# American Eagle Outfitters Quantum II Corporate Headquarters



Technical Report #2: Pro-Con Structural Study Of Alternative Floor System

# **Michael Sandretto**

Structural Option 27 October 2006 Advisor: Dr. Memari

## **Executive Summary**

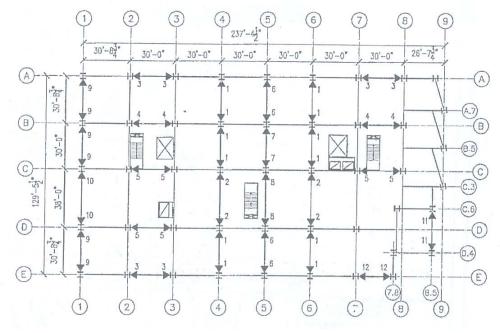
This report is a detailed analysis and comparison of various floor systems that could be utilized in the American Eagle Quantum II Corporate Headquarters. The first part of the report studies the existing design. Typical floor loads are defined per ASCE-7 02 and the buildings design. A typical framing bay is defined and analyzed, both manually and with RAM structural design software

The second and third sections of this report deal with alternative floor systems. The first investigates two more options in steel, non-composite beams and non-composite joists. The later section looks at the options provided by concrete floor systems. Hollow core planks and double tee beams are considered and designed with the use of manufacturer's charts. A design summary is presented for each of the four methods in the body of the report, while specific calculations are located in the appendix. Inherent strengths and weaknesses of each system are also discussed.

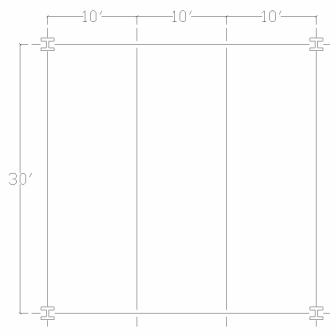
The final section is a comparison chart of all five floor systems. The ultimate aim of the report is to determine which system options are worthy of further consideration, and it is determined that the existing system of composite steel beams and the option of hollow core concrete planks are the most advantageous, and will be considered in further design work.

### Existing System

The structure consists of 6 floors. Each level is approximately 31,000 square feet and consists mostly of office space, with a large cafeteria on the top floor. Each deck is made of a composite steel system, where 3" of 4 ksi strength concrete lays on top of a 3" 20 gauge steel deck. Steel studs <sup>3</sup>/<sub>4</sub>" in diameter and 4 <sup>1</sup>/<sub>2</sub>" long are used to create composite action between the beams and the deck. A copy of a standard floor framing plan is shown below.



The plan is dominated by three rows of bays measuring 30' x 30' and one row measuring 30' x 38'. All bays contain two beams spaced 10' apart spanning parallel to the 38' long side of the larger bays. For the purpose of the analyses herein the 30' x 30' bay, shown below, was considered being that it dominated the vast majority of the floor plan.



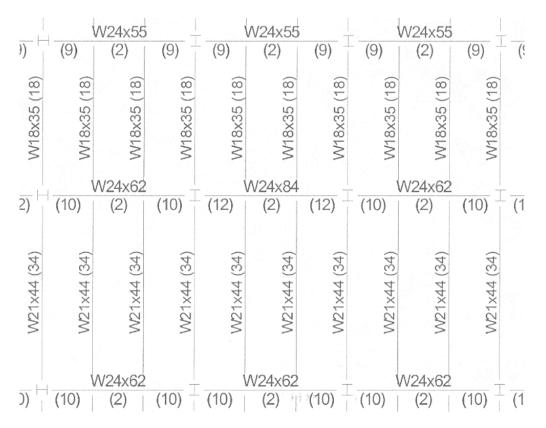
## **Floor Loads**

The structure was designed without a known tenant or floor plan. To prepare for various fit-outs the following loads are applied to the entire floor to ensure a conservative design.

- Live Load = 100 psf
- Metal Deck + Conc. Slab = 57 psf
- Miscellaneous Deal Load = 20 psf (ceilings, mechanical, etc.)

## Analysis

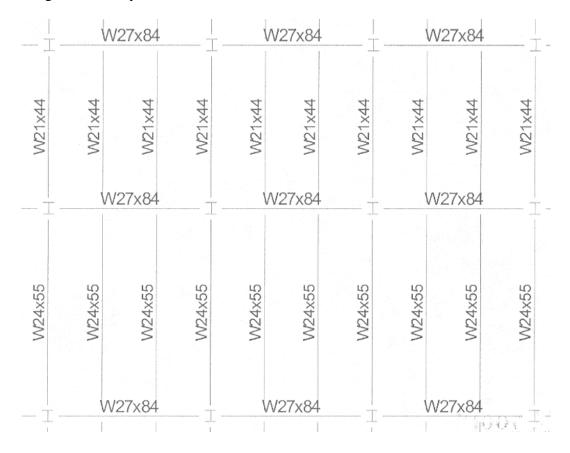
The existing floor system was analyzed by manual calculation and also with RAM structural design software. Both verified the structures design as adequate. The manual calculations are located in appendix B, while the Ram design, of both long and short bays, is shown below.



## Alternative Steel Systems

## **Composite Decking – Noncomposite Beams**

Often times steel framing is used without composite beams. This method can save time and money because the materials and manpower to attach the two systems is eliminated. In this example the same decking as in the existing system was utilized. The new system was modeled and analyzed using RAM, the design is shown below. As expected without utilizing composite action between the beams and deck the beam sizes must be larger to resist the load. This must be weighed against installation cost when deciding on a floor system.



## **Composite Decking – Steel Joists**

Another way to utilize steel is with a steel joist system. Steels joists are very light weight and east to install. Not as strong as conventional steel beams, joists must be placed closer together to decrease the tributary are they support and therefore their load. Steel Joists are also deeper then beams and are more expensive to fireproof. The same decking as used in the existing design was used here. Again, RAM was utilized to perform an analysis of this design method, a layout of the results are shown below.

   	1941	1	N27	′x84					W27	′x84				1	N27	′x84		
W16x31	24LH09	24LH09	24LH09	24LH09	24LH09	W16x31	24LH09	24LH09	24LH09	24LH09	24LH09	W16x31	24LH09	24LH09	24LH09	24LH09	24LH09	W16x31
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W21x44	28LH12	28LH12	28LH12	28LH12	28LH12	W21x44	28LH12	28LH12	28LH12	28LH12	28LH12	W21x44	28LH12	28LH12	28LH12	28LH12	28LH12	W21x44
	Terra and a second	V	N27	x84					N27	x84					N27	x84		

## **Steel Cost**

The following breaks down the cost of spanning members for one bay of a steel system. Costs were taken from RS Means and are shown in appendix E with calculations.

