	#14
3	20 in	30 in	0.87	0.1880	1.0450	0.075	45	(20)	#14
2	20 in	30 in	0.87	0.1880	1.1197	0.075	45	(20)	#14

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## Typical Columns Along Column Line 3

k	2	trib. W	30'
A <sub>t</sub>	540 sf	f <sub>c</sub>	6 ksi
span l <sub>ab</sub>	52.5'	beam	800 plf
span l <sub>bc</sub>	36'		

	w <sub>LL</sub>	A <sub>t</sub> (ft <sup>2</sup> )	A <sub>i</sub> (ft <sup>2</sup> ) = A <sub>t</sub> x k	Reduction= 0.25+15/√A <sub>i</sub>	LL (k)	w <sub>DL</sub> (psf)	DL (k)	Pu (k)	w <sub>uTL</sub> (psf)	w <sub>uDL</sub> (psf)	FEM <sub>bc</sub>
R	60	540	1,080	0.71	23	65	50	96 k	3.24	2.34	152'k
15	80	1,080	2,160	0.57	49	115	153	263 k	7.98	4.14	268'k
14	80	1,620	3,240	0.51	67	115	230	382 k	7.98	4.14	268'k
13	80	2,160	4,320	0.48	83	115	306	499 k	7.98	4.14	268'k
12	80	2,700	5,400	0.45	98	115	383	616 k	7.98	4.14	268'k
11	80	3,240	6,480	0.44	113	115	459	732 k	7.98	4.14	268'k
10	80	3,780	7,560	0.42	128	115	536	847 k	7.98	4.14	268'k
9	80	4,320	8,640	0.41	142	115	612	962 k	7.98	4.14	268'k
8	80	4,860	9,720	0.40	156	115	689	1076 k	7.98	4.14	268'k
7	80	5,400	10,800	0.40	173	115	765	1194 k	7.98	4.14	268'k
6	80	5,940	11,880	0.40	190	115	842	1314 k	7.98	4.14	268'k
5	80	6,480	12,960	0.40	207	115	918	1433 k	7.98	4.14	268'k
4	80	7,020	14,040	0.40	225	115	995	1553 k	7.98	4.14	268'k
3	80	7,560	15,120	0.40	242	115	1071	1672 k	7.98	4.14	268'k
2	80	8,100	16,200	0.40	259	115	1148	1792 k	7.98	4.14	268'k

	b	h	γ	Rn	Kn	ρ	As		
R	18 in	18 in	0.78	0.080	0.076	0.022	7.128	(9)	#8
15	18 in	24 in	0.83	0.080	0.156	0.022	9.504	(12)	#8
14	18 in	24 in	0.83	0.080	0.227	0.08	34.56	(10)	#8
13	18 in	24 in	0.83	0.080	0.296	0.08	34.56	(10)	#8
12	18 in	24 in	0.83	0.080	0.366	0.08	34.56	(10)	#8
11	18 in	24 in	0.83	0.080	0.434	0.08	34.56	(10)	#8
10	18 in	24 in	0.83	0.080	0.503	0.08	34.56	(10)	#8
9	18 in	24 in	0.83	0.080	0.571	0.03	12.96	(16)	#8
8	18 in	28 in	0.86	0.058	0.548	0.03	15.12	(16)	#8
7	18 in	28 in	0.86	0.058	0.608	0.03	15.12	(16)	#8
6	18 in	28 in	0.86	0.058	0.668	0.03	15.12	(16)	#8
5	18 in	28 in	0.86	0.058	0.729	0.05	25.2	(16)	#11
4	18 in	28 in	0.86	0.058	0.790	0.05	25.2	(16)	#11
3	18 in	28 in	0.86	0.058	0.851	0.05	25.2	(16)	#11
2	18 in	28 in	0.86	0.058	0.912	0.05	25.2	(16)	#11

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Column Schedule

	C-1	C-2	C-3	C-4	C-5	C-6	C-7	C-8
R	22x 22 (16)- #9 2228k	18x 18 (18)- #4 1212k	24x 24 (18)- #6 2218k	24x 24 (16)- #9 2533k	22x 22 (20)- #8 2221k	22x 26 (16)- #8 2389k	22x 26 (16)- #6 2171k	
15	22x 26 (16)- #6 2171k	18x 24 (18)- #5 1648k	32x 32 (18)- #7 3816k	22x 26 (16)- #9 2520k	22x 26 (20)- #7 2364k	22x 26 (16)- #9 2520k	22x 26 (16)- #6 2171k	
14	22x 26 (16)- #6 2171k	18x 24 (18)- #5 1648k	32x 32 (18)- #7 3816k	22x 26 (16)- #6 2171k	22x 26 (20)- #5 #N/A	22x 26 (16)- #6 2171k	22x 26 (16)- #6 2171k	
13	22x 26 (16)- #6 2171k	18x 24 (18)- #5 1648k	32x 32 (18)- #7 3816k	22x 26 (16)- #6 2171k	22x 26 (20)- #5 #N/A	22x 26 (16)- #6 2171k	22x 26 (16)- #6 2171k	
12	22x 26 (16)- #6 2170.740k	18x 24 (18)- #5 1647.594k	32x 32 (18)- #7 3815.760k	22x 26 (16)- #6 2170.740k	22x 26 (20)- #5 #N/A	22x 26 (16)- #6 2170.740k	22x 26 (16)- #6 2170.740k	
11	22x 26 (16)- #6 2171k	18x 24 (18)- #5 1648k	32x 32 (18)- #7 3816k	22x 26 (16)- #6 2171k	22x 26 (20)- #5 #N/A	22x 26 (16)- #6 2171k	22x 26 (16)- #6 2171k	
10	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	32x 32 (18)- #7 3816k	22x 32 (16)- #6 2608k	22x 32 (20)- #6 2677k	22x 30 (16)- #6 2462k	22x 30 (16)- #6 2462k	
9	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	32x 32 (18)- #7 3816k	22x 32 (16)- #6 2608k	22x 32 (20)- #6 2677k	22x 30 (16)- #6 2462k	22x 30 (16)- #6 2462k	
8	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	32x 32 (18)- #7 3816k	22x 32 (16)- #6 2608k	22x 32 (20)- #6 2677k	22x 30 (16)- #6 2462k	22x 30 (16)- #6 2462k	
7	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	32x 32 (18)- #7 3816k	22x 32 (16)- #6 2608k	22x 32 (20)- #6 2677k	22x 30 (16)- #6 2462k	22x 30 (16)- #6 2462k	
6	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	32x 32 (18)- #7 3816k	22x 32 (16)- #6 2608k	22x 32 (20)- #6 2677k	22x 30 (16)- #6 2462k	22x 30 (16)- #6 2462k	
5	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	34x 34 (18)- #8 4387k	22x 32 (16)- #6 2608k	22x 32 (20)- #6 2677k	22x 30 (16)- #6 2462k	22x 30 (16)- #6 2462k	12x 12 (8)- #4 539k
4	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	34x 34 (18)- #9 4534k	22x 32 (16)- #8 2827k	22x 32 (20)- #8 2950k	22x 30 (16)- #8 2681k	22x 30 (16)- #6 2462k	12x 12 (8)- #4 539k
3	22x 32 (16)- #6 2608k	18x 28 (18)- #5 1886k	34x 34 (18)- #11 4927k	22x 32 (16)- #10 3126k	22x 32 (20)- #10 3324k	22x 30 (16)- #10 2980k	22x 30 (16)- #6 2462k	12x 12 (8)- #4 539k
2	22x 32 (16)- #6 2608k	18x 28 (18)- #6 1980k	34x 34 (18)- #14 5412k	22x 32 (16)- #11 3307k	22x 32 (20)- #11 3551k	22x 30 (16)- #11 3161k	22x 30 (16)- #6 2462k	12x 12 (8)- #4 539k