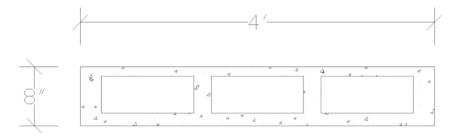
Existing System = \$2,850 Non-composite Beam = \$3,450 Steel Joist = \$3,525

## **Alternative Concrete Systems**

Concrete provides many options for spanning bays. Various self supporting floor slabs are available that can rest on steel members and span farther and hold more load than steel deck due to their utilization of pre-stressing. These slab systems come prefabricated and are easy to install. Also, bring made off site higher concrete strengths can be obtained. Finally, these systems save money on fireproofing due to the fire resistant nature of concrete.

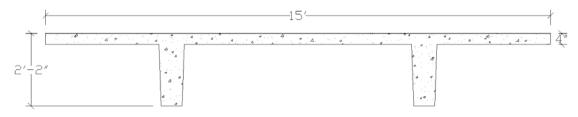
## **Hollow Core Concrete Planks**

The first concrete system considered is hollow core planks. Apart from advantages brought with concrete hollow core planks often have shallow depths. In order for this system to feasibly carry the load the span must be decreased. One girder must run vertically in the middle of the bay. The planks will rest on the steel girders and span the two 15' spans horizontally across the bays. Design tables obtained from Nitterhouse Concrete Products, Inc. were utilized to select the proper size. The 8" x 4' – U.L. – J952, with no topping, and strand pattern  $4 - \frac{1}{2}$ " was selected. This system has a concrete strength specified as 5 ksi, and a self weight of 57.5 psf, which is very comparable to the composite deck used in the steel systems.



## **Concrete Double Tee Beams**

Double tee beams are excellent at creating a floor slab that can span long distances. Unfortunately they are often very deep, increasing floor depth. Design charts obtained from High Concrete Structures, Inc. were used to select an appropriate size. The 15DT26 with strand pattern 128-S was chosen. This system has a concrete strength specified as 6 ksi, and a self weight of 75 psf, which is significantly greater then the composite deck used in the steel systems.



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System	Depth	Weight	Installation	Fireproofing	Cost	Further
	(in)	(psf)	5 = hardest	5 = hardest	(\$/sf)	Consideration
Existing	23.7	57	5	4	17.80	Yes
Non-Comp. Beams	26.7	57	4	4	24.75	No
Steel Joist	24	57	3	5	19.15	No
Hollow Core Plank	8	57	1	1	8.53	Yes
Double Tee Beam	22	75	2	1	9.30	No

<u>Comparison</u> The Following chart is designed to summarize and compare the pros and cons of each system, and states whether further consideration is planned.

## **Appendix A: References**

High Concrete Structures, Inc. Double Tee Beam Design Chart

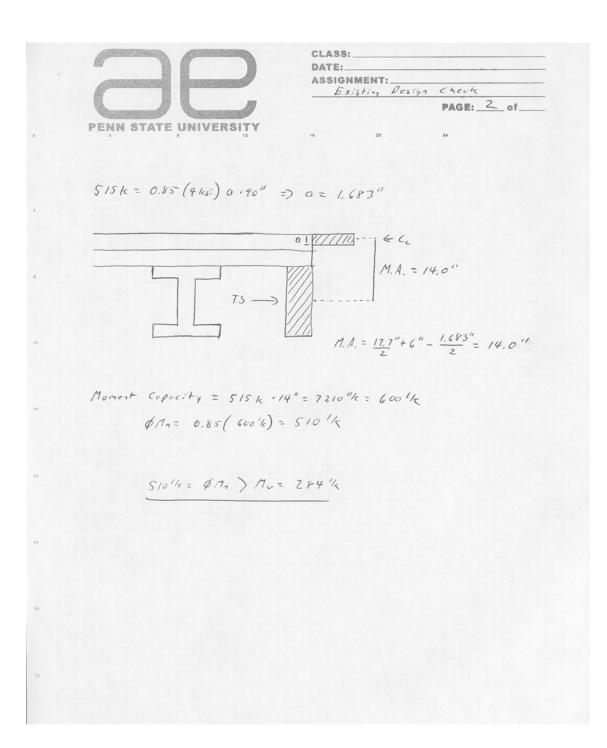
LRFD Manual of Steel Construction, Third Edition

Nitterhouse Concrete Products, Inc. Hollow Core Plank Design Chart

RS Means Assemblies and Cost Data, 2006 edition

Vulcraft

Steel Roof and Floor Deck, 2001 Edition

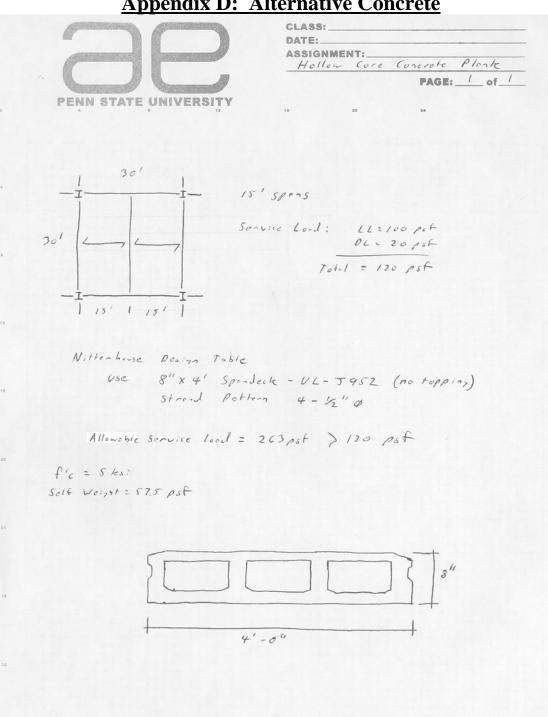


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# Appendix C: Alternative Steel

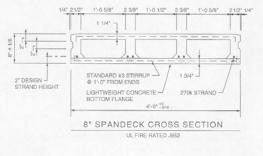
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be	W21x55	24LH09	N27x84	4FH06	N27x84		28LH12	N27x84	60H	
Ty	5	24LH09	5	60H77			28CH12	3	60H-	
Floor Type: TYP	-	24LH09		60H7+			28LH12		60H-	
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**Appendix D:** Alternative Concrete

## **Prestressed Concrete** 8" x 4' SpanDeck - U.L. - J952 (NO TOPPING)

		PHYSICAL P Prec		ER	TIES
A	=	199 in.2	Sb	=	332 in. <sup>3</sup>
1	=	1370 in.4	St	=	354 in. <sup>3</sup>
Yb	=	4.13 in.	Wt.	=	230 PLF
Yt	=	3.87 in.	Wt.	=	57.5 PSF
е	=	2.13 in.			