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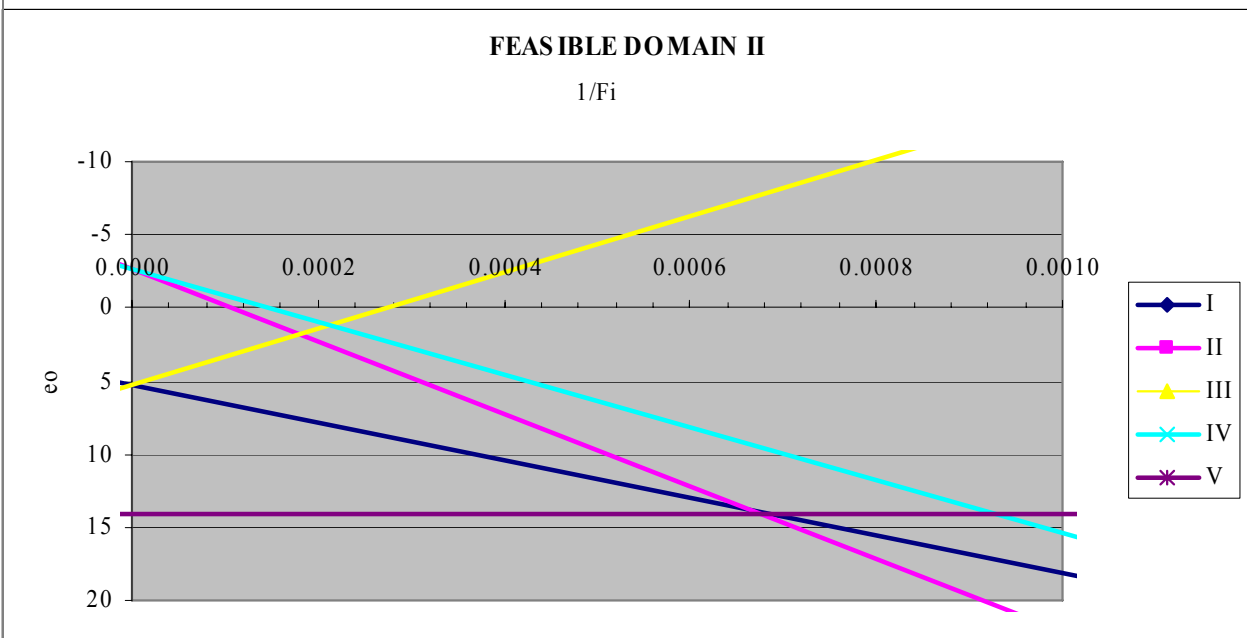
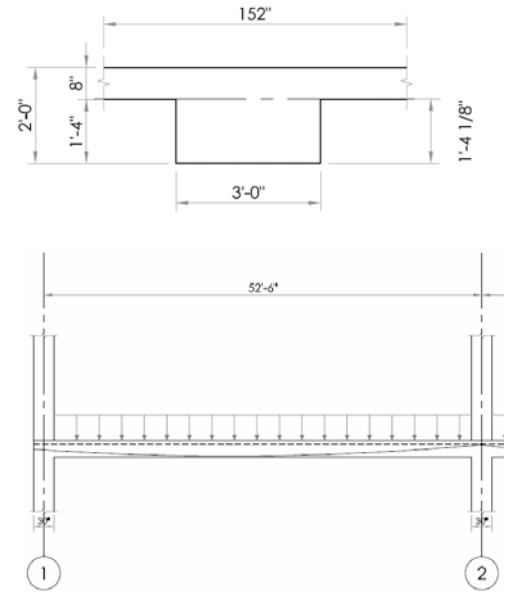
### B.3 Beams

Note: All beams analyzed in a similar manner to the following two procedures.

#### Detailed Calculation of 52' Post-tensioned beams

Stresses		Losses			
$f'_c$	6000 psi	$\sigma_{ci}$	3 ksi		
$f'_{ci}$	5000 psi	$\sigma_{cs}$	4 ksi		
$f_{pu}$	270 ksi	$\sigma_{ti}$	0 ksi		
$f_{pi}$	181 ksi	$\sigma_{ts}$	-1 ksi		
$f_{pv}$	243 ksi	$\eta$	0.85		
Input Information					
L span	53'	$A_{ps}$	0 sq in		
dc,min	2 in	h	24 in		
Section Properties					
A (in <sup>2</sup> )	I (in <sup>4</sup> )	$y_b$ (in)	$y_t$ (in)		
1792	75057	16.1429	7.8571		
$z_b$ (in)	$z_t$ (in)	$k_b$ (in)	$k_t$ (in)		
4650	9553	5.33	-2.59		
$M_{mid-span}$ (in-k)					
$\omega_g$ (plf)	$\omega_{LL}$ (plf)	$M_{min}$	$M_{max}$		
3600	2,400	10,825	18,041		
1/Fi					
$e_o$	I	II	III	IV	V
-30	-0.0027	-0.0011	0.0018	-0.0015	14.1429
30	0.0019	0.0013	-0.0013	0.0018	14.1429

Selection of Force	
IV	V
$F_i$	1078 k
Selection of Steel	
0.8 $f_{pu}$	216 ksi
0.7 $f_{pu}$	189 ksi
$A_s$	5.96 sq in
#strands	39
$F_i$	1080 k
$e_{o,u}$	14 in
$e_{o,l}$	14 in
$e_{o,mid}$	14 in
$e_{o,supp}$	5 in



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**Detailed Calculation of 36' Interior Post-tensioned Beam**

Stresses		Losses	
$f'_c$	6000 psi	$\sigma_{ci}$	3 ksi
$f'_{ci}$	5000 psi	$\sigma_{cs}$	4 ksi
$f_{pu}$	270 ksi	$\sigma_{ti}$	0 ksi
$f_{pi}$	181 ksi	$\sigma_{ts}$	-1 ksi
$f_{pv}$	243 ksi	$\eta$	0.85