### DESIGN DATA

- 1. Precast Strength @ 28 days = 5000 PSI.
- 2. Precast Strength @ release = 3000 PSI.
- 3. Precast Density = 150 PCF (Top and Webs) = 115 PCF (Soffit)
- 4. Strand = 1/2"ø, 270 K Lo-Relaxation.
   5. Strand Height = 2.00 in.
- 6. Ultimate moment capacities (when fully developed) . . . 4-1/2"ø, 270K = 68.0'K
  - 6-1/2"ø, 270K = 96.3'K
- 7. Maximum bottom tensile stress is  $6\sqrt{fc} = 424$  PSI.
- 8. All superimposed load is treated as live load in the strength analysis of flexure and shear.
- 9. Flexural strength capacity is based on stress/strain strand relationships.
- 10. Shear values are the maximum allowable before shear reinforcement is required.
- 11. Deflection limits were not considered when determining allowable loads in this table.
- 12. All values in this table are based on ultimate strength and are not governed by service stress.

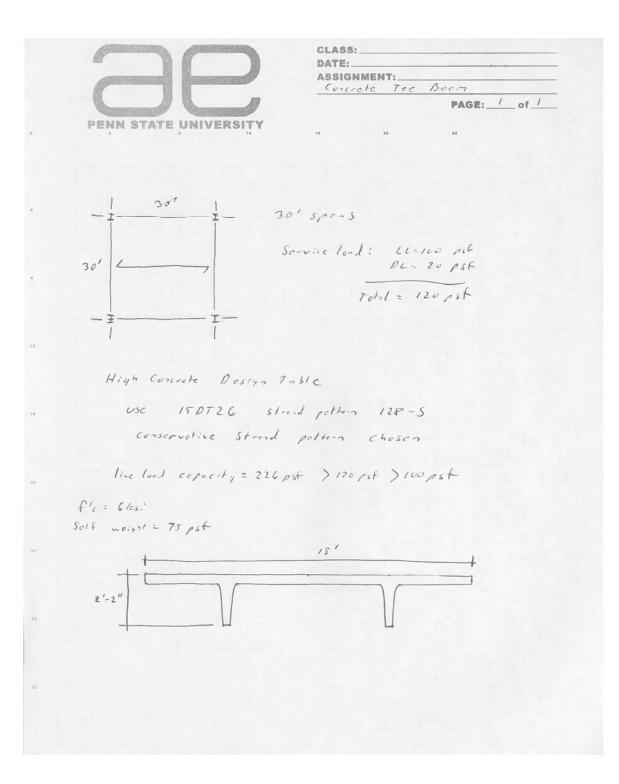
			8" SP	ANDE	CK V	V/O 1	OPP	PING				A	ALLO	WA	BLE	SUP	ERIM	POS	ED L	OAD	(PS	F)				
STRAN		ATT	EDN											SPA	N (F	EET)										
STRAN	DF		LINK	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
Flexure	4	-	1/2"ø	565	510	460	420	361	309	265	231	199	175	152	133	118	105	91	80	71	62	54	47	41	35	
Shear	4	-	1/2"ø	429	383	345	313	286	263	241	225	209	195	177	159	143	130	118	110	104	95	88	79	72	66	$\overline{V}$
Flexure	6	-	1/2"ø	825	745	675	619	531	456	395	344	302	265	236	209	186	167	149	134	120	107	96	86	78	70	6
Shear	6	-	1/2"ø	446	398	359	326	298	274	253	234	218	204	191	179	169	159	150	138	126	115	106	97	89	82	7



This table is for simple spans and uniform loads. Design data for any of these span-load conditions is available on request. Individual designs may be furnished to satisfy unusual conditions of heavy loads, concentrated loads, cantilevers, flange or stem openings and narrow widths.

2655 Molly Pitcher Hwy. South, Box N Chambersburg, PA 17201-0813 717-267-4505 • FAX: 717-267-4518

REVISED 12/93



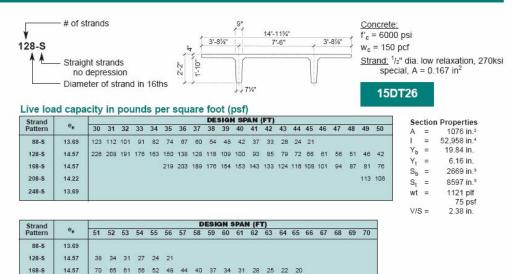


208-S

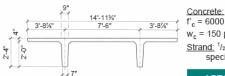
248-S

14.22

13.69



99 93 88 82 77 72 67 63 59 55 51 47 44 41 38 35 32 29 26 24



78 73 69 65 61 57 53 50 47 43 40 38

f'<sub>c</sub> = 6000 psi  $w_c = 150 \text{ pcf}$ Strand: 1/2" dia. low relaxation, 270ksi special, A = 0.167 in<sup>2</sup>

15DT28

### Live load capacity in pounds per square foot (psf)

Strand										DE	51QI	N SP	AN	(FT)									6	er	tio	n Properties
Pattern	ee	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	Ā		=	1104 in. <sup>2</sup>
88-S	15.17	141	128	116	105	96	87	78	71	64	57	52	46	41	36	32	27	24	20				I		=	64,938 in.4
128-S	16.05	253	233	215	198	183	169	156	145	134	124	115	106	98	91	84	77	71	66	60	55	51	Y	b	=	21.30 in.
	40.05									400													Y	ł.	=	6.70 in.
168-S	16.05						245	228	212	198	185	173	101	151	141	132	123	115	108	101	94	88	s	h	=	3049 in. <sup>3</sup>
208-S	15.70																				129	121	s	ĩ	=	9692 in. <sup>3</sup>
248-S	15.17																							۰.	=	1150 plf
																										77 nof

A	=	1104 in. <sup>2</sup>
1	=	64,938 in.4
Υ <sub>b</sub>	=	21.30 in.
Υt	=	6.70 in.
Sb	=	3049 in.3
St	=	9692 in.3
wt	=	1150 plf
		77 psf
V/S	5 =	2.40 in.