Input Information			
$L_{span}$	36'	$A_{ps}$	0.15 sq in
$d_{c,min}$	2 in	$h$	24 in

Section Properties			
$A$ (in <sup>2</sup> )	$I$ (in <sup>4</sup> )	$y_b$ (in)	$y_t$ (in)
1600	56702	17.12	6.88
$z_b$ (in)	$z_t$ (in)	$k_b$ (in)	$k_t$ (in)
3312	8242	5.15	-2.07

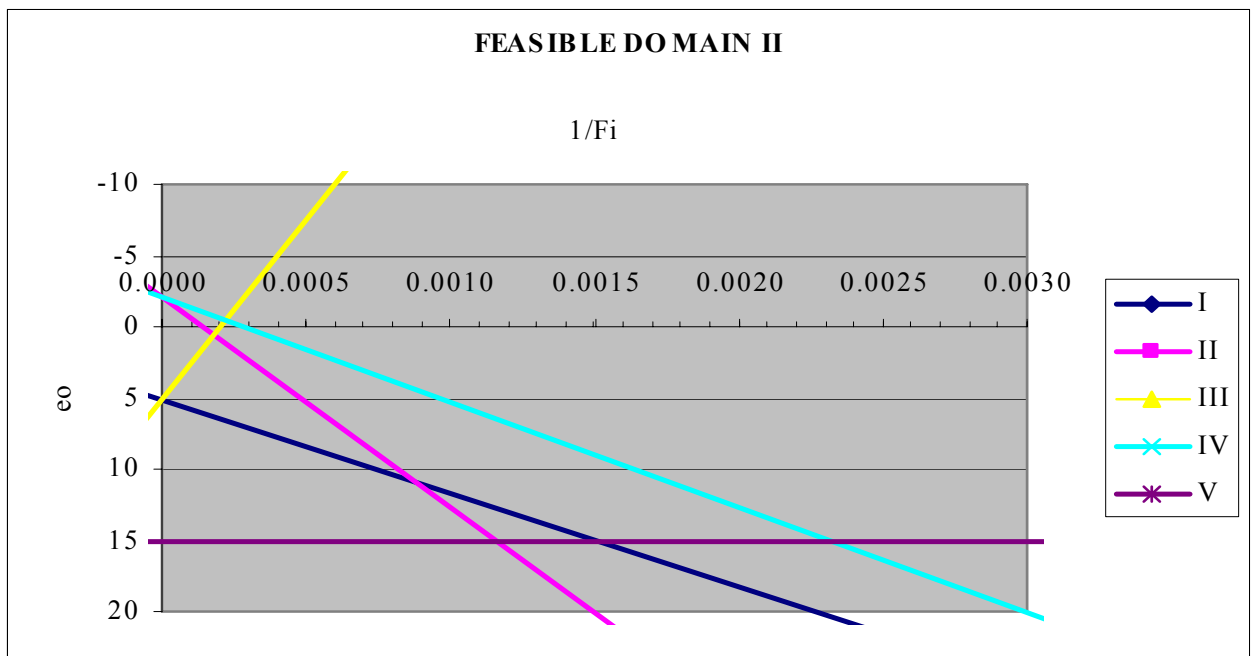
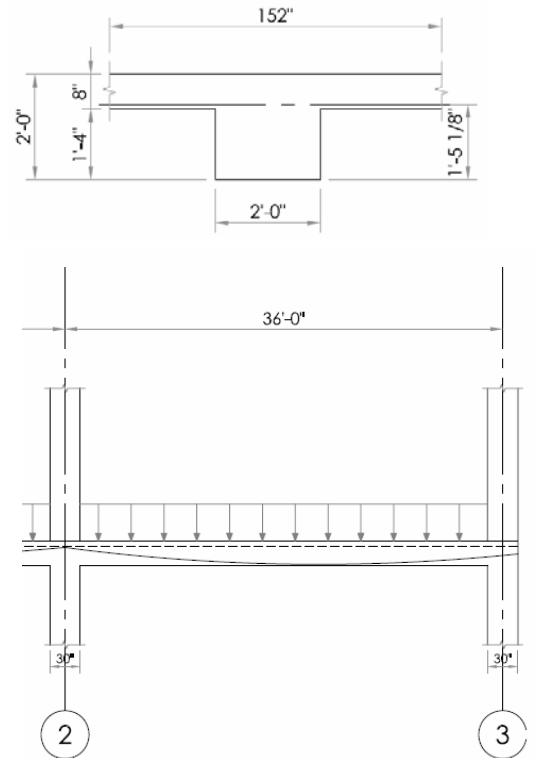
$M_{mid-span}$ (in-k)			
$\omega_g$ (plf)	$\omega_{LL}$ (plf)	$M_{min}$	$M_{max}$
3400	2,400	4,807	8,200

1/Fi					
$e_o$	I	II	III	IV	V
-30	-0.0054	0.0019	0.0014	-0.0038	15.12
30	0.0038	0.0022	-0.0010	0.0043	15.12

Selection of Force	
IV	V
$F_i$	430 k

Selection of Steel	
$0.8f_{pu}$	216 ksi
$0.7f_{pu}$	189 ksi
$A_s$	2.37 sq in
$\#_{strands}$	16
$F_i$	443 k
$e_{o,u}$	15 in
$e_{o,l}$	15 in
$e_{o,mid}$	15 in
$e_{o,supp}$	5 in





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**B.4 Shearwalls**

The shearwalls are designed using 4000 psi concrete and use the forces for wind in the north-south direction for the north-south walls and use the forces for seismic activity in the east-west direction. The hand calculations below show preliminary designs and the formulas used in the following spreadsheets.

$$V_u \leq \phi V_n$$

$$V_n = V_c + V_s$$

- $V_c = 2\sqrt{f'_c}hd = 2\sqrt{4000\text{ psi}}(12'')\left(0.8 \times 36' \times 12 \frac{\text{in}}{\text{ft}}\right) = 525k$

- $V_s = \frac{A_v f_y d}{s}$

- Horizontal Reinforcing

$$\rho_{h,\min} = 0.0025$$

$$A_{h,\min} = 0.0025(13.5' \times 12'')(36' \times 12'') = 175 \text{ in}^2$$

$$s_{\max} = \min \begin{cases} \frac{l_w}{5} = 86.4'' \\ 3h = 36'' = 18'' \\ 18'' \end{cases}$$

Try #6 @ 14'':  $A_h = 183 \text{ in}^2, \rho = 0.0026$

- Vertical Reinforcing

$$\rho_{v,\min} = 0.0025$$

$$\rho_v = 0.0025 + 0.5 \left( 2.5 - \frac{211'}{36'} \right) (0.0026 - 0.0025) = 0.0023 \therefore 0.0025$$

$$s_{\max} = \min \begin{cases} \frac{l_w}{3} = 144'' \\ 3h = 36'' = 18'' \\ 18'' \end{cases}$$