Strand									D	ESK	an s	PAN	I (F1	r)							
Pattern	ee	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70
88-S	15.17																				
128-S	16.05	46	42	38	34	31	28	24	21												
168-S	16.05	82	76	71	66	62	57	53	49	45	42	38	35	32	29	26	23	21			
208-S	15.70	114	107	101	95	89	84	79	74	69	65	61	57	53	49	46	43	40	37	34	31
248-S	15.17										86	81	76	72	68	64	60	56	53	50	46

Ų	05	100   Structural Metal Framin	9								
I	05	120 Structural Steel	0051	DAILY	LABOR-	UNIT	MAT.	2006 BAR	EQUIP.	TOTAL	TOTAL INCL 08P
t	2350	1" thick	_	UUIPUI	HUUNS	Cwt.	40	LADUN	EQUIT.	40	44 8 640
Т	2400	1" thick	23				41.50	2.37	betering t	41.50	45.50
ь.	2450	4" thick		1 117			43.50		1.20	43.50	48
	2500	6" thick					46			46	50.50
н.	2550	8" thick	*			*	46			46	50.50
ļ				-							
	0010	STRESSED SKIN ROOF & CEILING SYSTEM Double panel flat roof, spans to 100'	E-2	1150	.049	S.F.	7.60	1.89	1.24	10.73	13
	0100	Double panel convex roof, spans to 200'		960	.058		12.35	2.27	1.49	16.11	19.15
	0200	Double panel arched roof, spans to 200		760	.074		19	2.87	1.88	23.75	28
				1.00	1071	- ×					R.
Т	0020	Structural steel MEMBERS Shop fab'd for 100-ton, 1-2 story project, bolted conn's.	23	1 8 0							1.00
	0100	W 6 x 9	E-2	600	.093	L.F.	9.40	3.63	2.38	15.41	19.20
	0120	x 16		600	.093		16.70	3.63	2.38	22.71	27.50
	0140	x 20		600	.093		21	3.63	2.38	27.01	32
	0300	W 8 x 10		600	.093		10.45	3.63	2.38	16.46	20.50
	0320	x 15		600	.093		15.70	3.63	2.38	21.71	26
	0350	x 21		600	.093		22	3.63	2.38	28.01	33
ł	0360	x 24		550	.102		- 25	3.96	2.59	31.55	37
	0370	x 28	2	550	.102		29.50	3.96	2.59	36.05	41.50
	0500	x 31		550	.102		32.50	, 3.96	2.59	39.05	45
	0520	x 35		550	.102		36.50	3.96	2.59	43.05	49.50
	0540	x 48		550	.102		50	3.96	2.59	56.55	64.50
	0600	W 10 x 12		600	.093		12.55	3.63	2.38	18.56	22.50
	0620	x 15		600	.093		15.70	3.63	2.38	21.71	26
	0700	x 22		600			23	3.63	2.38	29.01	34.50
	0720	x 26		600			27	3.63	2.38	33.01	39
	0740	x 33		550			34.50	3.96	2.59	41.05	47.50
	0900	x 49		550			51	3.96	2.59	57.55	66
	1100	W 12 x 14		880	_		14.65	2.48	1.62	18.75	22
	1300	x 22	1111	880			23	2.48	1.62	27.10	31.50
	1500	x 26		880			27	2.48	1.62	31.10	36
	1520	x 35		810		1 I.	36.50	2.69	1.76	40.95	46.50
	1560	x 50		750	-		52.50	2.90	1.90	57.30 65.30	64.50
	1580	x 58		750			60.50	2.90	1.90	65.30 80.63	73.50 91.50
	1700	x 72		640	_		75	3.40	2.23	96.63	108
	1740	x 87		640			91 27	3.40 2.20	2.23 1.44	96.63 30.64	35.50
	1900	W 14 x 26		990			31.50	2.20	1.44	30.64	40.50
	2100	x 30		810			35.50	2.42	1.59	39.95	45.50
	2300	x 34		810			45	2.69	1.76	49.45	56
	2320 2340			800			55.50			60	67.50
	2340			760	_		77.50		1.88	82.25	92
	2360			740			94	2.94	1.93	98.87	110
	2500			740			125	3.03	1.98	130.01	145
	2700			100			27	2.18	1.43	30.61	35.50
	2900			- 900			32.50	2.42	1.59	36.51	41.50
	3100			800			42	2.72		46.50	52.50
	3120			800			52.50			57	64
	3140			760			70	2.87		74.75	84
	3300		E				36.50			41.36	47.50
	3500			96			42	3.28		46.86	53.50
	3520			96	_		48	3.28		52.86	60.50
	3700			91			52.50			57.62	
	3900			91	_		57.50			62.62	71
	392			90			68	3.50		73.18	82.50

## Appendix E: Cost & Pricing

148 Important: See the Reference Section for supporting data - Crews, Rental Equipment, City Cost Indexes and Reference Dat

0512	0 Structural Steel			DAILY	LABOR			2006 BAR	RE COSTS		TOTAL
	o   Structural Steel		CREV		THOUR		MAT.	LABOR	EQUIP.	TOTAL	INCL 0&P
940	x 76	R051223	E-5		.089	L.F.	79.50	3.50	1.68	84.68	95.
960	x 86	-10		900	.089		90	3.50	1.68	95.18	107
980	x 106	105-12		900	.089		111	3.50	1.68	116.18	130
	W 21 x 44	1.1.1.1		1064	.075		46	2.96	1.42	50.38	57.
300	x 50			1064	.075		52.50	2.96	1.42	56.88	64.
	x 62			1036	.077		65	3.04	1.46	69.50	78.
1700	x 68			1036	.077		71	3.04	1.46	75.50	85
	x 83			1000	.080		86.50	3.15	1.52	91.17	103
1740	x 93	1.11		1000	.080		97	3.15	1.52	101.67	114
1760	x 101	104		1000	.080		106	3.15	1.52	110.67	123
1780	x 122	1		1000	-		127	3.15	1.52	131.67	147
	W 24 x 55			1110			57.50	2.84	1.37	61.71	69.
5100	x 62			1110	.072		65	2.84	1.37	69.21	78
	x 68			1110			71	2.84	1.37	75.21	84.
500	x 76			1110			79.50	2.84	1.37	83.71	94
	x 84			1080			88	2.92	1.40	92.32	103
720	x 94			1080	.074		98	2.92	1.40	102.32	105
740	x 104			1050			109	3	1.40	102.32	115
5760	x 117			1050	.076		105	3	1.44	115.44	127
	x 146			1050	.076		153	3	1.44	120.44	141
800	W 27 x 84			1190	.070		88	2.65	1.44	91.92	1/5
900	x 94			1190			98	2.65	1.27	101.92	
920	x 114			1150	.007		119	2.00	1.27		114
940	x 146			1150			153	2.74	1.32	123.06	137
960	x 161		++	1150	.070		153	2.74	1.32	157.06	174
	W 30 x 99			1200	.070		108			172.06	191
300	x 108		+	1200	.067		103	2.63	1.26	106.89	120
	x 116			1200	.067			2.63	1.26	116.89	130
520	x 132			1160	.069		121	2.72	1.31	125.03	139
5540	x 148	1.10		1160	.069			2.72	1.31	142.03	158
1560	x 173		++	1100	.069		155 181	2.72	1.31	159.03	176
	× 191			1120	.071				1.35	185.17	205
6700	W 33 x 118			1120			200	2.82	1.35	204.17	226
	x 130			1176	.068		123	2.68	1.29	126.97	142
7100	x 150 x 141		$\vdash$		.071		136	2.78	1.34	140.12	155
	× 169			1134	.071		147	2.78	1.34	151.12	168
7143	x 201		$\vdash$	1100	.073		177	2.87	1.38	181.25	201
	W 36 x 135			1100	.073		210	2.87	1.38	214.25	238
7500	x 150		$\vdash$	1170	.068		141	2.70	1.30	145	161
	x 150 x 170			1170	.068		157	2.70	1.30	161	178
7700	× 194		$\vdash$	1150	.070		178	2.74	1.32	182.06	201
	x 230			1125	.071		203	2.80	1.35	207.15	229
7920	x 260		$\vdash$	1125	.071		240	2.80	1.35	244.15	270
	x 300			1035			272	3.05	1.46	276.51	305
8490	For projects 75 to 99 tons, add			1030	.077		315	3.05	1.46	319.51	350
	50 to 74 tons, add	1.1					10%	200	101 to 380	0.000	
894	25 to 49 tons, add		-		-		20%	1.004			0
8496	10 to 24 tons, add			100			30%	10%	0.00	100.000	
8498	2 to 9 tons, add	1 101 1	-	-	11		50%	25%	alter Marke	2646.046352	0
	Less than 2 tons, add			1.1.			75%	50%	100	100	
-	RUCTURAL STEEL PROJECTS		-	-		V I	100% .	100%	102 million	den salah	
120		R050516 -30	10	1.1						1.0	
	Shop fab'd for 100-ton, 1-2 story project, bolted conn's.	-30		10.07					5.2001 82 p	010105-25	3 (d
	Apartments, nursing homes, etc., 1 to 2 stories	R050523	E-5	10.30		Ton	1,900	305	147	2,352	2,800
0800	3 to 6 stories	-10	1	10.10			1,950	310	150	2,410	2,825
3400	7 to 15 stories	R051223	E-6	14.20	9.014		1,975	355	115	2,445	2,925
1500	Over 15 stories	-10	1	13.90	9.209	141	2,050	365	118	2,533	3,025