Try #6 @ 14'':  $A_v = 183 \text{ in}^2, \rho = 0.0026$

$$V_s = \frac{A_v f_y d}{s} = \frac{183 \text{ in}^2 (60 \text{ ksi}) (0.8 \times 36' \times 12'')}{14''} = 271k$$

$$V_n = 525k + 271k = 796k$$

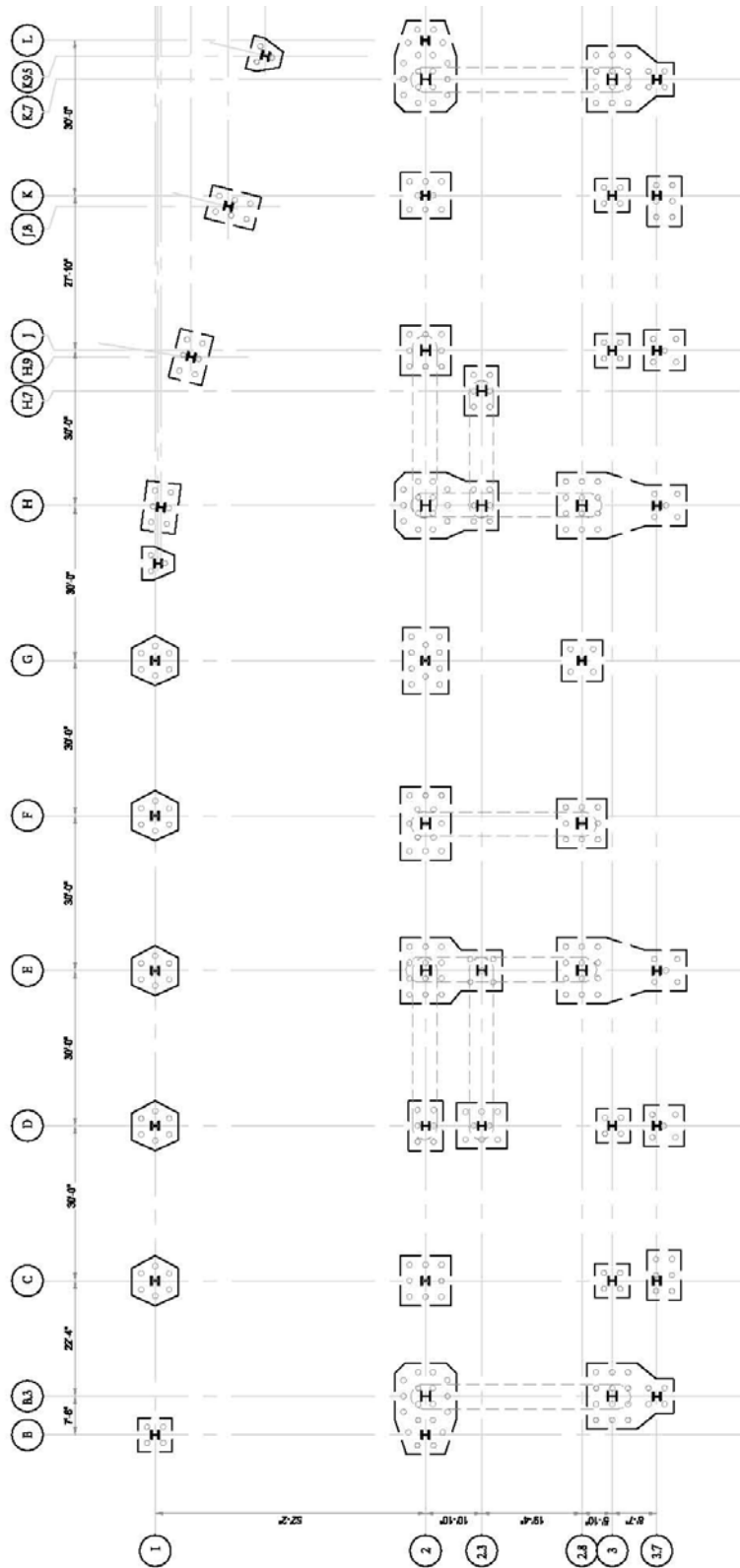
$$\phi V_n = 0.75(796k) = 597k$$

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## APPENDIX C: PLANS

500 Delaware Ave.

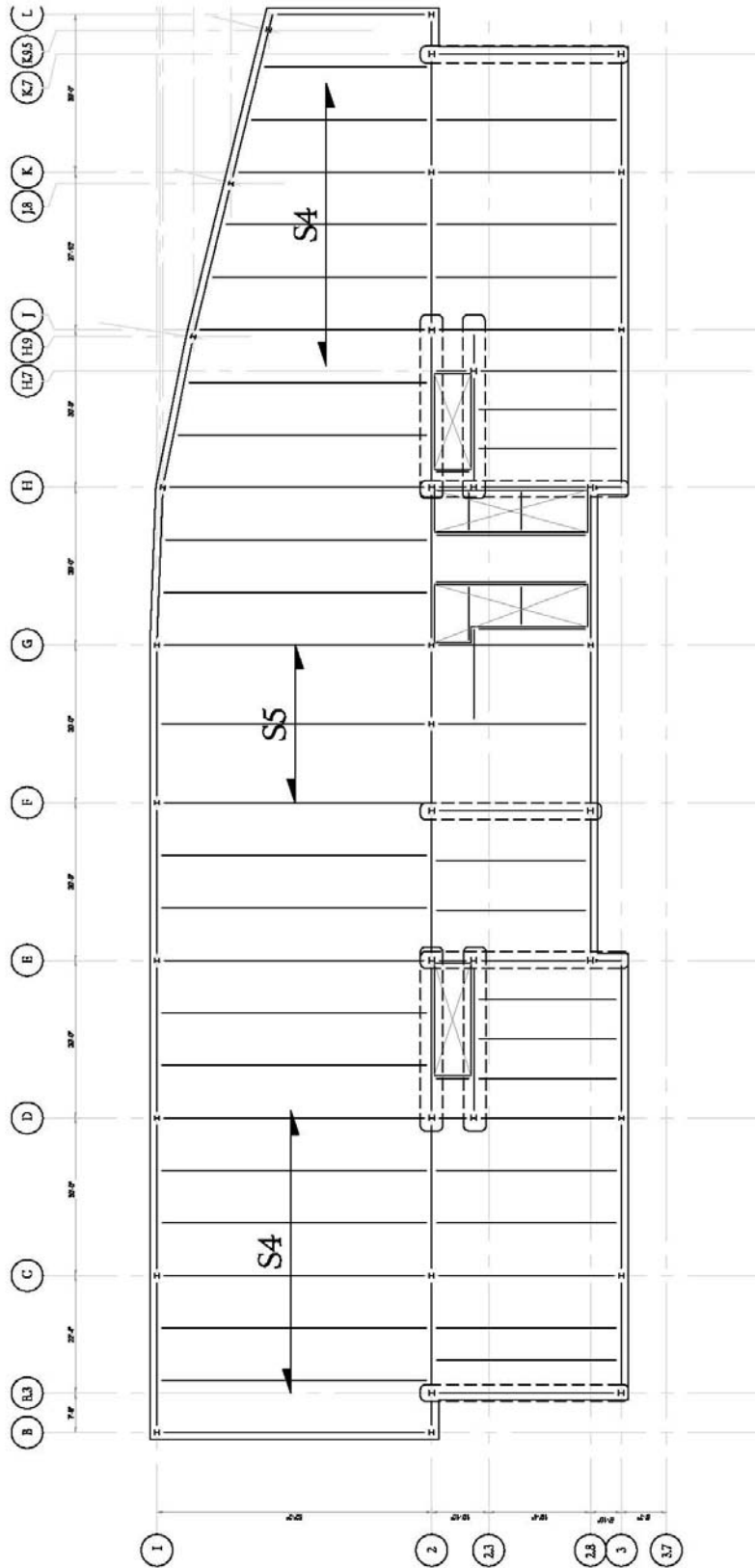
C.I Composite Steel-Foundation