05	210 Steel Joists			DAILY	LABOR			2006 BA	RE COSTS		T
		S DATE ME	CRE	N OUTPL	T HOURS	UNIT	MAT.	LABOR	EOUIP.	TOTAL	INC
600 0160	12K3, 5.7 Lb/LF		E-7	1500	.053	L.F.	3.76	2.10	1.07	6.93	
0180	14K3, 6.0 Lb/LF	5, o / 11300705		1500	.053		3.96	2.10	1.07	7.13	
0200	16K3, 6.3 Lb/LF	8.81		1800	.044		4.16	1.75	.89	6.80	-
0220	16K6, 8.1 Lb/LF	02.85,		1800	.044		5.35	1.75	.89	7.99	
0240	18K5, 7.7 Lb/LF	15.35		2000	.040		5.10	1.58	.80	7.48	-
0260	18K9, 10.2 Lb/LF	08.30		2000	.040	I + I	6.75	1.58	.80	9.13	
0410	Span 30' to 50', minimum	6 1610		17	4.706	Ton	1,150	186	94.50	1.430.50	
0440	Average	CN		17	4.706	100	1,300	186	94.50	1,580.50	1333
0460	Maximum	10181 I I I I B		10	8	+	1,375	315	161	1.851	1
0500	20K5, 8.2 Lb/LF	JELSE /		2000	.040	LE	5.35	1.58	.80	7.73	l '
0520	20K9, 10.8 Lb/LF			2000	.040		7	1.58	.80	9.38	-
0540	22K5, 8.8 Lb/LF	- Carallel		2000	.040		5.70	1.58	.80	8.08	
0560	22K9, 11.3 Lb/LF			2000	.040		7.35	1.58	.80	9.73	
0580	24K6, 9.7 Lb/LF			2200	.036		6.30	1.43	.73	9.73	
0600	24K10, 13.1 Lb/LF			2200	.036		8.50	1.43	.73		
0620	26K6, 10.6 Lb/LF			2200	.036		6.90	1.43		10.66	
0640	26K10, 13.8 Lb/LF			2200	.036	$\vdash$	8.95	1.43	.73	9.06	
0660	28K8, 12.7 Lb/LF			2400	.033		8.25	1.43	.73	11.11	
0680	28K12, 17.1 Lb/LF			2400	.033		11.10	1.31	.67	10.23	
0700	30K8, 13.2 Lb/LF			2400	.033				.67	13.08	
0720	30K12, 17.6 Lb/LF		+	2400	.033		8.60	1.31	.67	10.58	
1010	CS series, horizontal bridging			2400	.055	*	11.45	1.31	.67	13.43	
1020	Spans to 30', minimum		E-7	15	5.333	Ton	1.005	010	3.0.1.52	11010	
1040	Average		1	12	6.667	Ion	1,225	210	107	1,542	1
1060	Maximum			9	8.889		1,350	263	134	1,747	2
1100	10CS2, 7.5 Lb/LF			1200		*	1,600	350	178	2,128	2
1120	12CS2, 8.0 Lb/LF		-	1200	.067	L.F.	5.10	2.63	1.34	9.07	
1140	14CS2, 8.0Lb/LF						5.40	2.10	1.07	8.57	
1160	16CS2, 8.5 Lb/LF		-	1500	.053	_	5.40	2.10	1.07	8.57	
1180	16CS4, 14.5 Lb/LF		1	1800	.044		5.75	1.75	.89	8.39	
1200	18CS2, 9.0 Lb/LF		-	1800	.044		9.80	1.75	.89	12.44	
1220	18CS4, 15.0 Lb/LF			2000	.040		6.10	1.58	.80	8.48	
1240	20CS2, 9.5 Lb/LF		-	2000	.040		10.15	1.58	.80	12.53	
1260	20CS4, 16.5 Lb/LF			2000	.040		6.45	1.58	.80	8.83	
1280	- 220034, 10.5 Lb/LF			2000	.040		11.15	1.58	.80	13.53	
1300	22CS2, 10.0 Lb/LF 22CS4, 16.5 Lb/LF		1	2000	.040		6.75	1.58	.80	9.13	
1320	24CS2, 10.0 Lb/LF			2000	.040		11.15	1.58	.80	13.53	
1340				2200	.036		6.75	1.43	.73	8.91	
1360	24CS4, 16.5 Lb/LF 26CS2, 10.0 Lb/LF			2200	.036		11.15	1.43	.73	13.31	
1380				2200	.036		6.75	1.43	.73	8.91	-
1380	26CS4, 16.5 Lb/LF		- 00	2200	.036		11.15	1.43	.73	13.31	
1400	. 28CS2, 10.5 Lb/LF		100	2400	.033		7.10	1.31	.67	9.08	
1420	28CS4, 16.5 Lb/LF	10 million (1997)		2400	.033		11.15	1.31	.67	13.13	
1460	30CS2, 11.0 Lb/LF			2400	.033		7.45	1.31	.67	9.43	
2000	30CS4, 16.5 Lb/LF		*	2400	.033	*	11.15	1.31	.67	13.13	
2020	LH series, bolted cross bridging	5-65 - 1 - F									
2020	Spans to 96', minimum	1.02	E-7	16	5	Ton	1,325	197	100	1,622	1,9
	Average			13	6.154		1,450	243	124	1,817	2,1
2080	Maximum	102		11	7.273	↓	1,725	287	146	2,158	2,5
2200	18LH04, 12 Lb/LF			1400	.057	L.F.	8.75	2.25	1.15	12.15	210
2220	18LH08, 19 Lb/LF	100		1400	.057		13.90	2.25	1.15	17.30	
2240	20LH04, 12 Lb/LF			1400	.057		8.75	2.25	1.15	12.15	-
2260	20LH08, 19 Lb/LF	22.35		1400	.057		13.90	2.25	1.15	17.30	
2280	24LH05, 13 Lb/LF	1 3351 1 1 1 1 2 2		1400	.057		9.50	2.25	1.15	17.30	_
2300	24LH10, 23 Lb/LF	10 COL 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1400	.057		16.80	2.25	1.15	20.20	
	28LH06, 16 Lb/LF	10.000.0		1800	.044	++-	11.70	1.75	.89	14.34	
2340	28LH11; 25 Lb/LF	27288 av		1800	.044		18.25	1.75	.89	20.89	

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20	CLASS: DATE: ASSIGNMENT: Steel Price (Bey
PENN STATE UNIVERSITY	PAGE: / of /

Existing  

$$W = 18 \times 35^{-} = \frac{47.5}{47.5} = \frac{47.5}{47.5} + \frac{2500}{500} = \frac{42.850.160}{100}$$

Noncomposite - Beam  

$$w 21x44 = \frac{$157.5/$}{$57.5/$}$$
  
 $\frac{$157.5}{$f_i} \cdot \frac{30f_i}{$sp_n} \cdot \frac{25p_n}{$box} = $13,450/$box$ 

## **B10 Superstructure**

35

8.35

Idex

## **B1010 Floor Construction**

	/				
A		TA		1.4	
				AS S	
				Ð	
	T		T		
	6	19			
	200	/			

Description: Table below lists costs (\$/S.F.) for a floor system using composite steel beams with welded shear studs, composite steel deck, and light weight concrete slab reinforced with W.W.F. Price includes sprayed fiber fireproofing on steel beams. Design and Pricing Assumptions:

Design and Pricing Assumptions: Structural steel is A36, high strength bolted. Composite steel deck varies from

22 gauge to 16 gauge, galvanized.

Shear Studs are 3/4''. W.W.F.,  $6 \times 6 - W1.4 \times W1.4$  (10 x 10) Concrete f'c = 3 KSI, lightweight. Steel trowel finish and cure. Fireproofing is sprayed fiber (nonasbestos).

Spandrels are assumed the same as interior beams and girders to allow for exterior wall loads and bracing or moment connections.

em Components			(	COST PER S.F.	
components	QUANTITY	UNIT	MAT.	INST.	TOTAL
SYSTEM B1010 256 2400					
20X25 BAY, 40 PSF S. LOAD, 5-1/2" SLAB, 17-1/2" TOTAL THICKNESS					
Structural steel	4.320	Lb.	4.62	1.52	6.14
Welded shear connectors 3/4" diameter 4-7/8" long	.163	Ea.	.10	.26	.36
Metal decking, non-cellular composite, galv. 3" deep, 22 gauge	1.050	S.F.	1.76	.80	2.56
Sheet metal edge closure form, 12", w/2 bends, 18 ga, galv	.045	L.F.	.15	.09	.24
Welded wire fabric rolls, 6 x 6 - W1.4 x W1.4 (10 x 10), 21 lb/csf	1.000	S.F.	.13	.30	.43
Concrete ready mix, light weight, 3,000 PSI	.333	C.F.	2.23		2.23
Place and vibrate concrete, elevated slab less than 6", pumped	.333	C.F.		.42	.42
Finishing floor, monolithic steel trowel finish for finish floor	1.000	S.F.		.74	.74
Curing with sprayed membrane curing compound	.010	C.S.F.	.06	.07	.13
Shores, erect and strip vertical to 10' high	.020	Ea.		.34	.34
Sprayed mineral fiber/cement for fireproof, 1" thick on beams	.483	S.F.	.23	.38	.61
TOTAL			9.28	4.92	14.20

B101	0 256		Composi	te Beams, I	eck & Slab			
	BAY SIZE	SUPERIMPOSED	SLAB THICKNESS	TOTAL DEPTH	TOTAL LOAD	C	OST PER S.F.	
	(FT.)	LOAD (P.S.F.)	(IN.)	(FTIN.)	(P.S.F.)	MAT.	INST.	TOTAL
2400	20x25	40	5-1/2	1 - 5-1/2	80	9.30	4.91	14.
2500	RB1010	75	5-1/2	1 - 9-1/2	115	9.65	4.92	14.
2750	-100	125	5-1/2	1 - 9-1/2	167	11.75	5.75	17.
2900		200	6-1/4	1 - 11-1/2	251	13.25	6.20	19.
3000	25x25	40	5-1/2	1 - 9-1/2	82	9.15	4.68	13.
3100		75	5-1/2	1 - 11-1/2	118	10.15	4.75	14.
3200		125	5-1/2	2 - 2-1/2	169	10.60	5.15	15.
3300		200	6-1/4	2 - 6-1/4	252	14.30	6	20.
3400	25x30	40	5-1/2	1 - 11-1/2	83	9.35	4.65	14
3600		75	5-1/2	1 - 11-1/2	119	10.05	4.70	14.
3900		125	5-1/2	1 - 11-1/2	170	11.60	5.30	16.
4000		200	6-1/4	2 - 6-1/4	252	14.35	6	20.
4200	30x30	40	5-1/2	1 - 11-1/2	81	9.40	4.79	14.
4400		75	5-1/2 .	2 - 2-1/2	116	10.10	5	15.
4500		125	5-1/2	2 - 5-1/2	168	12.20	5.60	17.
4700		200	6-1/4	2 - 9-1/4	252	14.60	6.50	21.
4900	30x35	40	5-1/2	2 - 2-1/2	82	9.80	4.95	14.
5100		75	5-1/2	2 - 5-1/2	117	10.70	5.05	15.
5300		125	5-1/2	2 - 5-1/2	169	12.55	5.75	18.
5500		200	6-1/4	2 - 9-1/4	254	14.75	6.50	21.
5750	35x35	40	5-1/2	2 - 5-1/2	84	10.45	4.98	15.
6000		75	5-1/2	2 - 5-1/2	121	11.90	5.30	17