COMPOSITE STEEL FOUNDATION PLAN

500 Delaware Ave.

C.2 Composite Steel-Typical Floor

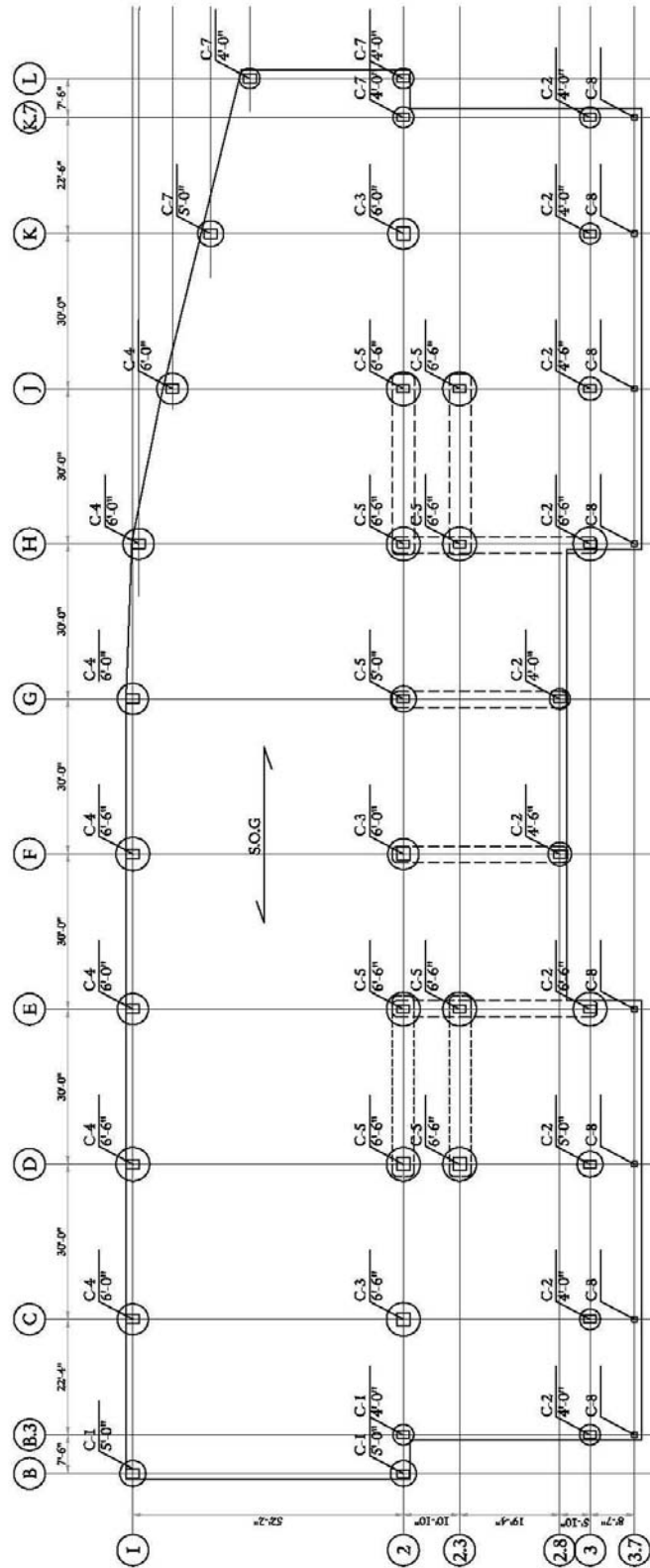


TYPICAL FLOOR FRAMING PLAN

1. DECK OVERHANG IS 16"
2.  $\overline{S4}$  REFERS TO 3-1/4" NWT. CONC. ON 3" 20 GAGE COMPOSITE LOK-FLOOR DECK, UNSHORED.
3.  $\overline{S5}$  REFERS TO 3-1/4" NWT. CONC. ON 3" 16 GAGE COMPOSITE LOK-FLOOR DECK, SHORED.

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C.3 Post-tensioned Concrete-Foundation