# B10 Superstructure

10	10 254			W Shape,	Composite	Deck, & Sl	ab			
	BAY SIZE (F BEAM X GI	T.)	SUPERIMPOSED LOAD (P.S.F.)	SLAB THICKNESS (IN.)	TOTAL DEPTH (FTIN.)	TOTAL LOAD (P.S.F.)		OST PER S.F.		
100		10					MAT.	INST.	TOTAL	
400	25x30		40	5	2-5	91	10.95 13.25	6 6.70	16.95 19.95	
500			75 125	5	2-5 2-8	128 180				
500							15.05	7.40	22.45	
700	00.05		200	5	2-11	259	18.75	8.55	27.30	
800	30x25	100	40	diono <mark>5</mark> e dove d	2.5	92	11.60	6.30	17.90	
900			75	5	2-5 belied	129	13.65	7	20.65	
000			125	5	2-8	181	15.55	7.70	23.25	
100			200	5-1/2	2-11	200	18.95	8.90	27.85	
200	30x30		40	5	2-2	92	12.10	6.40	18.50	
300			75	5 .	2-5	129	14.15	7.10	21.25	
400			125	5	2-11	182	16.75	8	24.75	
500		· ·	200	5	3-2	263	22.50	10.10	32.60	
600	30x35		40	5	2-5	94	13.20	6.80	20	-
700			75	5	2-11	131	15.35	7.50	22.85	
800			125	5	3-2	183	. 18	8.40	26.40	
900			200	5-1/2	3-5-1/2	268	22	9.70	31.70	
400	35x30		40	5	2-5	93	12.75	6.65	19.40	
500	00,00		75	5	2-8	130	15.20	7.50	22.70	
600			125	5	2.11	183	18.05	8.50	26.55	
700			200	5	3-5	262	22	9.90	31.90	-
	2525		40		2-8	94				
800	35x35			5			13.55	6.75	20.30	
900			75	5	2.11	131	15.75	7.55	23.30	
000			125	5	3-5	184	18.85	8.65	27.50	
100		1.1.1	200	5-1/2	3-5-1/2	270	24.50	10.20	34.70	
200	35x40		40	5	2-11	94	14.15	7.10	21.25	
300			75	5	3-2	131	16.40	7.95	24.35	
400			125	5	3-5	184	19.40	8.95	28.35	
500			200	5	3-5-1/2	264	24.50	10.75	35.25	
1.1.1	12/1	TAM	(3.2.5)	1000	11	[325] 0401	0.91	BEAM X C		
										-
								15.25		1
										-

	C	A COLUMN TO A		
10	 -11.	I H & Y	ructu	LI CE
		ALC .		

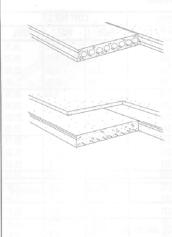
B101	0 250	secoled no S	teel Joists,	Beams & S	lab on Colu	ymns		
	BAY SIZE	SUPERIMPOSED	DEPTH	TOTAL LOAD	COLUMN		OST PER S.F.	
0.00	(FT.)	LOAD (P.S.F.)	(IN.)	(P.S.F.)	ADD	MAT.	INST.	TOTAL
3700	20x25	40	44	83	Linearly 99-0 sh	7.80	4.35	12.
3800	108	00000			column	.87	.29	1.
3900	20x25	65	26	110	depth Shd sp	8.50	4.61	13.
4000	00.05	75			column	.87	.29	1.
4100 4200	20x25	75	26	120		8.35	4.37	12.
4300	20x25	100	00	145	column	1.04	.35	1.
4400	ZUXZO	100	26	145	<ul> <li>Design Assu</li> </ul>	8.85	4.55	13.
4500	20x25	125	29	170	column	1.04	.35	1.
4600	LONED	125	23	170	column	9.90	4.95	14.
4700	25x25	40	23	84	column	1.21	.40 4.53	1.
4800	107110	40	20	04	column	.83	4.53	
4900	25x25	65	29	110	CONTINU	8.85	4.72	1.
5000	and the second s			110	column	.83	4.72	
5100	25x25	75	26	120	Column	9.25	4.67	1.
5200		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	27	120	column	.97	4.07	13.
5300	-25x25	100	29	145	Column	10.35	5.10	15.4
5400				140	column	.97	.32	15.
5500	25x25	125	32	170	column	10.90	5.30	16.2
5600				170	column	1.08	.36	10.
5700	25x30	40	29	84	ooranni	8.70	4.74	13.
5800					column	.81	.27	1.0
5900	25x30	65	29	110		9.05	4.93	13.9
6000					column	.81	.27	1.0
6050	25x30	75	29	120		9.80	4.45	14.2
6100					column	.89	.30	1.1
6150	25x30	100	29	145		10.60	4.71	15.3
6200					column	.89	.30	1.
6250	25x30	125	32	170		11.35	5.85	17.
6300					column	1.03	.35	1.
6350	30x30	40	29	84		9.10	4.25	13.
6400	0.2.3			and a second	column	.75	.25	1
6500	30x30	65	29	110		10.35	4.65	15
6600					column	.75	.25	1
6700	30x30	75	32	120	(Setting)	10.55	4.71	15.2
6800	2020	100	0.5		column	.86	.29	1.1
6900 7000	30x30	100	35	145		11.75	5.10	16.8
7100	30x30	105	25	170	column	1 .	.34	1.3
7200	30730	125	35	172	272	12.80	6.35	19.1
7300	- 30x35	40	29	00	column	· 1.11	.37	1.4
7400	50/30	40	23	85		10.30	4.61	14.9
7500	30x35	65	29	111	column	.64	.21	
7600	00000		<i>LJ</i>	111	column	11.45	5.85	17.3
7700	30x35	75	32	121	column	.83	.27 5.85	1.1
7800			UL.	161	column	11.45 .84	.28	17.3
7900	30x35	100	35	148	column	.84	5.25	1.1
8000				140	column	12.40	.35	17.8
8100	30x35	125	38	173	conditiit	1.05	5.70	1.3
8200					column	1.05	.35	19.0
8300	35x35	40	32	85	ovum	10.55	4.70	15.2
8400				~~	column	.74	4.70	10.2

dexes

see the Belorence Section for without supporting data - Robrouce Rumbers and City (

## **B10** Superstructure

## **B1010** Floor Construction



General: Units priced here are for plant produced prestressed members, transported to site and erected.	Description of Table: Enter table at span and load. Most economical sections will generally consist of normal weight
Normal weight concrete is most frequently used. Lightweight concrete may be used to reduce dead weight.	concrete without topping. If acceptable, note this price, depth and weight. For topping and/or lightweight concrete, note appropriate data.
Structural topping is sometimes used on floors: insulating concrete or rigid insulation on roofs.	Generally used on masonry and concrete bearing or reinforced concrete and steel framed structures.
Camber and deflection may limit use by depth considerations.	The solid 4" slabs are used for light loads
Prices are based upon 10,000 S.F. to 20,000 S.F. projects, and 50 mile to 100 mile transport.	and short spans. The 6" to 12" thick hollow core units are used for longer spans and heavier loads. Cores may carry utilities.
Concrete is f'c = 5 KSI and Steel is fy = 250 or 300 KSI	Topping is used structurally for loads or rigidity and architecturally to level or
Note: Deduct from prices 20% for	slope surface.
Southern states. Add to prices 10% for Western states.	Camber and deflection and change in direction of spans must be considered
	(door openings, etc.), especially untopped.