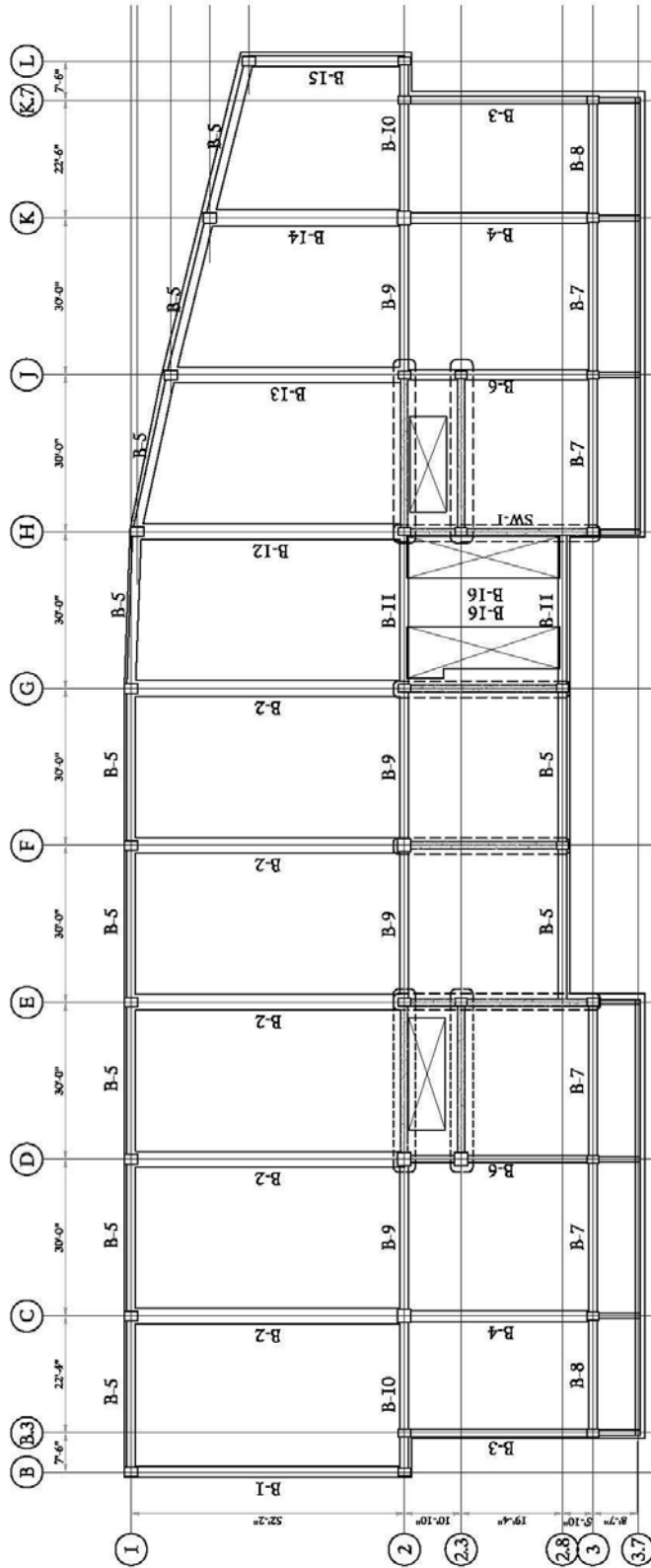


FOUNDATION PLAN

1.  $\leftarrow$  S.O.G.  $\rightarrow$  INDICATES 5" THK. SLAB ON GRADE ON STONE AND COMPACTED FILL.
2. REFER TO COLUMN SCHEDULE COLUMN SCHEDULE FOR COLUMN SIZES.
3.  $\square$  COLUMN  
 $\square$  CAISSON

500 Delaware Ave.

### C.4 Post-tensioned Concrete-Floor Framing

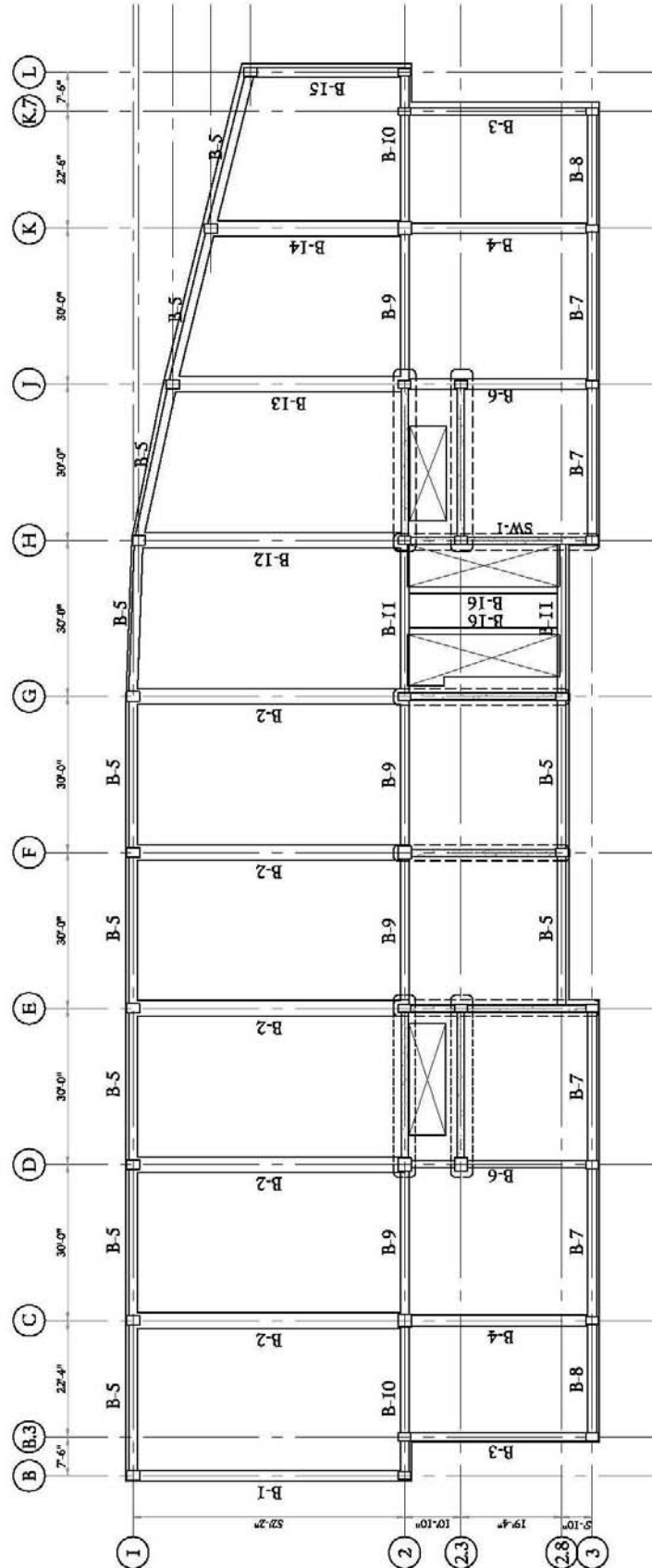


## FLOORS 2-5 FRAMING PLAN

1. INDICATES 8" THK. POST-TENSIONED CONCRETE SLAB. SEE POST-TENSIONED SLAB PLAN.
2. REFER TO BEAM SCHEDULE FOR BEAM SIZES AND REINFORCEMENT.



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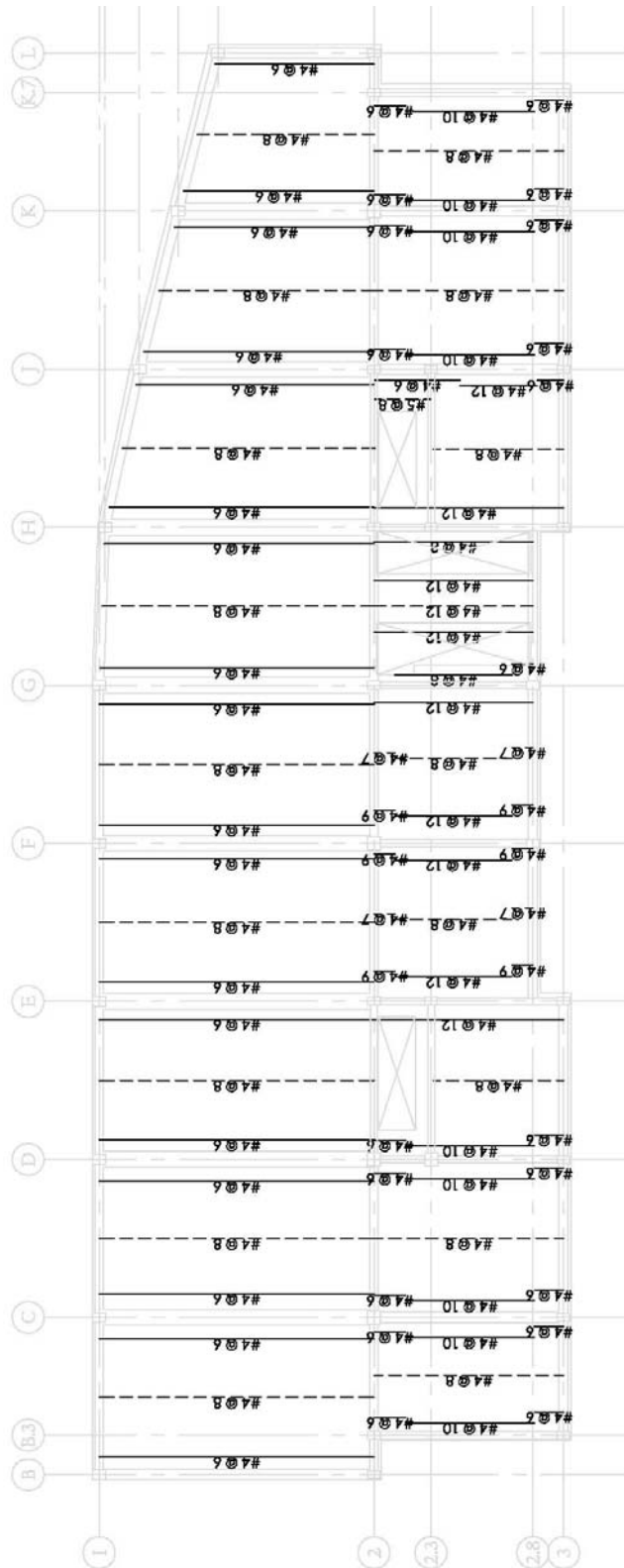


## TYPICAL FRAMING PLAN

1. INDICATES 8" THK. POST-TENSIONED CONCRETE SLAB. SEE SLAB TENDON PLAN.
2. REFER TO BEAM SCHEDULE FOR BEAM SIZES AND REINFORCEMENT.

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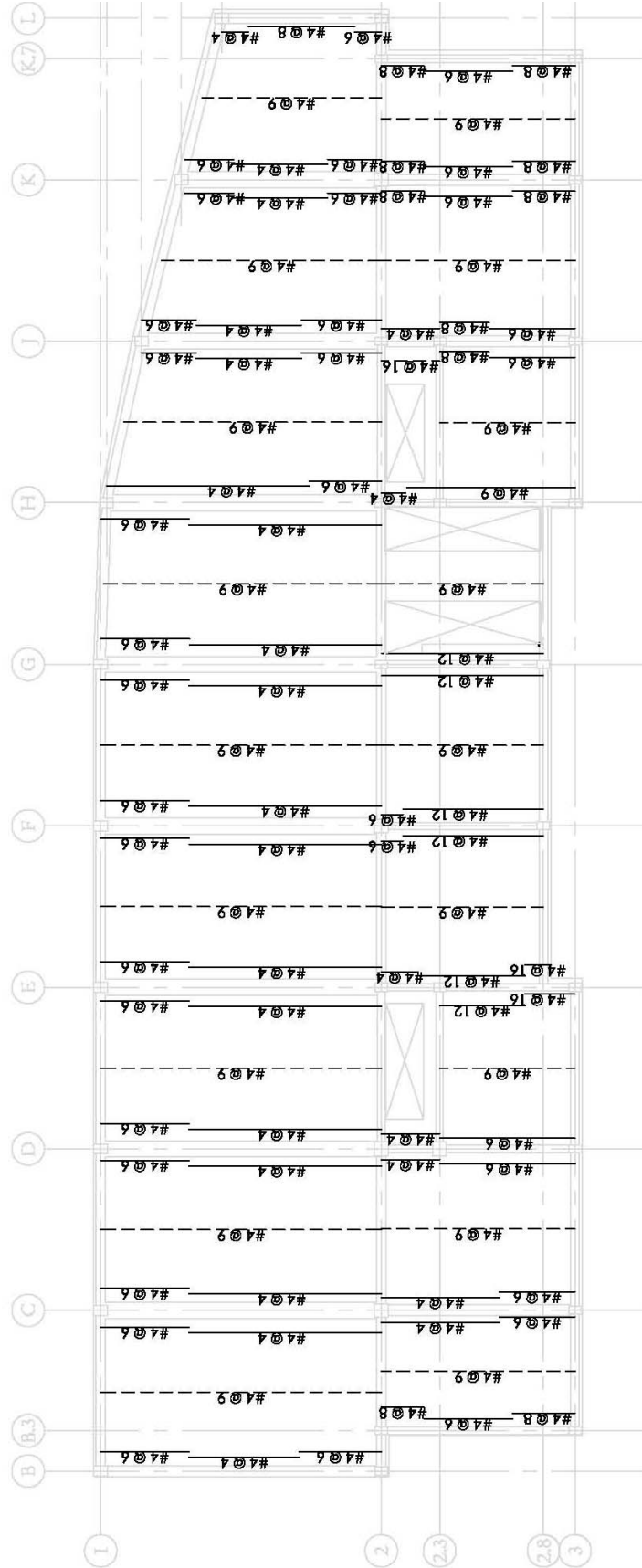
C.5 Post-tensioned Concrete-Reinforcement



LONGITUDE TOP REINFORCING PLAN

- 1. ——— INDICATES COLUMN STRIP REINFORCING.
- 2. - - - - - INDICATES MIDDLE STRIP REINFORCING.

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# LONGITUDE BOTTOM REINFORCING PLAN

- 1. ——— INDICATES COLUMN STRIP REINFORCING.
- 2. - - - - INDICATES MIDDLE STRIP REINFORCING.