Sector Comments			Ç	OST PER S.F.	
System Components	QUANTITY	UNIT	MAT.	INST.	TOTAL
SYSTEM B1010 230 2000					
10' SPAN, 40 LBS S.F. WORKING LOAD, 2" TOPPING					
Precast prestressed concrete roof/floor slabs 4" thick, grouted	1.000	S.F.	4.88	2.75	7.6
Edge forms to 6" high on elevated slab, 4 uses	.100	L.F.	.02	.33	.3
Welded wire fabric 6 x 6 - W1.4 x W1.4 (10 x 10), 21 lb/csf, 10% lap	.010	C.S.F.	.13	.30	.4
Concrete ready mix, regular weight, 3000 psi	.170	C.F.	.60		.6
Place and vibrate concrete, elevated slab less than 6", pumped	.170	C.F.		.22	.2
Finishing floor, monolithic steel trowel finish for resilient tile	1.000	S.F.		.68	.6
Curing with sprayed membrane curing compound	.010	C.S.F.	.06	.07	.13
	11/2010		-		10
TOTAL			5.69	4.35	10.0

B101	0 229		Precast	Plank with	No Topping	l		
	SPAN	SUPERIMPOSED	TOTAL	DEAD	TOTAL	CC	ST PER S.F.	
	(FT.)	LOAD (P.S.F.)	DEPTH (IN.)	LOAD (P.S.F.)	LOAD (P.S.F.)	MAT.	INST.	TOTAL
0720	10	40	4	50	90	4.88	2.75	7.6
0750	RB1010	75	6	50	125	6.05	2.35	8.4
0770	-010	100	6	50	150	6.05	2.35	8.4
0800	15	40	6	50	90	6.05	2.35	8.4
0820	RB1010	75	6	50	125	6.05	2.35	8.4
0850	-100	100	6	50	150	6.05	2.35	8.4
0875	20	40	6	50	90	6.05	2.35	8.4
0900	-	75	6	50	125	6.05	2.35	8.4
0920	25 x 30	100	6	50	. 150	6.05	2.35	8.4
0950	25	40	6	50	90	6.05	2.35	8.4
0970		75	8	55	130	6.35	2.06	8.4
1000		100	8	55	155	6.35	2.06	8.4
1200	30	40 .	8	55	95	6.35	2.06	-8.4
1300		75	8	55	130	6.35	2.06	8.4
1400		100	10	70	170	6.70	1.83	8.5
1500	40	40	10	70	110	6.70	1.83	8.5
1600		75	12	70	145	7.60	1.65	9.2

72 Important: See the Reference Section for critical supporting data - Reference Numbers and City Cost Indexes

B1 B1

**B1** 

1700 B1

> 200 210

B1010 Floor Construction			212 2 13	107 101		
		flo te	ors and ro	used for mode ofs. At shorter ompetitive with are also used a	spans, they h hollow cor	e
		930	123.040	CC	OST PER S.F.	
System Components		QUANTITY	UNIT	CC MAT.	OST PER S.F. INST.	TOTAL
System Components SYSTEM B1010 235 6700 PRECAST, DOUBLE "T", 2" TOPPING, 30' SPAN, 30 PSF SUP. LOAD, 18" X 8' Double "T" beams, reg. vt, 18" x 8' w, 30' span Edge forms to 6" high on elevated slab, 4 uses Concrete ready mix, regular weight, 3000 psi Place and vibrate concrete, elevated slab less than 6", pumped Finishing floor, monolithic steel trowel finish floor Curing with sprayed membrane curing compound	(12) (12) (12) (12) (12) (12) (12) (12)	QUANTITY 1.000 .050 .250 1.000 .010	UNIT S.F. L.F. C.F. C.F. S.F. C.S.F.		the second s	TOTAL

	47444	CUDEDINDOCED	DBL. "T" SIZE	CONCRETE "T"	TOTAL LOAD (P.S.F.)	COST PER S.F.		
	SPAN (FT.)	SUPERIMPOSED LOAD (P.S.F.)	D (IN.) W (FT.)	TYPE		MAT.	INST.	TOTAL
500	30	30	18x8	Reg. Wt.	92	7.30	1.37	8.67
.600	RB1010 -010	40	18x8	Reg. Wt.	102	7.40	1.78	9.18
700		50	18x8	Reg. Wt	112	7.40	1.78	9.18
800		75	18x8	Reg. Wt.	137	7.45	1.85	9.30
1900		100	18x8	Reg. Wt.	162	7.45	1.85	9.30
	40	30	20x8	Reg. Wt.	87	5.65	1.14	6.79
2000	40 RB1010 -100	40	20x8	Reg. Wt.	97	5.70	1.38	7.08
2100		50	20x8	Reg. Wt.	107	5.70	1.38	7.08
2200		- 75	20x8	Reg. Wt.	132	5.75	1.48	7.23
2300		100	20x8	Reg. Wt.	157	5.85	1.82	7.67
2400	50	30	20x8	Reg. Wt.	103	5.95	1.03	6.98
2500	50		24x8	Reg. Wt.	113	6	1.26	7.28
2600		40	24x8	Reg. Wt.	123	6.05	1.34	7.39
2700		50	24x8	Reg. Wt.	148	6.05	1.36	7.41
2800		75	24x8	Reg. Wt.	173	6.15	1.70	7.85
2900		100	24x8	Reg. Wt.	82	6.05	1.36	7.4
3000	60	30	24x8 32x10	Reg. Wt.	104	7.05	1.12	8.1
3100		40	32x10	Reg. Wt.	114	7	.97	7.9
3150		50		Reg. Wt.	139	7.05	1.05	8.1
3200		75	32x10		164	7.10	1.31	8.4
3250		100	32x10	Reg. Wt.	94	7.05	1.04	8.0
3300	70	30	32x10	Reg. Wt.	104	7.05	1.05	8.1
3350		40	32x10	Reg. Wt.	104	7.10	1.31	8.4
3400		50	32x10	Reg. Wt.	139	7.20	1.58	8.7
3450		75	32x10	Reg. Wt.	164	7.35	2.11	9.4
3500		100	32x10	Reg. Wt.		7.10	1.31	8.4
3550	80	30	32x10	Reg. Wt.	94	7.10	1.84	9.1
3600		40	32x10	Reg. Wt.	104	7.30	2.10	9.4
3900		50	32x10	Reg. Wt.	114	7.35	2.10	9.4

Important: See the Reference Section for critical supporting data - Reference Numbers and City Cost Indexes

B' B'