500 Delaware Ave.

## APPENDIX D: BREADTH STUDIES

500 Delaware Ave.

**D.I Mechanical Studies**

## ASHRAE Standard 62-Ventilation for Indoor Air Quality

Office	$A_z$ (ft <sup>2</sup> )	$R_p$	$P_z$	$R_a$	$A_z$ (ft <sup>2</sup> )	$V_{bz}$ (cfm)	$V_{oz}$ (cfm)	$V_{pz}$ (cfm)	$Z_p$ (cfm)	$V_{ou}$ (cfm)	# diffusers	cfm/duct
1	2911	5	30	0.06	2911	325	325	3782	0.0859	325	6	630
2	3738	5	38	0.06	3738	415	415	4857	0.0855	415	9	540
3	3513	5	36	0.06	3513	391	391	4564	0.0857	391	6	761
4	2137	5	22	0.06	2137	239	239	2776	0.0861	239	4	694
5	2600	5	26	0.06	2600	286	286	3378	0.0847	286	5	676
6	2592	5	26	0.06	2592	286	286	3368	0.0849	286	5	674
<b><math>\Sigma</math></b>	<b>17491</b>				<b>17491</b>		<b>1942</b>			<b>1942</b>		

500 Delaware Ave.

## D.2 Construction Studies

## D.2.1 Material Takeoffs

<b>Post-tensioned Concrete</b>					
<b>Beams and Slabs: Takeoffs from RAM Concept</b>		<b>Beam Formwork</b>			
<i>Volume</i>	687 CY	<i>Type</i>	<i>#</i>	<i>A</i>	<i>Contact Area</i>
<i>Perimeter</i>	719'	<i>B-1</i>	1.5	228 SF	341 SFCA
<i>Floor Area</i>	24000 SF	<i>B-2</i>	7.5	298 SF	2231 SFCA
<i>Slab thickness</i>	8 in	<i>B-3</i>	2	150 SF	300 SFCA
<i>Prestressing</i>	26350 lb	<i>B-4</i>	4	168 SF	672 SFCA
<i>Reinforcing</i>	46.18 tons	<i>B-5</i>	25	140 SF	3500 SFCA
<i>Slab Formwork</i>	21910 sf			<b>Total</b>	<b>7045 SFCA</b>
<i>Slab Edge Forms</i>	479 SFCA	<b>Shearwalls</b>			
<b>Columns</b>		<i>#</i>	<i>length</i>	<i>height</i>	<i>Area</i>
<i>Volume/column</i>	2 CY	6	30'	14'	2430 SF
<i># columns/floor</i>	36	2	36'	14'	972 SF
<b>Volume/floor</b>	<b>72</b>			<b>Total</b>	<b>3402 SF</b>

<b>Composite Steel</b>			
<b>Structural Steel: Takeoffs from RAM Beam</b>			
<i>Steel</i>	107 tons	<i>Slab Thickness</i>	4 in
<i># shear studs</i>	27352	<i>Frames</i>	50 tons
<b>Fireproofing</b>			
<i>Beam</i>	<i>#</i>	<i>A</i>	<i>Totals</i>
W24x55	28	295	8260
W24x55	20	202	4040
W24x76	27	185	4995
<i>Column</i>			
W14x120	36	97.4	3506.4

<b>Caissons</b>						
		<b>Amount</b>	<b>Material</b>	<b>Labor</b>	<b>Equipment</b>	<b>Cost</b>
A1020-310	4'-0" dia. x 100'	20 Ea	4358	70459		\$1,496,329
	5'-0" dia. x 100'	6 Ea	8064	144990		\$918,324
	6'-0" dia. x 100'	10 Ea	11730	172277		\$1,840,069
					<b>TOTAL</b>	<b>\$4,254,722</b>
<b>Concrete Filled, Drilled Piers</b>						
A1020-130	End Bearing Steel Piles					<b>Cost</b>
2380	4 pile cluster	5	5625	3325		\$44,750
2460	6 pile cluster	8	8425	5025		\$107,600
2480	7 pile cluster	7	9825	5850		\$109,725
2500	8 pile cluster	5	12600	7525		\$100,625
2560	12 pile cluster	9	15400	9200		\$221,400
03310-240	Pile caps, incl. forms and reinf.	612	108	49	0.31	\$96,309
					<b>TOTAL</b>	<b>\$680,409</b>



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## D.2.2 Estimates

Estimate of Post-tensioned Concrete Design for One Typical Floor						
Slabs System		Amount	Material	Labor	Equipment	Cost
03110-405	Beam formwork	7044 SFCA	0.91	4.05		\$63,466
03110-420	slab edge forms	479 SFCA	0.48	4.6		\$2,432
	slab formwork	21910 sf	1.3	2.86		\$216,471
03210-600	Slab Reinforcing	46.18 tons	800	380		\$72,041
032230-600	UngROUTed Post-tensioned strand	26350 lb	0.47	0.87	0.02	\$58,761
03300-220	6000 psi Concrete	687 CY	109			\$74,883
03310-700	Placing	687 CY	11.5	4.7		\$11,129
	<b>Total</b>					<b>\$499,183</b>
Columns						
03310-240	24"x24" average reinforcing including 4 use forms, concrete, placement, reinforcing	72 CY	370	400	41	\$58,392
	<b>Total</b>					<b>\$58,392</b>
Shearwalls						
B2010-101	12" thick, plain finish, 4000 psi wall including 4 use forms, reinforcing, concrete, placement	3402 sf	6.6	15.35	21.95	\$97,127
	<b>Total</b>					<b>\$97,127</b>
					<b>Total</b>	<b>\$654,702</b>
					<b>Cost/sf</b>	<b>\$28</b>

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Estimate of Composite Steel Design for One Typical Floor						
Slabs System		Amount	Material	Labor	Equipment	Total Cost
05310-300	20 ga. 3-1/4" Metal Deck	23403 SF	1.88	0.34	0.02	\$60,380
03210-200	6x6 W1.4xW1.4	234 CSF	19.35	17.35		\$12,649
03300-220	6000 psi concrete	253 CY	81			\$20,478
03310-700	Placing concrete	253 CY		13.1	5.35	\$4,664
05120-260	Curb Edging	718 LF	14	4.95	0.33	\$17,397
	<b>Total</b>					<b>\$98,171</b>
Structural Steel						
05120-680	Offices over 15-stories	107 TON	1900	345	109	\$251,878
05090-840	3/4" dia Shear Studs	27352	0.49	0.67	0.28	\$57,713
	<b>Total</b>					<b>\$309,591</b>
Frames						
05120-680	Columns, Beams, and Braces	50 TON	1900	345	109	\$117,700
Fireproofing						
07800-600	Decking	22000 SF	0.62	0.54	0.09	\$51,260
	Beams	17295 SF	0.41	0.45	0.07	\$31,650
	Columns	3506 SF	0.47	0.62	0.1	\$8,521
	<b>Total</b>					<b>\$91,430</b>
					<b>TOTAL</b>	<b>\$616,892</b>
					<b>Cost/sf</b>	<b>\$26</b>

























500 Delaware Ave.